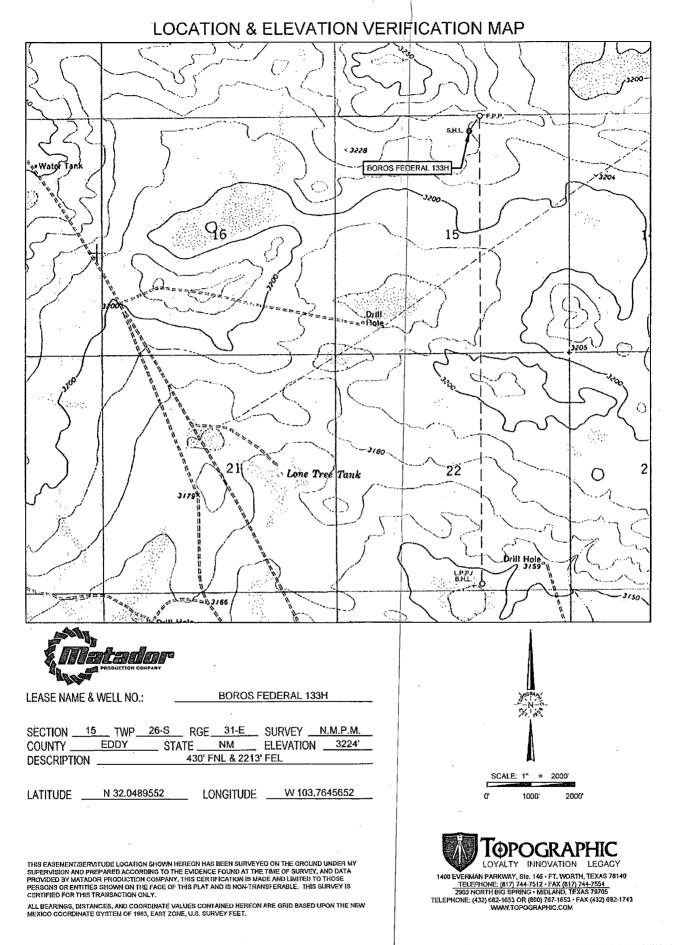
RECEIVED	RECEIVED	
Form 3160-3 (June 2015) DEC 2 6 2019 UNITED SD/S		FORM APPROVED OMB No. 1004-0137 Expires: January 31, 2018
DISTRICT/ARTERACTOR DISTRICTOR DISTACTOR DISTRICTOR DISTRICTOR DISTRICTOR DISTRICTOR DISTRICTOR		5. Lease Serial No. NMNM138865
APPLICATION FOR PERMIT TO I		6, If Indian, Allotee or Tribe Name
Ib. Type of Well:     Image: Completion in the second	REENTER Dther Single Zone 🔲 Multiple Zone	7. If Unit or CA Agreement, Name and No. 8. Lease Name and Well No. BOROS FEDERAL 133H 3 2 6 3 29
2. Name of Operator MATADOR PRODUCTION COMPANY		9. API Well No. 30-015-4657/
3a, Address 5400 LBJ Freeway, Suite 1500 Dallas TX 75240	3b. Phone No, <i>(incluide area code)</i> (972)371-5200	2ND BONE SPRING SHALE 97860
<ol> <li>Location of Well (Report location clearly and in accordance At surface NWNE / 430 FNL / 2213 FEL / LAT 32,048 At proposed prod, zone SWSE / 100 FSL / 1980 FEL / 1</li> </ol>	9552 / LONG -103.7645652	11, Sect T, R, M, of Blk, and Survey or Area SEC 15//T265:/ R31E / NMP 24
14. Distance in miles and direction from nearest town or post of	lice*	12. County or Parish 13, State EDDY NM
<ul> <li>15. Distance from proposed*</li> <li>430 feet</li> <li>property or lease line, ft.</li> <li>(Also to nearest drig, unit line, if any)</li> </ul>	1240 320	Spacing Unit dedicated to this well
<ol> <li>Distance from proposed location* to nearest well, drilling, completed, 30 feet applied for, on this lease, ft.</li> </ol>	NA CONT	BLM/BIA Bond No, in file D: NMB001079
21. Elevations (Show whether DF, KDB. RT, GL, etc.) 3224 feet	22.7Approximate date work will start	23. Estimated duration 60 days
The following, completed in accordance with the requirements (as applicable)	24. Attachments	the Hydraulic Fracturing rule per 43 CFR 3162:3-3
<ol> <li>Well plat certified by a registered surveyor,</li> <li>A Drilling Plan,</li> <li>A Surface Use Plan (if the location is on National ForestSyster SUPO must be filed with the appropriate Horest Service Office</li> </ol>	Item 20 above) en Lands, the 5. Operator certification by 6, Such other site specific	rations unless covered by an existing bond on file (see
25. Signature (Electronic Submission)	BLM. Name (Printed/Typed) Lara Thompson / Ph: (505)25	Datc 4-1115 05/01/2019
Title Assistant Project Manager		
Approved by (Signature) (Electronic Submission)	Name (Printed/Typed) Christopher Walls / Ph: (575):	Date 234-2234 12/05/2019
Title Petroleum Engineer Application approval does not warrant or certify that the applica applicant to conduct operation at the conduct operation		
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, of the United States any false, fictitious or fraudulent statements		
	VED WITH CONDITION	VS
(Continued on page 2)	Vol Date: 12/05/2019	*(Instructions on page 2)

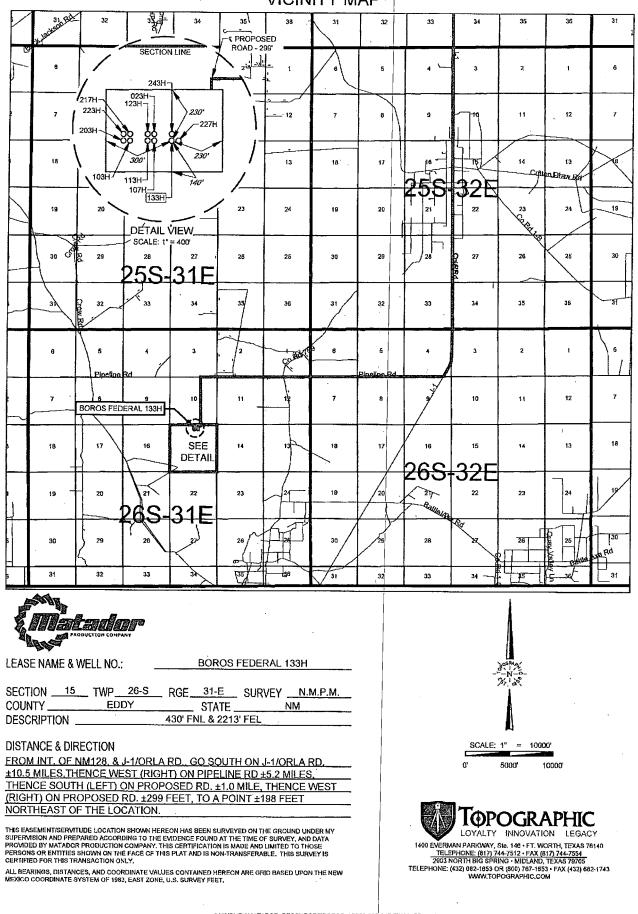
Å

Rw 1-8-2020

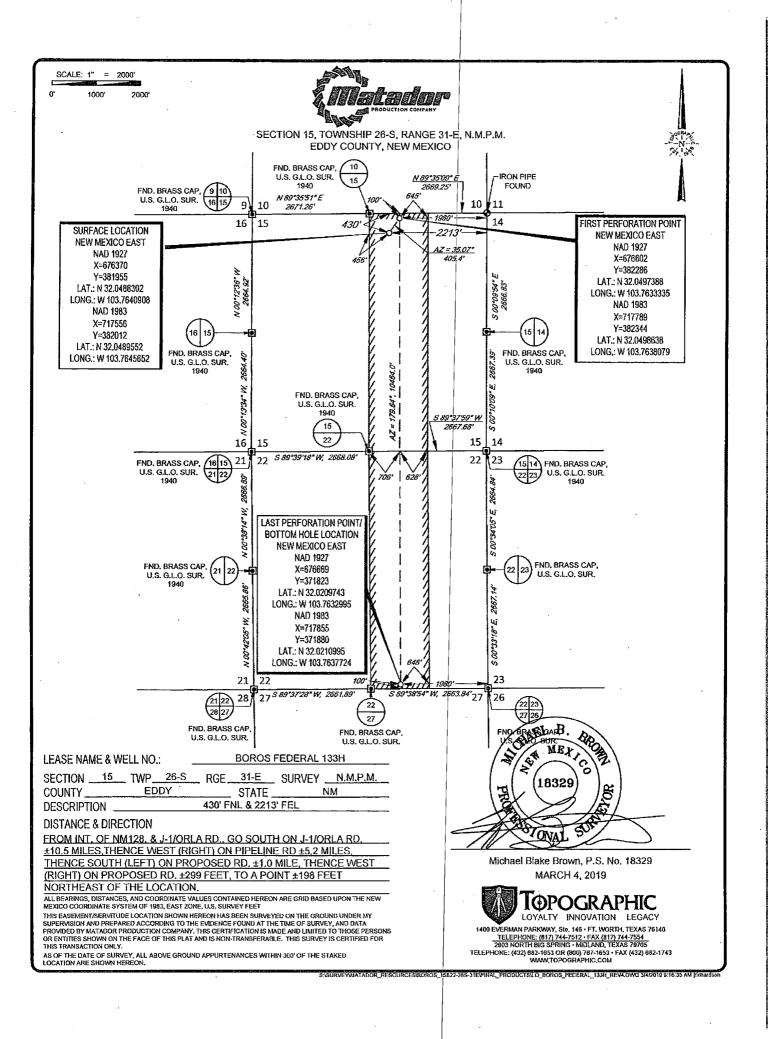


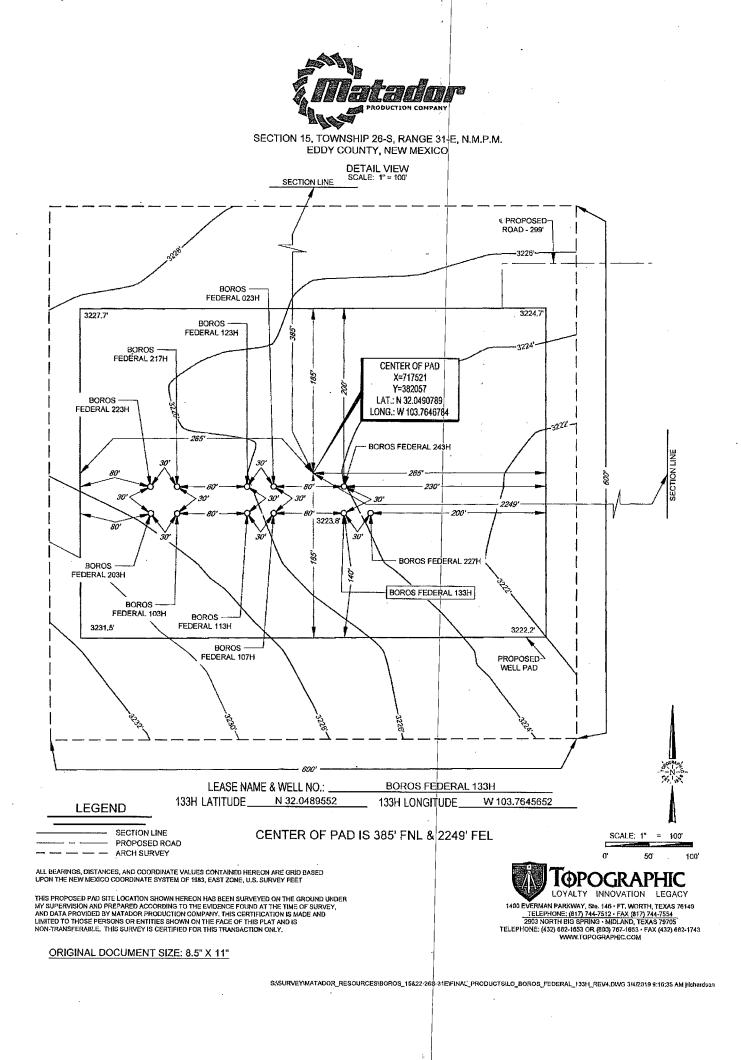
SISURVEYIMATADOR\_RESOURCESIBOROS\_15822-25-31EVFINAL\_PRODUCTSILO\_BOROS\_FEDERAL\_133H\_REV4.DWG 3/4/2019 9:16:34 AM jitchardson

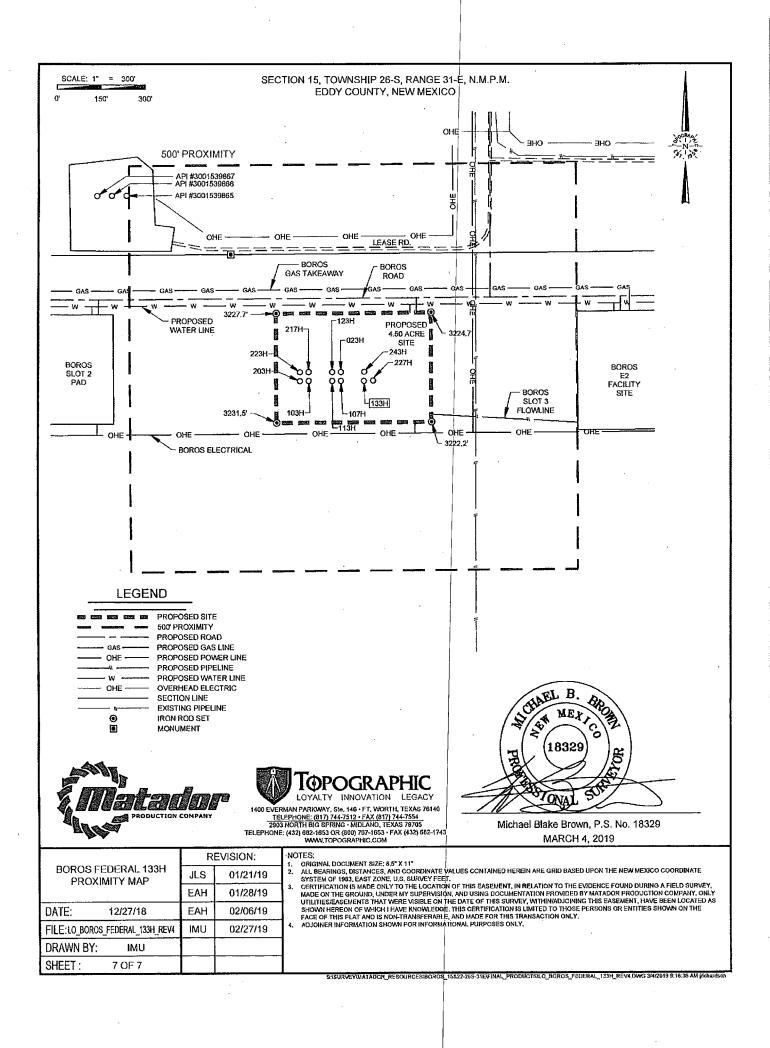
VICINITY MAP



SISURVEYIMATADOR\_RESOURCES/BOROS\_15822-265-31E/FINAL\_PRODUCTS/LO\_BOROS\_FEDERAL\_133H\_REV4.DWG 3/4/2019 9:16:34 AM jrichardson







# **FMSS**

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT Drilling Plan Data Report

12/06/2019

APD ID: 10400041094

Operator Name: MATADOR PRODUCTION COMPANY

Submission Date: 05/01/2019

Highlighted data reflects the most recent changes

Well Name: BOROS FEDERAL

Well Number: 133H

Show Final Text

Well Type: OIL WELL

Well Work Type: Drill

# **Section 1 - Geologic Formations**

Formation ID	Formation Name	Elevation	True Vertical Depth	Measured Depth		Lithologies	Mineral Resources	Producing Formation
1	RUSTLER	1868	1356	1356		ANHYDRITE	NONE	N
2	TOP SALT	384	1488	1488		SALT	NONE	N
3	CASTILE	-1519	3391	3391		SALT	NONE	N
· 4	BASE OF SALT	-2225	4097	4097		SALT	NONE	N
5	BELL CANYON	-2254	4126	4126		SANDSTONE	NATURAL GAS,OIL	N
6	CHERRY CANYON	-3307	5179	5179		SANDSTONE	NATURAL GAS, ÖIL	N
7	BRUSHY CANYON	-4513	6385	6385		SANDSTONE	NATURAL GAS,OIL	N
8	BONE SPRING LIME	-6196	8068	8068	4	LIMESTONE	NATURAL GAS,OIL	N
9	BONE SPRING 1ST	-7340	9212	9212	ΟΤΙ	HER,SANDSTONE : Carbonate	NATURAL GAS,OIL	N
10	BONE SPRING 2ND	-7620	9492	9492	ОТ	HER,SANDSTONE : Carbonate	NATURAL GAS,OIL	N
11	BONE SPRING 3RD	-8334	10202	10202	2	SANDSTONE	NATURAL GAS,OIL	Y

# **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M

Rating Depth: 12000

**Equipment:** A 12,000' 5000 psi BOP stack consisting of 3 rams with 2 pipe rams,1 blind ram,and one annular preventer will be utilized below surface casing to TD. See attachments for BOP and choke manifold diagrams. An accumulator complying with Onshore Order#2 requirements for the pressure rating of the BOP stack will be present. A rotating head will also be installed as needed.

Requesting Variance? YES

**Variance request:** Matador requests a variance to have the option of running a multi-bowl wellhead assembly for setting the Intermediate 1 and Production Strings. The BOPs will not be tested again unless any flanges are separated. Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. The hose is not required by the manufacturer to be anchored. If the specific hose is not available, then one of equal or higher rating will be used. Matador requests a variance to have the option of batch drilling this well with other

## Operator Name: MATADOR PRODUCTION COMPANY

Well Name: BOROS FEDERAL

#### Well Number: 133H

wells on the same pad. In the event that this well is batch drilled, the wellbore will be secured with a blind flange of like pressure. When the rig returns to this well and BOPs are installed, the operator will perform a full BOP test. **Testing**, **Procedure:** BOP will be inspected and operated as required in Onshore Order#2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position. A third party company will test the BOPs. After setting surface casing, a minimum 5M BOPE system will be installed. Test pressures will be 250psi low and 5000psi high with the annular preventer being tested to 250psi low and 2500psi high before drilling below surface shoe. In the event that the rig drills multiple wells on the pad and any seal subject to test pressures are broken, a full BOP test will be performed when the rig returns and the 5M BOPE system is re-installed.

## **Choke Diagram Attachment:**

Boros\_Federal\_\_133H\_5M\_Choke\_Manifold\_Arrangement\_20190424111917.pdf

## BOP Diagram Attachment:

Boros\_Federal\_\_133H\_5M\_BOP\_20190424111954.pdf

Boros\_Federal\_\_133H\_Co\_Flex\_Certs\_20190424111958.pdf

Section 3 - Casing

Casing ID	String Type	Hole Size	sg Size	Condition	Standard	Tapered String	op Set MD	Bottom Set MD	op Set TVD	Bottom Set TVD	op Set MSL	Bottom Set MSL	alculated casing	length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
O	ت	I	U U	·O	Ś	ΗË	Ĕ	õ	ГĔ	ā	Ĕ	m	ပြီ	lei	9	3	٦٢	0	ā	٦٢	ř	õ	õ
1	SURFACE	17.5	13.375	NEW	API	N	0	1381	0	1381			138	81	J-55	54.5	BUTT	-	1.12 5	BUOY	1.8	BUOY	1.8
2		12.2 5	9.625	NEW	API	N	0	4151	0	4151			415	51	J-55	40	BUTT	-	1.12 5	BUOY	1.8	BUOY	1.8
3	PRODUCTI ON	8.75	5.5	NEW	API	N	0	21587	0	11279			21	587	P- 110		OTHER - DWC/C-IS HT Plus	-	1.12 5	BUOY	1.8	BUOY	1.8

## **Casing Attachments**

perator Name: MATADOR PRODUCTION COMPANY	
ell Name: BOROS FEDERAL Well I	Number: 133H
· · · · · · · · · · · · · · · · · · ·	
asing Attachments	
Casing ID:     1     String Type:SURFACE       Inspection Document:	
Spec Document:	
Tapered String Spec:	
Casing Design Assumptions and Worksheet(s):	
Boros_Federal133H_BLM_Casing_Design_Assumption	s_3_string_20190424112109.pdf
Casing ID: 2 String Type: INTERMEDIATE Inspection Document:	· · · ·
Spec Document:	
Tapered String Spec:	
Casing Design Assumptions and Worksheet(s):	
Boros_Federal133H_BLM_Casing_Design_Assumption	s_3_string_20190424112122.pdf
Casing ID: 3 String Type: PRODUCTION	
Inspection Document:	
Spec Document:	
Tapered String Spec:	
Casing Design Assumptions and Worksheet(s):	
Boros_Federal133H_BLM_Casing_Design_Assumption	s_3_string_20190424112134.pdf
Section 4 - Cement	

•

**Operator Name:** MATADOR PRODUCTION COMPANY **Well Name:** BOROS FEDERAL

Well Number: 133H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	ı Ft	Excess%	Cement type	Additives
び	Le	ŭ ŭ	To	Щ	ð	Ϋ́	ă	Сп	μ <b>ω</b>	Ŭ	Ac
SURFACE	Lead		0	1081	700	1.72	12.5	1198	50	С	5% NaCl + LCM
SURFACE	Tail	,	1081	1381	250	1.38	14.8	347	50	С	5% NaCl + LCM
INTERMEDIATE	Lead		0	3321	780	2.13	12.6	1663	50	С	Bentonite + 1% CaCL2 + 8% NaCl + LCM
INTERMEDIATE	Tail		3321	4151	310	1.38	14.8	424	50	С	5% NaCl + LCM
PRODUCTION	Lead		3951	1024 4	890	2.22	11.5	1976	25	н	Fluid Loss + Dispersant + Retarder + LCM
PRODUCTION	Tail		1024 4	1127 9	2660	1.35	13.2	3592	25	H	Fluid Loss + Dispersant + Retarder + LCM

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

**Describe what will be on location to control well or mitigate other conditions:** All necessary mud products (barite,bentonite,LCM) for weight addition and fluid loss control will be on location at all times. Mud program is subject to change due to hole conditions.

**Describe the mud monitoring system utilized:** An electronic Pason mud monitoring system complying with Onshore Order 2 will be used.

# Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (Ibs/gal)	Max Weight (Ibs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	Н	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	1381	SPUD MUD	8.4	8.8				-			
1381	4151	SALT SATURATED	9.5	10.2							
4151	1127 9	OTHER : FW/Cut Brine	8.6	9.4							

Page 4 of 6

# Operator Name: MATADOR PRODUCTION COMPANY Well Name: BOROS FEDERAL

Well Number: 133H

# Section 6 - Test, Logging, Coring

## List of production tests including testing procedures, equipment and safety measures:

A 2-person mud logging program will be used from Kick-off point to TD. No electric logs are planned at this time. GR will be collected through the MWD tools from Intermediate casing to TD. CBL with CCL will be run as far as gravity will let it fall to top of curve.

List of open and cased hole logs run in the well:

CBL,GR

#### Coring operation description for the well:

No core or drill stem test is planned.

## Section 7 - Pressure

Anticipated Bottom Hole Pressure: 5513

Anticipated Surface Pressure: 3031.62

Anticipated Bottom Hole Temperature(F): 186

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

**Contingency Plans geoharzards description:** 

Contingency Plans geohazards attachment:

Hydrogen Sulfide drilling operations plan required? NO

Hydrogen sulfide drilling operations plan:

## Section 8 - Other Information

## Proposed horizontal/directional/multi-lateral plan submission:

Boros\_Federal\_\_133H\_Directional\_AC\_Report\_v1\_20190424112425.pdf

Boros\_Federal\_\_133H\_Directional\_Well\_Plan\_v1\_20190424112427.pdf

## Other proposed operations facets description:

## Other proposed operations facets attachment:

Boros Federal\_133H\_Closed\_Loop\_System\_20190424112523.pdf

Boros\_Federal\_\_133H\_Drill\_Plan\_20190424112524.pdf

H2S\_Plan\_20190424112524.pdf

Boros\_Federal\_\_133H\_BLM\_Casing\_Design\_Assumptions\_3\_string\_20190424112555.pdf

Gas\_Capture\_Plan\_\_\_Boros\_Federal\_\_023H\_103H\_\_107H\_\_113H\_\_123H\_\_133H\_\_203H\_\_217H\_\_223H\_\_227H\_\_24 3H\_20190424112959.docx

## Other Variance attachment:

## **Casing Design Criteria and Load Case Assumptions**

## Surface Casing

## Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

## Intermediate #2 Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43, psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
  pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
  with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
  (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
  which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

## **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud
  gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient
  of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

## Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Casing Design Criteria and Load Case Assumptions**

#### **Surface Casing**

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a
more conservative backup force than pore
pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

#### Intermediate #2 Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

#### **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud
  gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient
  of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

## Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Casing Design Criteria and Load Case Assumptions**

## Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF<sub>b</sub>=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

## Intermediate #2 Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
  gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
  pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
  pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
  with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
  (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
  which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

## **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

## Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

## Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Casing Design Criteria and Load Case Assumptions**

#### Surface Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

## Intermediate #2 Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
  pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
  with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
  (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
  which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

#### **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud
  gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient
  of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

#### Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Casing Design Criteria and Load Case Assumptions**

## **Surface Casing**

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

#### Intermediate #2 Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
  pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
  with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
  (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
  which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

## **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

#### Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).



# **Matador Production Company**

Rustler Breaks Boros Boros Federal #133H

Wellbore #1

Plan: BLM Plan #1

# **Standard Planning Report**

03 April, 2019



Database:										
		5000.14 Single			Local Co-c	ordinate Ref	erence:	Well Boros Feder	al #133H	
ompany:	Matad	or Production C	Company		TVD Refer	ence:	1 . I	KB @ 3252.5usft		
roject:	Rustle	r Breaks			MD Refere	nce:	) I	KB @ 3252.5usft		
ite:	Boros				North Refe	erence:		Grid		
/ell:	Boros	Federal #133H			Survey Ca	Iculation Me	thod:	Minimum Curvatu	ire	
lelibore:	Wellbo	ore #1			•					
esign:	BLM F									
		·				`	h		• • •	· · · · · · · · · · · · · · · · · · ·
Project	Rustler	Breaks					r	• • -		·····
Map System: Geo Datum:		Plane 1927 (E 7 (NADCON C			System Dat	um:	Me	ean Sea Level		
Map Zone:	New Mex	cico East 3001					Us	ing geodetic scal	e factor	
Site	Boros		A 1	. <u></u> at.		· · · · · · · · · · · · · · · · · · ·		<u>_</u>		· · · · · · · · · · · · · · · · · · ·
					201	052.26	· · · ·		•	000 01 55 700 1
Site Position:			Northi	-		953.36 usft	Latitude:			32° 2' 55.786 I
rom:		Long	Easting	-	676,	179.89 usft	Longitude:			103° 45' 52.934 V
Position Uncert	tainty:		) usft Slot Ra	adius:	un	13-3/16 "	Grid Converg	ence:	<u> </u>	0.30
Well	Boros F	ederal #133H			<u></u>		-			· · · ·
Well Position	+N/-S	1.	.3 usft No	rthing:	•	381,954.6	5 usft Lati	itude:		32° 2' 55.789 I
	+E/-W	190.		sting:		676,369.8	35 usft Lon	gitude:		103° 45' 50.727 V
Position Uncert	tainty	0		lihead Elevat	ion <sup>.</sup>			und Level:		3,224.0 us
						<u> </u>				
Welibore	Wellbo	ore #1			. ~	u	- m.		- 1	
Magnetics	Мо	del Name	Sample	e Date	Declina	tion	Dip A	-		Strength
		IGRF200510		2/31/2009	(°)	7.82	(°	60.04		nT) 666.85486204
Design	BLM PI	on #1		· · · · · · · · · · · ·	······				~ `	
Design		-				R	· · · · ·	• • • •		,
Audit Notes:										
	4		<b>D</b> h			-		,		
Version:	1		Phase		PLAN	۲	ie On Depth:		0.0	
Version: Vertical Sectior		D	epth From (TV		+N/-S	1 1 1 1	E/-W	Dire	ction	
		D				1 1 1 1		Dire		
		D	epth From (TV		+N/-S	1 1 1 1	E/-W	Dire (	ction	
Vertical Section	n:		Pepth From (TV (usft) 0.0		+N/-S (usft)	1 1 1 1	E/-W (usft)	Dire (	ction °}	· · · · ·
Vertical Sectior Plan Survey To	n: pol Program	Date	epth From (TV (usft)		+N/-S (usft)	1 1 1 1	E/-W (usft)	Dire (	ction °}	
Vertical Section Plan Survey To Depth Fre	n: pol Program om Depti	Date h To	epth From (TV (usft) 0.0 4/3/2019		+N/-S (usft) 0.0	1 1 1 1	-E/-W (usft) 0.0	Dire (	ction °}	· · · · ·
Vertical Section Plan Survey To Depth Fro (usft)	n: bol Program om Depti (us	Date h To ft) Survey	Vepth From (TV (usft) 0.0 4/3/2019 (Wellbore)	/D)	+N/-S (usft) 0.0 Tool Name	1 1 1 1	E/-W (usft)	Dire (	ction °}	· · · · ·
Vertical Section Plan Survey To Depth Fre	n: pol Program om Depti (us	Date h To	Vepth From (TV (usft) 0.0 4/3/2019 (Wellbore)	/D)	+N/-S (usft) 0.0 Tool Name MWD		-E/-W (usft) 0.0	Dire (	ction °}	· · · · ·
Vertical Section Plan Survey To Depth Fro (usft)	n: bol Program om Depti (us	Date h To ft) Survey	Vepth From (TV (usft) 0.0 4/3/2019 (Wellbore)	/D)	+N/-S (usft) 0.0 Tool Name		-E/-W (usft) 0.0	Dire (	ction °}	· · · · ·
Vertical Section Plan Survey To Depth Fro (usft)	n: bol Program om Depti (us	Date h To ft) Survey	Vepth From (TV (usft) 0.0 4/3/2019 (Wellbore)	/D)	+N/-S (usft) 0.0 Tool Name MWD		-E/-W (usft) 0.0	Dire (	ction °}	
Vertical Section Plan Survey To Depth Frr (usft) 1 Plan Sections	n: bol Program om Depti (us	Date h To ft) Survey	epth From (TV (usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore	/D)	+N/-S (usft) 0.0 Tool Name MWD	Standard	FE/-W (usft) 0.0 Remarks	Dire ( 17!	ction °}	
Vertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured	n: ool Program om Depti (us 0.0 21,5	Date h To ft) Survey 587.3 BLM Pla	Vertical	(D) = #1)	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD	Standard	E/-W usft) 0.0 Remarks Build	Dire ( 179	ction °} 9.64	
/ertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth	n: ool Program om Depti (us 0.0 21,5	Date h To ft) Survey 587.3 BLM Pla Azimuth	Vertical Depth From (TV (usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore)	'D) ⇒ #1) +N/-S	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD - +E/-W	- Standard Dogleg	E/-W usft) 0.0 Remarks Build Rate	Dire ( 179	ction °) 9.64	
Vertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured	n: ool Program om Depti (us 0.0 21,5	Date h To ft) Survey 587.3 BLM Pla	Vertical	(D) = #1)	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD	Standard	E/-W usft) 0.0 Remarks Build	Dire ( 179	ction °} 9.64	Target
/ertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth (usft)	n: ool Program om Depti (us 0.0 21,5 0.0 21,5 Inclination (°)	Date h To ft) Survey 587.3 BLM Pla 587.3 Azimuth (°)	Vertical Depth (Usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft)	'D) ∋ #1) +N/-S (usft)	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD - +E/-W (usft)	- Standard Dogleg Rate (°/100usft)	E/-W (usft) 0.0 Remarks Build Rate (°/100usft)	Dire ( 175	ction °) 9.64 TFO (°)	Target
/ertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth (usft) 0.0	n: ool Program om Depti (us 0.0 21,5 0.0 21,5 Inclination (°) 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 BLM Pla 687 587 587 587 587 587 587 587 587 587 5	Vertical Usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0	(D) = #1) +N/-S (usft) 0.0	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0	- Standard Dogleg Rate (°/100usft) 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00	Dire ( 175	ction °) 9.64 TFO (°) 0.00	Target
Vertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0	n: ool Program om Deptil (us 0.0 21,5 0.0 21,5 (°) 0.00 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 Contemporation 587.3 Date 587.3 Date 597.3 Date	Vertical Usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0 1,500.0	(D) +N/-S (usft) 0.0 0.0	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 0.0	Standard Dogleg Rate (°/100usft) 0.0 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00	Dire ( 175 Turn Rate (°/100usft) 0.00 0.00	Ction °) 9.64 (°) (°) 0.00 0.00	Target
/ertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth (usft) 0.0	n: ool Program om Depti (us 0.0 21,5 0.0 21,5 Inclination (°) 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 Contemporation 587.3 BLM Pla 587.3 Date 587.3 Date 597.3 D	Vertical (usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0 1,500.0 2,494.9	(D) +N/-S (usft) 0.0 0.0 67.8	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 0.0 54.6	Standard Dogleg Rate (°/100usft) 0.0 0.0 1.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00	Dire ( 17: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7	ction °) 9.64 TFO (°) 0.00 0.00 38.85	Target
Vertical Section Plan Survey To Depth Fro (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0	n: ool Program om Deptil (us 0.0 21,5 0.0 21,5 (°) 0.00 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 Contemporation 587.3 Date 587.3 Date 597.3 Date	Vertical Usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0 1,500.0	(D) +N/-S (usft) 0.0 0.0	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 0.0	Standard Dogleg Rate (°/100usft) 0.0 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00	Dire ( 175 Turn Rate (°/100usft) 0.00 0.00	ction °) 9.64 TFO (°) 0.00 0.00 38.85 0.00	Target
/ertical Section Plan Survey To Depth Fre (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0 2,500.0	n: ool Program om Depti (us 0.0 21,5 Inclination (°) 0.00 0.00 10.00	Date h To ft) Survey 587.3 BLM Pla 587.3 Contemporation 587.3 BLM Pla 587.3 Date 587.3 Date 597.3 D	Vertical (usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0 1,500.0 2,494.9	(D) +N/-S (usft) 0.0 0.0 67.8	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 0.0 54.6	Standard Dogleg Rate (°/100usft) 0.0 0.0 1.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00 0 0.00	Dire ( 17: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7: 7	ction °) 9.64 TFO (°) 0.00 0.00 38.85	Target
Vertical Section Plan Survey To Depth Fre (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0 2,500.0 4,484.5 5,151.2	n: ool Program om Depti (us 0.0 21,5 Inclination (°) 0.00 0.00 10.00 10.00 10.00 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 BLM Pla 60.00 0.00 38.85 38.85 0.00	Vertical (usft) 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) vertical Depth (usft) 0.0 1,500.0 2,494.9 4,449.3 5,112.6	<pre>/D) +N/-S (usft) 0.0 0.0 67.8 336.2 381.4</pre>	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 0.0 54.6 270.8 307.2	Standard Dogleg Rate (°/100usft) 0.0 0.0 1.0 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00 0 0.00 0 -1.50	Dire ( 17: Turn Rate (°/100usft) 0.00 0.00 0.00 0.00 0.00	ction °) 9.64 (°) (°) 0.00 0.00 38.85 0.00 180.00	
Vertical Section Plan Survey To Depth Frr (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0 2,500.0 4,484.5 5,151.2 10,744.6	n: ool Program om Depti (us 0.0 21,5 Inclination (°) 0.00 0.00 10.00 10.00 10.00 0.00 0.00 0.00 0.00 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 BLM Pla 60.00 0.00 38.85 38.85 38.85 0.00 0.00	Vertical 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Depth (usft) 0.0 1,500.0 2,494.9 4,449.3 5,112.6 10,706.0	<pre>/D) +N/-S (usft) 0.0 67.8 336.2 381.4 381.4</pre>	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 54.6 270.8 307.2 307.2	Standard Dogleg Rate (°/100usft) (°/100usft) 0.0 0.0 1.0 0.0 1.5 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00 0 0.00 0 -1.50 0 0.00	Dire ( 17: 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	ction °) 9.64 TFO (°) 0.00 0.00 38.85 0.00 180.00 0.00	
Vertical Section Plan Survey To Depth Frr (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0 2,500.0 4,484.5 5,151.2 10,744.6 11,644.6	n: ool Program om Depti (us 0.0 21,5 Inclination (°) 0.00 0.00 10.00 10.00 10.00 0.00 0.00 90.00	Date h To ft) Survey 587.3 BLM Pla 587.3 BLM Pla 600 0.00 38.85 38.85 38.85 0.00 0.00 185.60	Vertical 0.0 (Wellbore) an #1 (Wellbore) an #1 (Wellbore) Vertical Depth (usft) 0.0 1,500.0 2,494.9 4,449.3 5,112.6 10,706.0 11,279.0	<pre>/D) +N/-S (usft) 0.0 67.8 336.2 381.4 381.4 -188.9</pre>	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 54.6 270.8 307.2 307.2 307.2 251.2	Standard	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00 0 -1.50 0 0.00 0 10.00	Dire ( 17: 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	ction °) 9.64 TFO (°) 0.00 0.00 38.85 0.00 180.00 0.00 185.60	
Vertical Section Plan Survey To Depth Frr (usft) 1 Plan Sections Measured Depth (usft) 0.0 1,500.0 2,500.0 4,484.5 5,151.2 10,744.6	n: ool Program om Depti (us 0.0 21,5 Inclination (°) 0.00 0.00 10.00 10.00 10.00 0.00 0.00 0.00 0.00 0.00	Date h To ft) Survey 587.3 BLM Pla 587.3 BLM Pla 60.00 0.00 38.85 38.85 38.85 0.00 0.00	Vertical 0.0 4/3/2019 (Wellbore) an #1 (Wellbore) Depth (usft) 0.0 1,500.0 2,494.9 4,449.3 5,112.6 10,706.0	<pre>/D) +N/-S (usft) 0.0 67.8 336.2 381.4 381.4</pre>	+N/-S (usft) 0.0 Tool Name MWD OWSG MWD OWSG MWD +E/-W (usft) 0.0 54.6 270.8 307.2 307.2	Standard Dogleg Rate (°/100usft) (°/100usft) 0.0 0.0 1.0 0.0 1.5 0.0	E/-W (usft) 0.0 Remarks Build Rate (°/100usft) 0 0.00 0 0.00 0 1.00 0 0.00 0 -1.50 0 0.00 0 10.00 0 0.00	Dire ( 17: 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	ction °) 9.64 TFO (°) 0.00 0.00 38.85 0.00 180.00 0.00 185.60 -90.00	Target VP - Boros Federal # BHL - Boros Federal



EDM 5000.14 Single User Db

Matador Production Company

Rustler Breaks

Wellbore #1

BLM Plan #1

Boros Federal #133H

Boros

## Planning Report

Local Co-ordinate Reference: TVD Reference: MD Reference: North Reference: Survey Calculation Method:

1

Well Boros Federal #133H

KB @ 3252.5usft KB @ 3252.5usft

Grid

Minimum Curvature

Planned Survey

Database:

Company:

Project:

Wellbore:

Design:

Site:

Well:

Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	) 0.00 0.0	Azimuth (*) 0.00	Depth (usft) 0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,709.9	+N/-S (usft) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	+E/-W (usft) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(usft) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(°/100usft) 0.000 0.00	(*/100usft) 0.00	(°/100usft) 0.000 0.00
100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,356.2 <b>Rustler</b> 1,400.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,300.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,900.0 3,000.0 3,300.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100.0 200.0 300.0 400.0 500.0 600.0 700.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,100.0 1,300.0 1,356.2 Rustler 1,400.0 1,356.2 Rustler 1,400.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,600.0 2,600.0 2,600.0 2,600.0 2,600.0 3,000.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,100.0 1,300.0 1,356.2 Rustler 1,400.0 1,356.2 Rustler 1,400.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,600.0 2,600.0 2,600.0 2,600.0 2,600.0 3,000.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	200.0 300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,000.0 1,200.0 1,200.0 1,200.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 1,700.0 2,000.0 2,000.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 2,900.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	300.0 400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,300.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 2,000.0 2,000.0 2,000.0 2,000.0 2,000.0 2,000.0 2,000.0 2,600.0 Start 1984.5 hold at 2 2,600.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 38.85 38.85 38.85	400.0 500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
500.0 600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 <b>Start Build 1.00</b> 1,800.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	500.0 600.0 700.0 800.0 900.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 2,000.0 2,000.0 2,000.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,000.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	600.0 700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
700.0 800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,300.0 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,000.0 3,000.0 3,100.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	700.0 800.0 900.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
800.0 900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 1,800.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	800.0 900.0 1,000.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,300.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 38.85 38.85 38.85	900.0 1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 1,700.0 2,000.0 2,000.0 2,000.0 2,000.0 2,300.0 2,300.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,000.0 3,300.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 38.85 38.85 38.85	1,000.0 1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00
1,100.0 1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 1,800.0 2,000.0 2,100.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 0.00 0.00 38.85 38.85 38.85	1,100.0 1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 0.00
1,200.0 1,300.0 1,356.2 <b>Rustler</b> 1,400.0 1,487.5 <b>Salado (Top Salt)</b> 1,500.0 <b>Start Build 1.00</b> 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,300.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 <b>Start 1984.5 hold at 2</b> 2,600.0 3,000.0 3,000.0 3,300.0 3,300.0 3,300.0 3,500.0	0.00 0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 0.00 38.85 38.85 38.85	1,200.0 1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00
1,300.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,200.0 2,300.0 2,300.0 2,600.0 2,600.0 2,600.0 3,700.0 3,000.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 38.85 38.85 38.85	1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00
1,300.0 1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,000.0 2,000.0 2,200.0 2,300.0 2,300.0 2,600.0 2,600.0 2,600.0 3,700.0 3,000.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	0.00 0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 0.00 38.85 38.85 38.85	1,300.0 1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00
1,356.2 Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 1,900.0 2,000.0 2,000.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 0.00 38.85 38.85 38.85	1,356.2 1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0 0.0 -0.7	0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00 0.00 1.00	0.00 0.00 0.00
Rustler 1,400.0 1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 2,000.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 3,000.0 3,000.0 3,100.0 3,300.0 3,300.0 3,300.0 3,300.0 3,300.0	0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 38.85 38.85 38.85	1,400.0 1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.0 0.5 2.2	0.0 0.0 0.0	0.00 0.00 0.00 1.00	0.00 0.00 0.00 1.00	0.00 0.00 0.00
1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 1,900.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,900.0 3,000.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 38.85 38.85 38.85	1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.5 2.2	0.0 .0 -0.7	0.00 0.00 1.00	0.00 0.00 1.00	0.00
1,487.5 Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 1,900.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,900.0 3,000.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	0.00 0.00 1.00 2.00 3.00 4.00	0.00 0.00 38.85 38.85 38.85	1,487.5 1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.0 0.7 2.7 6.1	0.0 0.0 0.5 2.2	0.0 .0 -0.7	0.00 0.00 1.00	0.00 0.00 1.00	0.00
Salado (Top Salt) 1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,000.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	0.00 1.00 2.00 3.00 4.00	0.00 38.85 38.85 38.85	1,500.0 1,600.0 1,700.0 1,799.9	0.0 0.7 2.7 6.1	0.0 0.5 2.2	0.0	0.00	0.00	0.00
1,500.0 Start Build 1.00 1,600.0 1,700.0 1,800.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,300.0 2,300.0 2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 2,800.0 3,000.0 3,000.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	1.00 2.00 3.00 4.00	38.85 38.85 38.85	1,600.0 1,700.0 1,799.9	0.7 2.7 6.1	0.5 2.2	-0.7	1.00	1.00	
1,600.0 1,700.0 1,800.0 2,000.0 2,100.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	2.00 3.00 4.00	38.85 38.85	1,700.0 1,799.9	2.7 6.1	2.2				0.00
1,700.0 1,800.0 1,900.0 2,000.0 2,100.0 2,200.0 2,300.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	2.00 3.00 4.00	38.85 38.85	1,700.0 1,799.9	2.7 6.1	2.2				0.00
1,800.0 1,900.0 2,000.0 2,100.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,100.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,500.0	3.00 4.00	38.85	1,799.9	6.1		-2.7	1.00		0.00
1,900.0 2,000.0 2,100.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0	4.00				4.0			1.00	0.00
2,000.0 2,100.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0		20.05			4.9	-6.1	1.00	1.00	0.00
2,000.0 2,100.0 2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,300.0 3,300.0 3,500.0		30.00	1,899.7	10.9	8.8	-10.8	1.00	1.00	0.00
2,100.0 2,200.0 2,300.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	5.00	38.85	1,999.4	17.0	13.7	-16.9	1.00	1.00	0.00
2,200.0 2,300.0 2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	6.00	38.85	2,098.9	24.4	19.7	-24.3	1.00	1.00	0.00
2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	7.00	38.85	2,198.3	33.3	26.8	-33.1	1.00	1.00	0.00
2,400.0 2,500.0 <b>Start 1984.5 hold at 2</b> 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	8.00	38.85	2,297.4	43.4	35.0	-43.2	1.00	1.00	0.00
2,500.0 Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	9.00	38.85	2,396.3	54.9	44.2	-54.7	1.00	1.00	0.00
Start 1984.5 hold at 2 2,600.0 2,700.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,300.0 3,400.0 3,500.0	10.00	38.85	2,494.9	67.8	54.6	-67.4	1.00	1.00	0.00
2,600.0 2,700.0 2,800.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0		00.00	2,404.0	07.0	01.0	07.1			0.00
2,700.0 2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0		38.85	2,593.4	81.3	65.5	-80.9	0.00	0.00	0.00
2,800.0 2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	10.00 10.00	38.85	2,593.4 2,691.9	94.8	76.4	-80.9 -94.4	0.00	0.00	0.00
2,900.0 3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	10.00	38.85	2,790.4	108.4	87.3	-107.8	0.00	0.00	0.00
3,000.0 3,100.0 3,200.0 3,300.0 3,400.0 3,500.0	10.00	38.85	2,888.9	121.9	98.2	-121.3	0.00	0.00	0.00
3,100.0 3,200.0 3,300.0 3,400.0 3,500.0		38.85	2,008.9	135.4	109.1	-121.3	0.00	0.00	0.00
3,200.0 3,300.0 3,400.0 3,500.0	10.00		,			-134.7	0.00	0.00	0.00
3,300.0 3,400.0 3,500.0	10.00	38.85	3,085.8	148.9	120.0				0.00
3,400.0 3,500.0	10.00	38.85	3,184.3	162.5	130.8	-161.6	0.00	0.00	
3,500.0	10.00	38.85	3,282.8	176.0	141.7	-175.1	0.00	0.00	0.00
	10.00	38.85	3,381.3	189.5	152.6	-188.5	0.00	0.00	0.00
0.000.0	10.00	38.85	3,479.7	203.0	163.5	-202.0	0.00	0.00	0.00
3,600.0	10.00	38.85	3,578.2	216.6	174.4	-215.5	0.00	0.00	0.00
	10.00	38.85	3,676.7	230.1	185.3	-228.9	0.00	0.00	0.00
	10.00	38.85	3,775.2	243.6	196.2	-242.4	0.00	0.00	0.00
3,900.0		38.85	3,873.7	257.1	207.1	-255.8	0.00	0.00	0.00
4,000.0	10.00	38.85	3,972.1	270.6	218.0	-269.3	0.00	0.00	0.00
	10.00 10.00	38.85	4,070.6	284.2	228.9	-282.7	0.00	0.00	0.00
4,126.3	10.00	38.85	4,096.5	287.7	231.7	-286.3	0.00	0.00	0.00
Base Salt									
4,156.7	10.00 10.00			291.8	235.1	-290.4	0.00	0.00	0.00
Bell Canyon	10.00 10.00 10.00	38.85	4,126.5						
4.200.0	10.00 10.00	38.85	4,126.5						0.00



ч.

## Planning Report

Database: Company: Project: Site: Nell: Nellbore:					TVD Re MD Re North I	Co-ordinate Ref eference: ference: Reference: / Calculation Me		Well Boros F KB @ 3252. KB @ 3252. Grid Minimum Cu	5usft	
Design:		BLM Plan #1						·		
Planned Sur	vey								· • · · ·	. ·
De	asured epth usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	4,300.0	10.00	38.85	4,267.6	311.2	250.7	-309.6	0.00	0.00	0.00
	4,400.0	10.00	38.85	4,366.1	324.7	261.6	-323.1	0.00	0.00	0.00
	4,484.5	10.00	38.85	4,449.3	336.2	270.8	-334.5	0.00	0.00	0.00
Sta	art Drop -1	.50				•				
	4,500.0	9.77	38.85	4,464.6	338.2	272.4	-336.5	1.50	-1.50	0.00
	4,600.0	8.27	38.85	4,563.3	350.4	282.3	-348.7	1.50	-1.50	0.00
	4,700.0	6.77	38.85	4,662.5	360.6	290.5	-358.8	1.50	-1.50	0.00
	4,800.0	5.27	38.85	4,761.9	368.8	297.0	-366.9	1.50	-1.50	0.00
	4,900.0	3.77	38.85	4,861.6	374.9	302.0	-373.0	1.50	-1.50	0.00
	5,000.0	2.27	38.85	4,961.4	379.0	305.3	-377.1	1.50	-1.50	0.00
	5,100.0	0.77	38.85	5,061.4	381.1	306.9	-379.2	1.50	-1.50	0.00
	5,151.2	0.00	0.00	5,112.6	381.4	307.2	-379,4	1.50	-1.50	0.00
Sta	art 5593.4	hold at 5151.2 N	1D							•
	5,200.0	0.00	0.00	5,161.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,217.1	0.00	0.00	5,178.5	381.4	307.2	-379.4	0.00	0.00	0.00
Ch	erry Cany	on								
	5,300.0	. 0.00	0.00	5,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,300.0	0.00	0.00	5,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,500.0	0.00	0.00	5,461.4	381.4	307.2	-379:4	0.00	0.00	0.00
	5,600.0	0.00	0.00	5,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,700.0	0.00	0.00	5,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,800.0	0.00	0.00	5,761.4	381.4	307.2	-379.4	0.00	0.00	0.00
	5,900.0	0.00	0.00	5,861.4	381.4	307.2	-379.4 -379.4	0.00 0,00	0.00 0.00	0.00
	6,000.0 6,100.0	0.00 0.00	0.00 0.00	5,961.4 6,061.4	381.4 381.4	307.2, 307.2	-379.4	0.00	0.00	0.00
	6,200.0	0.00	0.00	6,161.4	381.4	307.2	-379.4	0.00	0.00	0.00
						[				
	6,300.0	0.00	0.00	6,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,400.0	0.00	0.00	6,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,423.7	0.00	0.00	6,385.1	381.4	307.2	-379.4	0.00	0.00	0.00
Bru	ushy Cany								• • •	
	6,500.0	0.00	0.00	6,461.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,600.0	0.00	0.00	6,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,700.0	0.00	0.00	6,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,800.0	0.00	0.00	6,761.4	381.4	307.2	-379.4	0.00	0.00	0.00
	6,900.0	0.00	0.00	6,861.4	381.4	307.2	-379.4	0.00	0.00	. 0.00
	7,000.0	0.00	0.00	6,961.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,100.0	0.00	0.00	7,061.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,200.0	0.00	0.00	7,161.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,300.0	0.00	0.00	7,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,400.0	0.00	0.00	7,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,500.0	0.00	0.00	7,461.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,545.1	0.00	0.00	7,506.5	381.4	307.2	-379.4	0.00	0.00	0.00
L. I	Brushy Ca	anyon								۰,
	7,600.0	0.00	0.00	7,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,700.0	0.00	0.00	7,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,800.0	0.00	0.00	7,761.4	381.4	307.2	-379.4	0.00	0.00	0.00
	7,900.0	0.00	0.00	7,861.4	381.4	307.2	-379.4	0.00	0.00	0.00
	8,000.0	0.00	0.00	7,961.4	381.4	307.2	-379.4	0.00	0.00	0.00
		0.00	0.00	8,061.4	381.4	307.2	-379.4	0.00	0.00	0.00
	8,100.0 8,106.4	0.00	0.00	8,061.4	381.4	307.2	-379.4	0.00	0.00	0.00
		0.00	0.00	0,007.0		557.E	0,0.7	0.00	0.00	0.00
BS	GL	0.00	0.00	8 161 A	381.4	307.2	-379.4	0.00	0.00	0.00
	8,200.0 8,243.8	0.00 0.00	0.00 0.00	8,161.4 8,205.2	381.4 381.4	307.2	-379.4 -379.4	0.00	0.00	0.00

Page 4

COMPASS 5000.14 Build 83

-



111-										
		ED14 6000 44	Circle Uses Db	•	1 1			Mall Doros F	ederal #133H	
atabase:			Single User Db			Co-ordinate Ref	erence:			
ompany:			uction Company	,		eference:		KB @ 3252.		
roject:		Rustler Breaks	5			ference:		KB @ 3252,	Sust	
ite:		Boros				Reference:		Grid		
lell:		Boros Federal	#133H		Survey	y Calculation Mé	ethod:	Minimum Cu	rvature	
ellbore:		Wellbore #1								
esign:		BLM Plan #1	·.							
Planned Surve	у					. 6		· · ·	· · · · ·	
Measu	ured			Vertical			Vertical	Dogleg	Build	Turn
Dept		Inclination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate
(usf		(°)	· (°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
Avalo						1				
	300.0	0.00	0.00	8,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
84	400.0	0.00	0.00	8,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
,	500.0	0.00	0.00	8,461.4	381.4	307.2	-379.4	0.00	0.00	0.00
,	600.0	0.00	0.00	8,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
	700.0	0.00	0.00	8,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
	800.0	0.00	0.00	8,761.4	381.4	307.2	-379.4	0.00	0.00	0.00
,	900.0	0.00	0.00	8,861.4	381.4	307.2	-379.4	0.00	0.00	0.00
	000.0	0.00	0.00	8,961.4	381.4	307.2	-379.4	0.00	0.00	0.00
	100.0	0.00	0.00	9,061.4	381.4	307.2	-379.4	0.00	0.00	0.00
	200.0	0.00	0.00	9,161.4	381.4	307.2	-379.4	0.00	0.00	0.00
	250.8	0.00	0.00	9,212.2	381.4	307.2	-379.4	0.00	0.00	0.00
FBSG	;									
9,3	300.0	0.00	0.00	9,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
9,4	400.0	0.00	0.00	9,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
9,9	500.0	0.00	0.00	9,461.4	381.4	307.2	-379.4	0.00	0.00	0.00
9,9 SBSC	531.4	0.00	0.00	9,492.8	381.4	307.2	-379.4	0.00	0.00	0.00
	, 600.0	0.00	0.00	9,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
9,1	700.0	0.00	0.00	9,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
9,1 SBSG	785.4	0.00	0.00	9,746.8	381.4	307.2	-379.4	0.00	0.00	0.00
	9 800.0	0.00	0.00	9,761.4	381,4	307.2	-379.4	0.00	0.00	. 0.00
	900.0 000.0	0.00 0.00	0.00 0.00	9,861.4 9,961.4	381.4 381.4	307.2 307.2	-379.4 -379.4	0.00 0.00	0.00	0.00 0.00
	100.0	0.00	0.00	10,061.4	381.4	307.2	-379.4	0.00	0.00	0.00
	200.0	0.00	0.00	10,161.4	381.4	. 307.2	-379.4	0.00	0.00	0.00
	240.6	. 0.00	0.00	10,202.0	381.4	307.2	-379.4	0.00	0.00	. 0.00
TBSC										
10,3	300.0	0.00	0.00	10,261.4	381.4	307.2	-379.4	0.00	0.00	0.00
10,4	400.0	0.00	0.00	10,361.4	381.4	307.2	-379.4	0.00	0.00	0.00
10.5	500.0	0.00	0.00	10,461.4	381.4	307.2	-379.4	0.00	0.00	0.00
	600.0	0.00	0.00	10,561.4	381.4	307.2	-379.4	0.00	0.00	0.00
	700.0	0.00	0.00	10,661.4	381.4	307.2	-379.4	0.00	0.00	0.00
	744.6	0.00	0.00	10,706.0	381.4	307.2	-379.4	0.00	0.00	0.00
Start	Build 1	0.00 - VP - Boro	s Federal #133I	н						
	750.0	0.54	185.60	10,711.4	381.3	307.2	-379.4	10.00	10.00	0.00
	800.0	5.54	185.60	10,761.3	378.7	306.9	-376.8	10.00	10.00	0.00
	850.0	10.54	185.60	10,810.8	371.7	306.2	-369.8	10.00	10.00	0.00
	900.0	15.54	185.60	10,859.5	360.5	305.1	-358.6	10.00	10.00	0.00
,	950.0	20.54	185.60	10,907.0	345.1	303.6	-343.2	10.00	10.00	0.00
11,0	000.0	25.54	185.60	10,953.0	325.6	301.7	-323.7	10.00	10.00	0.00
	013.7	26.91	185.60	10,965.3	319.6	301.1	-317.7	10.00	10.00	0.00
TBSG								10.0-	40.00	
	050.0	30.54	185.60	10,997.1	302.3	299.4	-300.4	10.00	10.00	0.00
	100.0	35.54	185.60	11,039.0	275.1	296.7	-273.3	10.00	10.00	0.00
	150.0	40.54	185.60	11,078.4	244.5	293.7	-242.6	10.00	10.00	0.00
11,3	200.0	45.54	185.60	11,114.9	210.5	290.4	-208.7	10.00	10.00	0.00

11,250.0 11,300.0

11,350.0

11,400.0

11,450.0

50.54

55.54

60.54

65.54

70.54

185.60

185.60

185.60

185.60

185.60

173.5

133.8

91.6

47.2

1.1

286.8

282.9

278.7

274.4

269.9

-171.7

-132.0

-89.8

-45.5

0.6

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

11,148.4

11,178.4

11,204.9

11,227.5

11,246.2

COMPASS 5000.14 Build 83

0.00

0.00

0.00

0.00\*

0.00



Database: Company: Project: Site: Well:	Matador Pro Rustler Brea Boros Boros Fede	ral #133H		TVD Re MD Re North I	Co-ordinate Re eference: ference: Reference: r Calculation M		Well Boros F KB @ 3252. KB @ 3252. Grid Minimum Cu	5usft	•
Wellbore: Design:	Wellbore #1 BLM Plan #								
Planned Survey				- ,	•	8			
Measur	red		Vertical			Vertical	Dogleg	Build	Turn
Depth (usft)		Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Section (usft)	Rate (°/100usft)	Rate (°/100usft)	Rate (°/100usft)
11,5	00.0 75.54	185.60	11,260.8	-46.5	265.2	48.1	10.00	10.00	0.00
	50.0 80.54		11,271.2	-95.1	260.4	96.8	10.00	10.00	0.00
	00.0 85.54		11,277.2	-144.5	255.6	146.1	10.00	10.00	0.00
11,6		5 185.60	11,278.6	-168.4	253.3	170.0	10.00	10.00	0.00
L. TBS					•				
	44.6 90.00		11,279.0	-188.9	251.2	190.4	10.00	10.00	0.00
Start D	OLS 2.00 TFO -90.00								
11,7	00.0 90.00	184.49	11,279.0	-244.0	246.4	245.6	2.00	0.00	-2.00
	00.0 90.00		11,279.0	-343.9	240.3	345.4	2.00	0.00	-2.00
11,9	00,0 90.00	0 180.49	11,279.0	-443.8	237.7	445.3	2.00	0.00	-2.00
11,9	42.7 90.00	) 179.64	11,279.0	-486.5	237.6	488.0	2.00	0.00	-2.00
Start 9	644.6 hold at 11942	.7 MD							
12,0	00.0 90.00	0 179.64	11,279.0	-543.8	238.0	545.3	0.00	0.00	0.00
12.1	00.0 90.00	0 179.64	11,279.0	-643.8	238.6	645.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-743.8	239.3	745.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-843.8	239.9	845.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-943.8	240.5	945.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-1,043.8	241.2	1,045.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-1,143.8	241.8	1,145.3	0.00	0.00	0.00
•	00.0 90.00		11,279.0	-1,243.8	242.4	1,245.3	0.00	0.00	0.00
	90.00		11,279.0	-1,343.8	243.1	1,345.3	0.00	0.00	0.00
	00.0 90.00 00.0 90.00		11,279.0 11,279.0	-1,443.8 -1,543.8	243.7 244.3	1,445.3 1,545.3	0.00 0.00	0.00 0.00	0.00
13,0				-1,045.0					
	00.0 90.00		11,279.0	-1,643.8	245.0	1,645.3	0.00	0.00	0.00
- 13,2			11,279.0	-1,743:8	245.6	1,745.3	0.00	0.00	0.00
	90.00		11,279.0	-1,843.8	246.2	1,845.3	0.00	0.00	0.00
	90.00		11,279.0	-1,943.8	246.9	1,945.3	0.00	0.00	0.00
13,5	60.0 90.00	0 179.64	11,279.0	-2,043.8	247.5	2,045.3	0.00	0.00	0.00
13,6	00.0 90.00	0 179.64	11,279.0	-2,143.8	248.1	2,145.3	0.00	0.00 ·	0.00
13,7	00.0 90.00	0 179.64	11,279.0	-2,243.8	248.7	2,245.3	- 0.00	0.00	0.00
13,8	00.0 90.00	0 179.64	11,279.0	-2,343.8	249.4	2,345.3	0.00	0.00	0.00
13,9	90.00		11,279.0	-2,443.8	250.0	2,445.3	0.00	0.00	0.00
14,0	00.0 90.00	D 179.64	11,279.0	-2,543.8	250.6	2,545.3	0.00	0.00	0.00
14 1	00.0 90.00	179.64	11,279.0	-2,643.8	251.3	2,645.3	0.00	0.00	0.00
	200.0 90.00		11,279.0	-2,743.8	251.9	2,745.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-2,843.8	252.5	2,845.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-2,943.8	253.2	2,945.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-3,043.8	253.8	3,045.3	0.00	0.00	0.00
14 6	00.0 90.00	0 179.64	11,279.0	-3,143.8	254.4	3,145.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-3,143.8	254.4	3,145.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-3,343.8	255.7	3,345.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-3,443.8	256.3	3,445.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-3,543.8	257.0	3,545.3	0.00	0.00	0.00
,							0.00	0.00	0.00
	00.0 90.00 200.0 90.00		11,279.0 11,279.0	-3,643.8 -3,743.7	257.6 258.2	3,645.3 3,745.3	0.00	0.00	0.00
					258.2 258.9	3,745.3	0.00	0.00	0.00
	00.0 90.00 00.0 90.00		11,279.0 11,279.0	-3,843.7 -3,943.7	258.9	3,845.3 3,945.3	0.00	0.00	0.00
			11,279.0	-3,943.7 -4,043.7	259.5	4,045.3	0.00	0.00	0.00
15,5									
15,6	90.00		11,279.0	-4,143.7	260.8	4,145.3	0.00	0.00	0.00
	00.0 90.00		11,279.0	-4,243.7	261.4	4,245.3	0.00	0.00	0.00
15,8	90.00 90.00		11,279.0	-4,343.7	262.0	4,345.3	0.00	0.00	0.00
15,9	00.0 90.00		11,279.0	-4,443.7	262.7	4,445.3	0.00	0.00	0.00 0.00
	00.0 90.00	D 179.64	11,279.0	-4,543.7	263.3	4,545.3	0.00	0.00	

Page 6



Database: Company: Project: Site: Well:		EDM 5000.14 Matador Produ Rustler Breaks Boros Boros Federal	ction Company		TVD Re MD Re North I	Co-ordinate Re eference: ference: Reference: Calculation M		Well Boros F KB @ 3252. KB @ 3252. Grid Minimum Cu	5usft		
Wellbore: Design:		Wellbore #1 BLM Plan #1		·		1					
Planned Survey	y					· · · ·		-			
Measu Depti (usft	'n	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	
	100.0	90.00	179.64	11,279.0	-4,643.7	263.9	4,645.3	0.00	0.00	0.00	
-	200.0	90.00	179.64	11,279.0	-4,743.7	264.6	4,745.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-4,843.7	265.2	4,845.3	0.00	0.00	0.00	
	400.0	90.00	179.64	11,279.0	-4,943.7	265.8	4,945.3	0.00	0.00	0.00	
16,5	500.0	90.00	179.64	11,279.0	-5,043.7	266.5	5,045.3	0.00	0.00	0.00	
16,6	500.0	90.00	179.64	11,279.0	-5,143.7	267.1	5,145.3	0.00	0.00	0.00	
	700.0	90.00	179.64	11,279.0	-5,243.7	267.7	5,245.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-5,343.7	268.4	5,345.3	0.00	0.00	0.00	
16,9	900.0	90.00	179.64	11,279.0	-5,443.7	269.0	5,445.3	0.00	0.00	0.00	
,	0.000	90.00	179.64	11,279.0	-5,543.7	269.6	5,545.3	0.00	0.00	0.00	
		90.00	179.64		-5,643.7					•	
	100:0			11,279.0	,	270.2	5,645.3	0.00	× 0.00	0.00	
	200.0	90.00 90.00	179.64	11,279.0 11,279.0	-5,743.7	270.9	5,745.3	0.00	0.00	0.00	
	300.0		179.64	11,279.0	-5,843.7	271.5	5,845.3	0.00	0.00	0.00	
	400.0 500.0	90.00 90.00	179.64 179.64	11,279.0 11,279.0	-5,943.7 -6,043.7	272.1 272.8	5,945.3 6,045.3	0.00 0.00	0.00 0.00	0.00 0.00	
17,5	00.0	90.00	179.04	11,279.0	-0,043.7	272.0	0,045.5	0.00	0.00	0.00	
	600.0	90.00	179.64	11,279.0	-6,143.7	273.4	6,145.3	0.00	0.00	0.00	
	700.0	90.00	179.64	11,279.0	-6,243.7	274.0	6,245.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-6,343.7	274.7	6,345.3	0.00	0.00	0.00	
17,9	900.0	90.00	179.64	11,279.0	-6,443.7	275.3	6,445.3	0.00	0.00	0.00	
18,0	0.000	90.00	179.64	11,279.0	-6,543.7	275.9	6,545.3	0.00	0.00	0.00	
18.1	100.0	90.00	179.64	11,279.0	-6,643.7	276.6	6,645.3	0.00	0.00	0.00	
	200.0	90.00	179.64	11,279.0	-6,743.7	277.2	6,745.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-6,843.7	277.8	6,845.3	0.00	0.00	0.00	
	400.0	90.00	179.64	11,279.0	-6,943.7	278.5	6,945.3	0.00	0.00	0.00	
	500.0	90.00	179.64	11,279.0	-7,043.7	279.1	7,045.3	0.00	0.00	0.00	
						"					
,	500.0	90.00	179.64	11,279.0	-7,143.7	279.7	7,145.3	0.00	0.00	0.00	
	700.0	90.00	179.64	11,279.0	-7,243.7	280.4	7,245.3	0.00	0.00	0.00	
· ·	300.0	90.00	179.64	11,279.0	-7,343.7	281.0	7,345.3	0.00	0.00	0.00	
	900.0	90.00	179.64	11,279.0	-7,443.7	281.6	7,445.3	0.00	0.00	0.00	
19,0	0.000	90.00	179.64	11,279.0	-7,543.7	282.3	7,545.3	0.00	0.00	0.00	
19,1	100.0	90.00	179.64	11,279.0	-7,643.7	282.9	7,645.3	0.00	0.00	0.00	
19,2	200.0	90.00	179.64	11,279.0	-7,743.7	283.5	7,745.3	0.00	0.00	0.00	
19,3	300.0	90.00	179.64	11,279.0	-7,843.7	284.2	7,845.3	0.00	0.00	0.00	
	400.0	90.00	179.64	11,279.0	-7,943.7	284.8	7,945.3	0.00	0.00	0.00	
19,5	500.0	90.00	179.64	11,279.0	-8,043.7	285.4	8,045.3	0.00	0.00	0.00	
10 6	500.0	90.00	179.64	11,279.0	-8.143.7	286.1	8,145.3	0.00	0.00	0.00	
,	700.0	90.00	179.64	11,279.0	-8,243.7	286.7	8,245.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-8,343.7	287.3	8,345.3	0.00	0.00	0.00	
	900.0	90.00	179.64	11,279.0	-8,443.7	288.0	8,445.3	0.00	0.00	0.00	
	0.000	90.00	179.64	11,279.0	-8,543.7	288.6	8,545.3	0.00	0.00	0.00	
	100.0	90.00	179.64	11,279.0	-8,643.7	289.2	8,645.3	0.00	0.00	0.00	
	200.0	90.00	179.64	11,279.0	-8,743.6	289.9	8,745.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-8,843.6	290.5	8,845.3	0.00	0.00	0.00	
	400.0	90.00	179.64	11,279.0	-8,943.6	291.1	8,945.3	0.00	0.00	0.00	
20,5	500.0	90.00	179.64	11,279.0	-9,043.6	291.8	9,045.3	0.00	0.00	0.00	
20.6	600.0	90.00	179.64	11,279.0	-9,143.6	292.4	9,145.3	0.00	0.00	0.00	
	700.0	90.00	179.64	11,279.0	-9,243.6	293.0	9,245.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-9,343.6	293.6	9,345.3	0.00	0.00	0.00	
	900.0	90.00	179.64	11,279.0	-9,443.6	294.3	9,445.3	0.00	0.00	0.00	
	0.000	90.00	179.64	11,279.0	-9,543.6	294.9	9,545.3	0.00	0.00	0.00	
						1					
	100.0	90.00	179.64	11,279.0	-9,643.6	295.5	9,645.3	0.00	0.00	0.00	
	200.0	90.00	179.64	11,279.0	-9,743.6	296.2	9,745.3	0.00	0.00	0.00	
	300.0	90.00	179.64	11,279.0	-9,843.6	296.8	9,845.3	0.00	0.00	0.00	
	400.0	90.00	179.64	11,279.0	-9,943.6	297.4	9,945.3	0.00	0.00	0.00	

<b>//</b> *

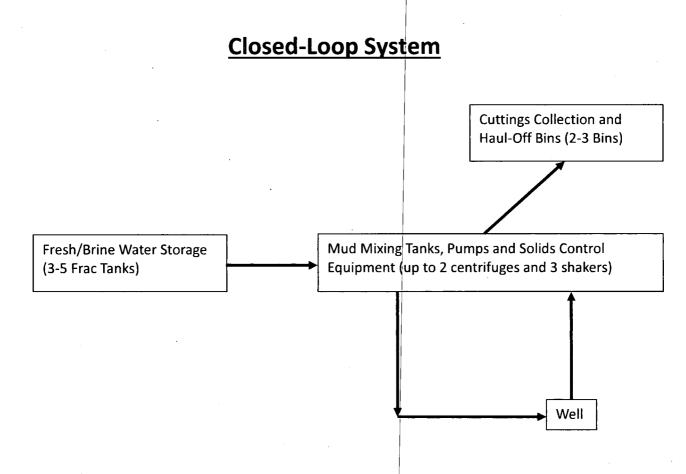
.

Database: Company: Project: Site: Well: Wellbore: Design:	Mat Rus Bor Bor Wel	ador Produ tler Breaks				TVD Refe MD Refe North Re	rence:		Well Boros F KB @ 3252. KB @ 3252. Grid Minimum Cu	•	
Planned Survey									·	· · · · · · · · · · · · · · · · · · ·	
Measur Depti (usft)	red h incl	ination (°)	Azimuth (°)	Vertical Depth (usft)		+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate {°/100usft)
21,5	500.0	90.00	179.6	4 11,27	9.0	-10,043.6	298.1 <sup>°</sup>	10,045.3	0.00	0.00	0.00
	587.3 <b>21587.3 - B</b> H	90.00 I <b>L - Boros</b> I	179.6 Federal #13	•	'9.0	-10,130.9	298.6	10,132.6	0.00	0.00	0.00
Design Targets			•					·			
Target Name - hit/miss tar - Shape	rget Di	p Angle (°)	Dip Dir. (°)	TVD (usît)	+N/-S (usft)	+E/-W (usft)	Northin (usft)	g I	Easting (usft)	Latitude	Longitude
/P - Boros Fede	eral #131		0.00	10 706 0	381	14 307 2	> 3823	36.00	676 677 00	32° 2' 59 547 N	103° 45' 47 135 V
- plan hits ta - Point	arget center deral #13	0.00	0.00	10,706.0 11,279.0	381 -10,130	·		36.00 22.91	676,677.00 676,668.50	32° 2' 59.547 N 32° 1' 15.507 N	
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #13	0.00				·					
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #13	0.00 0.00 Ver De				·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Feo - plan hits ta - Point	arget center deral #15 arget center 	0.00 0.00 Ver De	0.00 rtical epth	11,279.0	-10,130	·			676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Feo - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft)	0.00 0.00 Ver De (u 2	0.00 rtical apth isft) 1,356.2 R	11,279.0	-10,130	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Feo - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356	0.00 0.00 Ver De (u 2 5	0.00 rtical epth isft) 1,356.2 R 1,487.5 S	11,279.0	-10,130	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487.	0.00 0.00 Ver De (u 2 5 3	0.00 rtical epth sft) 1,356.2 R 1,487.5 S 4,096.5 B	11,279.0 ustler alado (Top Sal	-10,130	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	Arget center deral #15 arget center Measured Depth (usft) 1,356 1,487 4,126	0.00 0.00 Ver De (u 2 5 3 7	0.00 rtical epth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi	11,279.0 ustler alado (Top Sal ase Salt	-10,130	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Fec - plan hits ta - Point	Measured Depth (usft) 1,356 1,487 4,126 4,156	0.00 0.00 Ver De (u 2 5 3 7 1	0.00 rtical apth isft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C	11,279.0 ustler alado (Top Sal ase Salt ell Canyon	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106.	0.00 0.00 Ver De {u 2 5 3 7 1 7 1 4	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyo SGL	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point 3HL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 A	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243. 9,250.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8 8	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 Ai 9,212.2 Fi	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS BSG	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243. 9,250. 9,531.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8 8 4	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 Ai 9,212.2 Fi 9,492.8 Si	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS BSG BSC	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243. 9,250. 9,531. 9,785.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8 8 4 4	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 Ai 9,212.2 Fi 9,492.8 Si 9,746.8 Si	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS BSG BSC BSG	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- plan hits ta - Point BHL - Boros Fec - plan hits ta - Point	arget center deral #1: arget center (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243. 9,250. 9,531. 9,785. 10,240.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8 8 4 4 4 6 1	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 Ai 9,212.2 Fi 9,492.8 Si 9,746.8 Si 0,202.0 Ti	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS BSG BSC BSG BSC BSC	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V
- Point BHL - Boros Feo - plan hits ta	arget center deral #1: arget center Measured Depth (usft) 1,356. 1,487. 4,126. 4,156. 5,217. 6,423. 7,545. 8,106. 8,243. 9,250. 9,531. 9,785.	0.00 0.00 Ver De (u 2 5 3 7 1 7 1 4 8 8 4 4 4 6 1 7 1 1 7	0.00 tical pth sft) 1,356.2 R 1,487.5 Si 4,096.5 Bi 4,126.5 Bi 5,178.5 C 6,385.1 Bi 7,506.5 L 8,067.8 Bi 8,205.2 Ai 9,212.2 Fi 9,492.8 Si 9,746.8 Si	11,279.0 ustler alado (Top Sal ase Salt ell Canyon herry Canyon rushy Canyon Brushy Canyon SGL valon-SS BSG BSC BSG BSC BSG BSC BSG	-10,130 Name	·		22.91	676,668.50	32° 1' 15.507 N Dip Direction	103° 45' 47.878 V

tador

	·		E I	· · · · · · · · · · · · · · · · · · ·	
Database:	EDM 5000.14 Single User Db	Local Co	o-ordinate Reference:	Well Boros Federal #133H	
Company:	Matador Production Company	TVD Ref	erence:	KB @ 3252.5usft	
Project:	Rustler Breaks	MD Refe	rence:	KB @ 3252.5usft	
Site:	Boros	. North Re	eference:	Grid	
Well:	Boros Federal #133H	Survey (	Calculation Method:	Minimum Curvature	
Wellbore:	Wellbore #1				
Design:	BLM Plan #1				~
Plan Annotations	3		2	· · · ·	
	Measured Vertical	Local Coordinates	T		

	Measured	Vertical	Local Coordinates		
	Depth	Depth	+N/-S	+E/-W	
	(usft)	(usft)	(usft)	(usft)	Comment
	1,500.0	1,500.0	0.0	0.0	Start Build 1.00
	2,500.0	2,494.9	67.8	54.6	Start 1984.5 hold at 2500.0 MD
	4,484.5	4,449.3	336.2	270.8	Start Drop -1.50
	5,151.2	5,112.6	381.4	307.2	Start 5593.4 hold at 5151.2 MD
	10,744.6	10,706.0	381.4	307.2	Start Build 10.00
	11,644.6	11,279.0	-188.9	251.2	Start DLS 2.00 TFO -90.00
	11,942.7	11,279.0	-486.5	237.6	Start 9644.6 hold at 11942.7 MD
	21,587.3	11,279.0	-10,130.9	298.6	TD at 21587.3
L					



## **Operating and Maintenance Plan:**

During drilling operations, third party service companies will utilize solids control equipment to remove cuttings from the drilling fluids and collect it in haul-off bins. Equipment will be closely monitored at all times while drilling by the derrick man and the service company employees.

## **Closure Plan:**

During drilling operations, third party service companies will haul off drill solids and fluids to an approved disposal facility. At the end of the well, all closed loop equipment will be removed from the location.

Boros Federal #133H SHL: 430' FNL & 2213' FEL Section 15 BHL: 100' FSL & 1980' FEL Section 22 Township/Range: 26S 31E Elevation Above Sea Level: 3,224'

## **Drilling Operation Plan**

Proposed Drilling Depth: 21587' MD / 11279' TVD

Type of well: Horizontal well, no pilot hole

Permitted Well Type: Oil

Geologic Name of Surface Formation: Quaternary Deposits

KOP Lat/Long (NAD83): 32.0499991022 N / -103.7635674453 W TD Lat/Long (NAD83): 32.0210995208 N / -103.7637728498 W

#### 1. Estimated Tops

Formation	MD (ft)	TVD (ft)	Thickness (ft)	Lithology	Resource
Rustler	1,356	1,356	132	Anhydrite	Barren
Top of Salt	1,488	1,488	1,903	Salt	Barren
Castile	3,391	3,391	706	Salt	Barren
Base of Salt	4,097	4,097	29	Salt	Barren
Bell Canyon	4,126	4,126	1,053	Sandstone	Oil/Natural Gas
Cherry Canyon	5,179	5,179	1,206	Sandstone	Oil/Natural Gas
Brushy Canyon	6,385	6,385	1,683	Sandstone	Oil/Natural Gas
Bone Spring Lime	8,068	8,068	1,144	Limestone	Oil/Natural Gas
1st Bone Spring Sand	9,212	9,212	280	Sandstone	Oil/Natural Gas
2nd Bone Spring Carbonate	9,492	9,492	254	Carbonate	Oil/Natural Gas
2nd Bone Spring Sand	9,746	9,746	456	Sandstone	Oil/Natural Gas
3rd Bone Spring Carbonate	10,202	10,202	504	Carbonate	Oil/Natural Gas
КОР	10,744	10,706		Carbonate	Oil/Natural Gas
3rd Bone Spring Sand	11,013	10,965		Sandstone	Oil/Natural Gas
TD	21,587	11,279		Sandstone	Oil/Natural Gas

## 2. Notable Zones

3rd Bone Spring is the goal. All perforations will be within the setback requirements as prescribed or permitted by the New Mexico Oil Conservation Division. OSE estimated ground water depth at this location is 230'.

#### 3. Pressure Control

Equipment

A 12,000' 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and one annular preventer will be utilized below surface casing to TD. See attachments for BOP and choke manifold diagrams.

An accumulator complying with Onshore Order #2 requirements for the pressure rating of the BOP stack will be present. A rotating head will also be installed as needed.

#### **Testing Procedure**

## **Matador Production Company**

BOP will be inspected and operated as required in Onshore Order #2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position.

A third party company will test the BOPs.

After setting surface casing, a minimum 5M BOPE system will be installed. Test pressures will be 250 psi low and 5000 psi high with the annular preventer being tested to 250 psi low and 2500 psi high before drilling below surface shoe. In the event that the rig drills multiple wells on the pad and any seal subject to test pressures are broken, a full BOP test will be performed when the rig returns and the 5M BOPE system is re-installed.

#### Variance Request

Matador requests a variance to have the option of running a multi-bowl wellhead assembly for setting the Intermediate 1 and Production Strings. The BOPs will not be tested again unless any flanges are separated.

Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. The hose is not required by the manufacturer to be anchored. If the specific hose is not available, then one of equal or higher rating will be used.

Matador requests a variance to have the option of batch drilling this well with other wells on the same pad. In the event that this well is batch drilled, the wellbore will be secured with a blind flange of like pressure. When the rig returns to this well and BOPs are installed, the operator will perform a full BOP test.

#### 4. Casing & Cement

String	Hole Size (in)	Set MD (ft)	Set TVD (ft)	Casing Size (in)	Wt. (lb/ft)	Grade	Joint	Collapse	Burst	Tension
Surface	17.5	0 - 1381	0 - 1381	13.375	54.5	J-55	BUTT	1.125	1.125	1.8
Intermediate 1	12.25	0 - 4151	0 - 4151	9.625	40	J-55	BUTT	1.125	1.125	1.8
Production	8.75	0 - 21587	0 - 11279	5.5	20	P-110	DWC/C-IS HT Plus	1.125	1.125	1.8

All casing will be API and new. See attached casing assumption worksheet.

- All casing strings will be tested in accordance with Onshore Order #2 - III.B.1.h

- Rustler top will be validated via drilling parameters (i.e. reduction in ROP) and surface casing setting depth revised accordingly if needed

String	Туре	Sacks	Yield	Cu. Ft.	Weight	Percent Excess	Top of Cement	Class	Blend
. Surface	Lead	700	1.72	1198	12.5	50%	0	С	5% NaCI + LCM
Surface	Tail	250	1.38	347	14.8	50%	1081	С	5% NaCI + LCM
Intermediate 1	Lead	780	2.13	1663	12.6	50%	.0	С	Bentonite + 1% CaCL2 + 8% NaCl + LCM
	Tail	310	1.38	424	14.8	50%	3321	С	5% NaCI + LCM
Draduction	Lead	890	2.22	1976	11.5	25%	3951	. н	Fluid Loss + Dispersant + Retarder + LCM
Production	Tail	2660	1.35	3592	13.2	25%	10244	н	Fluid Loss + Dispersant + Retarder + LCM

#### 5. Mud Program

## **Matador Production Company**

An electronic Pason mud monitoring system complying with Onshore Order 2 will be used. All necessary mud products (barite, bentonite, LCM) for weight addition and fluid loss control will be on location at all times. Mud program is subject to change due to hole conditions.

Hole Section	Hole Size (in)	Mud Type	Interval MD (ft)	Density (lb/gal)	Viscosity	Fluid Loss
Surface	17.5	Spud Mud	0 - 1381	8.4 - 8.8	28-30	NC
Intermediate 1	12.25	Brine Water	1381 - 4151	9.5 - 10.2	28-30	NC
Production	8.75	FW/Cut Brine	4151 - 21587	8.6 - 9.4	28-30	NC

## 6. Cores, Test, & Logs

No core or drill stem test is planned.

A 2-person mud logging program will be used from Kick-off point to TD.

No electric logs are planned at this time. GR will be collected through the MWD tools from Intermediate casing to TD. CBL with CCL will be run as far as gravity will let it fall to top of curve.

## 7. Down Hole Conditions

No abnormal pressure or temperature is expected. Maximum anticipated surface pressure is 3032 psi. Expected bottom hole temperature is 186° F.

In accordance with Onshore Order 6, Matador does not anticipate that there will be enough H2S from the surface to the Bone Spring formations to meet the BLM's minimum requirements for the submission of a "H2S Drilling Operation Plan" or "Public Protection Plan" for the drilling and completion of this well. Since we have a H2S safety package on all wells, attached is a "H2S Drilling Operations Plan." Adequate flare lines will be installed off the mud/gas separator where gas may be flared safely. All personnel will be familiar with all aspects of safe operation of the equipment being used.

## **Matador Production Company**

# Hydrogen Sulfide Drilling Operations Plan Matador Resources

1 H2S safety instructions to the following:

- Characteristics of H2S
- Physical effects and hazards
- Principal and operation of H2S detectors, warning system and briefing areas
- Evacuation procedures, routes and first aid
- Proper use of safety equipment & life support systems
- Essential personnel meeting medical evaluation criteria will receive additional training on the proper use of 30min pressure demand air packs

2 H2S Detection and Alarm Systems:

- H2S sensor/detectors to be located on the drilling rig floor, in the base of the sub structure / cellar area, on the mud pits in the shale shaker area. Additional H2S detectors may be placed as deemed necessary
- An audio alarm system will be installed on the derrick floor and in the doghouse

3 Windsocks and / Wind Streamers:

- Windsocks at mud pit area should be high enough to be visible
- Windsock on the rig floor and / top of doghouse should be high enough to be visible

4 Condition Flags and Signs:

- Warning sign on access road to location
- Flags to be displayed on sign at entrance to location
  - Green Flag Normal Safe Operation Condition
  - Yellow Flag Potential Pressure and Danger
  - Red Flag Danger (H2S present in dangerous concentrations) Only H2S trained personnel admitted on location

5 Well Control Equipment:

• See Exhibit E-1

6 Communication:

- While working under masks chalkboards will be used for communications
- Hand signals will be used where chalk board is inappropriate
- Two way radio will be used to communicate off location in case of emergency help is required. In most cases cellular telephones will be available at most drilling foreman's trailer or living quarters.

1

7 Drilling Stem Testing:

• No DST cores are planned at this time

8 Drilling contractor supervisor will be required to be familiar with the effects H2S has on tubulars good and other mechanical equipment

9 If H2S is encountered, mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H2S scavengers if necessary

11 Emergency Contacts

• See exhibit E-6

۵

#### MRC ENERGY CO.'S

## HYDROGEN SULFIDE CONTINGENCY PLAN Drilling, Testing, & Completion

# MRC ENERGY CO.

#### Reviewers

------ Operations Manager ----- Operations Supt. ------ Staff RES ------ Field Supt. Blake Hermes---Engineering

H2S Contingency Plan #0165

**Revision#**0

This H2S Contingency Plan is subject to updating

Effective date: July 8, 2015

MRC ENERGY CO.'S

## TABLE OF CONTENTS

1.	INTRODUCTION	3			
II.	PURPOSE	4			
	A. Operating Procedures	5			
	B. Procedures to be Initiated Prior to reaching	6			
	H2S Contingency Plan Compliance				
	C. Drilling Below Contingency Plan Depth	• 7			
	D. Procedures program	7			
III.	<b>CONDITIONS &amp; H2S EMERGENCY PROCEDURES</b>	10			
	A. Definition of Operational "Conditions"	10			
	B. H2S Emergency Procedures; In Scope Personnel	12			
	C. Instructions for Igniting the Well	16			
	D. Coring	17			
	E. Normal Operations	18			
IV.	SAFETY EQUIPMENT	21			
V.	TOXICITY OF VARIOUS GASES	23			
VI.	PROPERTIES OF GASES				
VII.	TREATMENT PROCEDURES FOR H2S POISONING				
VIII.	BREATHING AIR EQUIPMENT DRILLS ON/OFF DUTY	26			
IX.	HYDROGEN SULFIDE TRAINING CURRICULUM	27			
Х.	FIT TEST	29			
XI.	H2S EQUIPMENT LIST	30			
XII.	EMERGENCY PHONE NUMBERS	32			
XIII.	EVACUATION OF GENERAL PUBLIC	37			
XIV.	SEPCO EMERGENCY PHONE NUMBERS AND DIRECTIONS TO WELL SITE	38			
XV.	ROE MAP (RADIUS OF EXPOSURE)				
XVI.	. RESIDENCE LIST WITHIN ROE				

## INTRODUCTION

The H2S equipment will be rigged up 2 days prior to reaching a potential H2S containing zone. Drilling into any potential H2S zone shall not commence until the on-site MRC Drilling Supervisor has confirmed this plan in place.

The onsite Drilling Foreman will give Total Safety one week (7 days) notice to prepare for rig up of H2S equipment)

To be effective, the plan requires the cooperation and effort of each person participating in the drilling of an  $H_2S$  well. Each person must know his/her responsibilities and all emergency and safety procedures. He/she should thoroughly understand and be able to use with accuracy, all safety equipment while performing his/her normal duties, if the circumstance should arise. He/she should therefore familiarize himself/herself with the location of all safety equipment and check to see that it is properly stored, easily accessible at all times, and routinely maintained.

It is the intention of MRC ENERGY CO. and the Drilling Contractor to make every effort to provide adequate safeguards against harm to persons on the rig and in the immediate vicinity from the effects of hydrogen sulfide, which may be released into the atmosphere under emergency conditions. However, the initiative rests with the individual in utilizing the safeguards provided. The ideas and suggestions of the individuals involved in the drilling of this well are highly welcomed and act as a fundamental tool for providing the safest working conditions possible.

The drilling representative is required to enforce these procedures. They are set up for your safety and the safety of all others.

## II. PURPOSE

It is MRC Energy Co.'s intent to provide a safe working place, not only for its employees, but also for other contractors who are aiding in the drilling of this well. The safety of the general public is of utmost concern. All precautions will be taken to keep a safe working environment and protect the public. MRC ENERGY CO.'S

There is a possibility of encountering toxic hydrogen sulfide gas. Safety procedures must be adhered to in order to protect all personnel connected with the operations as well as people living within the area.

The MRC Energy Co. representative will enforce all aspects of the H2S Contingency Plan. This job will become easier by a careful study of the following pages and training and informing all personnel that will be working on the responsibilities.

#### A. OPERATING PROCEDURES

#### **DEFINITIONS:**

For purpose of this plan, on-site personnel shall be referred to as "In Scope Personnel" or "Out of Scope Personnel", per the following definitions:

J

In Scope Personnel – Personnel who will be working or otherwise present in potential H2S release areas, including the rig floor, cellar, pits, and shaker areas.

**Out of Scope Personnel** – Personnel who will not be working or Otherwise present in potential H2S areas. Such personnel include rig Site visitor, delivery and camp services personnel.

## **GENERAL:**

Before this  $H_2S$  contingency plan becomes operational, all regularly assigned In Scope Personnel (primarily the MRC, drilling contractor, and certain service personnel,) shall be thoroughly trained in the use of breathing equipment, emergency procedures, and responsibilities. Total Safety Technician or a designee assigned by the MRC Drilling Foreman shall keep a list of all personnel who have been through the on-site  $H_2S$ training program at the drill site.

All In Scope Personnel shall be given H2S training and the steps to be taken during H2S conditions under which the well may be drilled. General information will be explained about toxic gases, as well as the physiological effects of  $H_2S$  and the various classified operating conditions. In addition, the reader will be informed his/her general responsibility concerning safety equipment and emergency procedures.

The Total Safety H<sub>2</sub>S Safety Technician or MRC on-site RSE Technician shall make available the H2S Contingency Plan for all personnel to review.

Without exception, all personnel that arrive on location must proceed directly to and sign-in with the on-site MRC RSE Technician. In Scope Personnel will be required to complete an on-site H2S training and respirator fit testing before starting work, or produce evidence that they have received equivalent training. Out of Scope Personnel will be required to complete a site H2S awareness and general safety briefing. This briefing will consist of a H2S hazard overview, alarm review and required response to alarms.

## B. PROCEDURES TO BE INITIATED PRIOR TO H2S CONTINGENCY PLAN COMPLIANCE:

A list of emergency phone numbers and contacts will be on location and posted at the following locations:

- 1. MRC ENERGY CO.'S Representative's Office
- 2. Drilling Contractor's, Toolpusher Office
- 3. Living Quarters Area

All safety equipment and  $H_2S$  related hardware must be set up as required by MRC Energy Co. with regard to location of briefing areas, breathing equipment, etc. All safety equipment must be inspected periodically (at least weekly) with particular attention to equipment.

In Scope Personnel working in the well site area will be assigned breathing apparatus. Operator and drilling contractor personnel required to work in the following areas will be provided with Self Contained Breathing Apparatus:

- 1. Rig Floor
- 2. Mud Pits
- 3. Derrick
- 4. Shale Shaker
- 5. Cellar

The Total Safety  $H_2S$  Safety Technician will be responsible for rigging up all  $H_2S$  continuous monitoring-type detectors. The Total Safety Technician will monitor and bump test the detector units periodically (at least at least once a week to test alarm function during drilling conditions. In the event  $H_2S$  is detected, or when drilling in a zone confirmed to contain  $H_2S$ , the units shall be bump tested at least once every 24 hours. A bump test/calibration log will be kept on location. All results will be reported to the MRC on-site Drilling Foreman.

All Total Safety H2S equipment will be maintained and inspected by a Total Safety Technician on at least a Weekly basis.

## C. DRILLING BELOW CONTINGENCY PLAN DEPTH

H2S response drills will be held at least once per week if possible or as often as necessary to acquaint the crews and service company personnel of their responsibilities and the proper procedures to shut-in a well. Initial drills will be performed until crews demonstrate competency donning and working under mask. After the MRC Energy Co.'s representative is satisfied with initial blowout drill procedures, a drill will be conducted weekly with each crew, as necessary. The H2S Safety Technician or designee will conduct safety talks and maintain the safety equipment, consult and carry out the instructions of the drilling supervisor. All personnel allowed in the well work area during drilling or testing operations will be instructed in the use of breathing equipment until supervisory personnel are satisfied that they are capable of using it.

After familiarization, each person must perform a drill with breathing equipment. The drill should include getting the breathing equipment, donning the breathing apparatus, and performing expected duties for a short period. A record shall be kept of all personnel drilled and the date of the drill. H2S training records will be kept on location for all personnel.

Rig crews and service company personnel shall be made aware of the location of spare air bottles, resuscitation equipment, portable fire extinguishers,  $H_2S$  monitors and detectors. Knowledge of the location of the  $H_2S$  monitors and detectors are vital in determining as our gas location and the severity of the emergency conditions.

After any device has initially detected H2S, all areas of poor ventilation shall be inspected periodically by means of a portable  $H_2S$  detector instrument. The buddy system will be utilized. (When an alarm sounds, personnel will don an SCBA, shut the well in, and proceed to SBA for roll call. The H2S Technician or designee will mask up, with a buddy and will verify source of H2S and report back to the on-site MRC Foreman.)

## **D. PROCEDURES PROGRAM**

- 1. Drill Site
  - a. The drilling rig will be located to allow prevailing winds to blow across the reserve pit.
  - b. A Safe Briefing Area will be provided with a breathing air cascade trailer and or 30-minute SCBA's at the Primary Area. Personnel will assemble at the most up-wind station under alarm conditions, or when so ordered by the MRC Energy Co. representative, the Contractor representative, or

MRC ENERGY CO.'S

the Total Safety  $H_2S$  Safety Technician. Windsocks or streamers will be anchored to various strategic places on a pole about 10 feet high, so it is in easy view from the rig floor at all times.

c. Warning signs will be posted on the perimeters. "No Smoking" signs will be posted by MRC Energy Co.as well.

d. One multi-channel automatic H<sub>2</sub>S monitor will be provided by Total Safety and the detector heads will be at the shale shaker, bell nipple, mud pits, rig floor, and quarter's area. The monitor will be located inside HSE or Company man trailer. Should the alarm be shut off to silence the sirens, the blinker light must continue to warn of H<sub>2</sub>S presence. The Total Safety H2S Safety Technician or designee will continuously monitor the detectors and will reactivate the alarm if H<sub>2</sub>S concentrations increase to a dangerous level.

e. A method of escape will be open at all times.

- f. If available, land line telephone service will be provided or cell phones provided. (Primary communications provided)
- g. A rig communication system will be provided, as needed.
- h. A gas trap, choke manifold, and degasser will be installed.
- i. A kill line, securely anchored and of ample strength, will be laid to the well-head from a safe location. This line is to be used only in an emergency.

#### General

- a. The MRC Energy Co. representative and/or the Contractor's Toolpusher will be available at all times. The drilling supervisor, while on duty, will have complete charge of the rig and location operations and will take whatever action is deemed necessary to insure personnel safety, to protect the well, and to prevent damage.
  - b. A Mud Engineer will be on location at all times when drilling takes place at the depth  $H_2S$  may be expected. The mud engineer will be able to verify the presence or absence of H2S.

## **III. CONDITIONS AND EMERGENCY PROCEDURES** A. DEFINITION OF OPERATIONAL "CONDITIONS"

<b>CONDITION I</b> Warning Flags Alarms	"POSS	SIBLE DA Green No Alarn	ANGER" n. Less than 10 ppm
Characterized By:		contain h remains i	operations in zones that may ydrogen sulfide. This condition in effect unless H <sub>2</sub> S is detected and es necessary to go to Condition II.
General Action:	<b>.</b>	a. B	e alert for a condition change
			heck all safety equipment for vailability and proper functioning.
			erform all drills for familiarization d proficiency.
<b>CONDITION II</b> Warning Flags	"MOD	<b>ERATE</b> Yellow	DANGER"
Alarms:		Actuates light.	at 10 ppm. Continuous flashing
Characterized By:		hydrogen remain ir the mud	operations in zones containing sulfide. This condition will effect until adding chemicals to system neutralizes the hydrogen r it becomes necessary to go to n III.
General Action:		a. B	e alert for a condition change
		E W W	VHEN DRILLING AHEAD - Driller and designated crewmember will don 30 min SCBA, shut-in the ell and immediately proceed to the afe Briefing Area.
		d n ir	VHEN TRIPPING – Driller and two esignated crewmembers will don 30 nin SCBA, shut in the well and nmediately proceed to the Safe riefing Area. The Derrickman will

don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

- All In Scope Personnel will proceed c. directly to the appropriate Safe Briefing Area.
- Remain in safe briefing area, take d. roll call and wait for instructions
- Contact the Total H2S Technician if e. not on location.
- f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H<sub>2</sub>S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases.
- All Out of Scope Personnel will g. report to the appropriate Safe Briefing Area.

#### **"EXTREME DANGER" CONDITION III** Red

Warning Flags

Actuate at 15 ppm. Continuous Sirens and Flashing Lights

Critical well operations which pose an immediate threat of H<sub>2</sub>S exposure to on-site personnel and a potential threat to the public.

WHEN DRILLING AHEAD a. Driller and designated crewmember will don 30 min SCBA, shut-in the well and immediately proceed to the Safe Briefing Area.

> WHEN TRIPPING – Driller and two designated crewmembers will don 30

#### Alarms

Characterized by:

General Action:

min SCBA, shut in the well and immediately proceed to the Safe Briefing Area. The Derrickman will don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

 All In Scope Personnel should don SCBA if nearby and immediately proceed to Safe Briefing Area. If SCBA in not nearby at time of alarm, DO NOT GO TOWARDS RIG AREA, but proceed directly to the Safe Briefing Area

c. All out of Scope Personnel shall evacuate the location.

d. Remain in the Safe Briefing Area, take roll call and wait for instructions.

e. Contact the Total H2S Technician if not on location.

 f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H<sub>2</sub>S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases. Use the buddy system.

g. Remain in safe briefing area, take roll call and wait for instructions.

h. A cascade breathing air systems shall be mobilized and utilized to conduct any additional on rig work required to correct the H2S release condition.

If well is ignited do not assume area is safe. SO2 is hazardous and not all H2S will burn.

13

i.

## H<sub>2</sub>S EMERGENCY PROCEDURES; IN SCOPE PERSONNEL

## A. Day To Day Drilling Operations

- 1. Upon discovering a release of H<sub>2</sub>S gas in the ambient air by warning alarms or in any other way **Do Not Panic**.
- 2. Hold your breath donning the nearest Self Contained Breathing Apparatus and rapidly move up or across-wind away from the areas where H<sub>2</sub>S sensing devices are in place, to the closest available safe briefing area. Continue to use breathing apparatus until it has been determined that the exposure of H<sub>2</sub>S gas in the ambient air no longer exists. **Do Not Panic**!
- 3. Utilize the "Buddy System", i.e.; select and pair up each person participating in the drilling of an H<sub>2</sub>S well prior to an emergency situation.
- 4. Help anyone who is overcome or affected by the H<sub>2</sub>S gas by taking him/her up-wind out of the contaminated area. (This should be done utilizing an SCBA and with a buddy.)
- 5. Take necessary steps to confirm the release of the  $H_2S$  gas into the ambient air.
  - When an H2S alarm activates, two designated personnel using the buddy system, while wearing their self contained breathing apparatus, will determine by the read-out on the fixed monitor which sensing device has detected the release of the H<sub>2</sub>S gas.
  - They will utilize the hand-held sniffer type device at the particular sensing point disclosed on the fixed monitor to corroborate the fact that H<sub>2</sub>S gas has actually been released. This will rule out the possibility of a false alarm. This will be done with a buddy and under mask after reporting to the Safe Briefing Area for roll call and instructions by on-site MRC Foreman.
- 6. Refer to the Emergency Phone Numbers and call emergency personnel.
- 7. Take the necessary steps to suppress the release of  $H_2S$  gas into the ambient air. Comply with the MRC Energy Co. Representative to physically suppress the release of  $H_2S$  gas at the actual release point.

8. Check all of MRC Energy Co.'s monitoring devices and increase gasmonitoring activities with the portable hand-operated H<sub>2</sub>S and gas detector units.

#### **Do Not Panic!**

The MRC Energy Co. representative will assess the situation and with assistance of the Contractor's Representative and Total Safety's H<sub>2</sub>S Safety Technician or on site designee, will assign duties to each person to bring the situation under control.

## **B. RESPONSIBILITIES OF WELL-SITE PERSONNEL**

In the event of a release of potentially hazardous amounts of  $H_2S$ , all personnel will immediately don their protective breathing apparatus, the well will be shut in and personnel will proceed upwind to the nearest designated safe briefing area for roll call and instructions by MRC Foreman. Consideration will be given to evacuating Out of Scope Personnel, as situation warrants.

#### 1. MRC ENERGY CO.'S Well-site Representatives

- a. If MRC Energy Co.'s well-site representative is incapacitated or not on location, this responsibility will fall to the Toolpusher/Driller.
- b. Immediately upon assessing the situation, set this plan into Action by initiating the proper procedures to contain the gas and notify the appropriate people and agencies.
- c. Ensure that the alarm area indicated by the fixed H<sub>2</sub>S Monitor is checked and verified with a portable H<sub>2</sub>S detector. (Safety Technician if on location or MRC assigned designee with a buddy utilizing SCBA's)
- d. Consult Pusher/driller of remedial actions as needed.
- e. Ensure that non-essential personnel proceed to the safe briefing area.
- f. Ensure location entrance barricades are positioned. Keep the number of persons on location to a minimum during hazardous operations.

- g. Consult each contractor, Service Company and all others allowed to enter the site, that H2S gas may be encountered and the potential hazards that may exist.
- h. Authorize the evacuation of local residents if H<sub>2</sub>S threatens Their safety.
  - i. Non essential personnel should be evacuated from location if Situation warrants.

#### 2. Toolpusher

- a. Toolpusher/Driller will assume responsibilities of MRC Energy Co.'s well-site representative if that person is incapacitated or not on location.
- Ensure that the alarm area indicated by the fixed H<sub>2</sub>S monitor is checked and verified with a portable H<sub>2</sub>S gas detector. (Alarm area indicated by the monitor will be Checked by the H2S Technician and a buddy, under mask.) This will be done after checking in and roll call at the Upwind Safe Briefing Area.
- c. Confer with MRC Energy Co.'s well-site representative or superintendent and direct remedial action to suppress the H<sub>2</sub>S and control the well.
- d. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- e. Ensure that personnel at the drill floor area are instructed on emergency actions required.
- f. Ensure that all personnel observe the appropriate safety and emergency procedures.
- g. Ensure that all persons are accounted for and provided emergency assistance as necessary.

## 3. Mud Engineer

- a. Run a sulfide check on the flowline mud.
- b. Take steps to determine the source of the H<sub>2</sub>S and suppress it. Lime and H<sub>2</sub>S scavenger shall be added to the mud as necessary.

#### 4. Total H<sub>2</sub>S Safety Technician, if on location, or MRC Designee

- a. H2S Safety Technician or designee don nearest SCBA and report to Safe Briefing Area for roll call, take a buddy masked up and check monitor and verify with a portable H<sub>2</sub>S detector the alarm area indicated by the fixed H<sub>2</sub>S monitor. Advise the Toolpusher/Driller and MRC Energy Co.'s well-site representative of findings. Record all findings.
- b. If H<sub>2</sub>S is flared, check for sulfur dioxide (SO<sub>2</sub>) near the flare as necessary. Take hourly readings at different perimeters, log readings and record on location.
- c. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- d. Ensure that the appropriate warning flags are displayed.
- e. Ensure that all personnel are in S.C.B.A. as necessary.
- f. Ensure that all persons are accounted for and provide emergency assistance as necessary.
- g. Be prepared to evacuate rig if order is issued.

#### 5. General Personnel & Visitors

a. All In Scope Personnel, if not specifically designated to shut the well in or control the well, shall proceed to the (upwind) safe briefing area. All Out of Scope Personnel shall immediately proceed to the appropriate (upwind) safe briefing area or evacuate the site as conditions warrant.

- b. During any emergency, use the "buddy" system to prevent anyone from entering or being left in a gas area alone, even wearing breathing apparatus.
- c. Provide assistance to anyone who may be injured or overcome by toxic gases. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering a potentially H<sub>2</sub>S contaminated area.
- d. Remain in safe briefing area and wait for instructions.

## C. INSTRUCTIONS FOR IGNITING THE WELL

1. The Toolpusher/Driller will confer with MRC Energy Co.'s wellsite representative who will secure the approval of the "Texas Wells Delivery Manager, prior to igniting the well, if at all possible.

The Toolpusher/Driller will be responsible for igniting the well in the event of severe well control problems. This decision should be made only as a last resort in situations where it is clear that:

- a. Human life and property are endangered, or
- b. There is no hope of controlling the well under current conditions.
- 2. Once the decision has been made, the following procedures should be followed:
  - a. Two people wearing self-contained breathing apparatus will be needed for the actual lighting of the well. They must first establish the flammable perimeter by using an explosimeter. This should be established at 30% to 40% of the lower flammable limits.
  - b. After the flammable perimeter has been established and everyone removed from the area, the ignition team should select a site upwind of the well from which to ignite the well. This site should offer the maximum protection and have a clear path for retreat from the area.

c. The ignition team should have safety belts and lifeline attached and manned before attempting ignition. If the leak is not ignited on the first attempt, move in 20 to 30 feet and fire again. Continue to monitor with the explosimeter and NEVER fire from an area with over 75% of the Lower Explosive Limit (LEL). If having trouble igniting the well, try firing 40 degrees to 90 degrees on either side of the well.

d. If ignition is not possible due to the makeup of the gas, the toxic perimeter must be established and evacuation continued until the well is contained.

NOTE: After the well is ignited, burning hydrogen sulfide  $(H_2S)$  will convert to sulfur dioxide  $(SO_2)$ , which is also a highly toxic gas.

## DO NOT ASSUME THE AREA IS SAFE AFTER THE WELL IS IGNITED

## **D. CORING PROCEDURES**

Only essential personnel shall be on the rig floor. Ten (10) stands prior to retrieving core barrel; all personnel on drill floor and in derrick shall confirm self-Contained breathing apparatus available and ready for use.

A Total H2S Technician will don a SCBA with a buddy assigned from the rig crew, and continuously monitor for H2S at each connection. Any levels detected will require operations to be shut down and all involved personnel to don SCBAs. Precautions will remain in place until barrel is laid down.

All involved personnel will don SCBAs when removing the inner barrel from the outer barrel. SCBAs can be removed once the absence of H2S in confirmed by the Total H2S Technician.

Cores will be appropriately marked and sealed for transportation.

e. All personnel must act only as directed by the person in charge of the operations.

## **Normal Operations**

## 1. Responsibilities of well-site personnel a. Well-site Representative

- 1. Notify H<sub>2</sub>S Technician of expected date to reach Contingency Plan implementation depth (Two (2) days prior to reaching suspected H<sub>2</sub>S bearing zone) or prior to starting well work.
- 2. Ensure H<sub>2</sub>S Safety Technician completes rig-up procedures prior to reaching Contingency Plan effective depth.
- 3. Restrict the number of personnel at the drilling rig or well site to a minimum while drilling, starting well work, testing or coring.
- 4. Ensure weekly H<sub>2</sub>S drills/training are performed, if possible.

## B. Toolpusher

- 1. Ensure that necessary  $H_2S$  safety equipment is provided on the rig, and that it is properly inspected and maintained.
- 2. Ensure that all personnel that work in the well area, are thoroughly trained in the use of  $H_2S$  safety equipment and periodic drills are held to maintain an adequate level of proficiency.

## C. In Scope Personnel

- 1. Remain clean-shaven. Beards and long sideburns do not allow a proper facepiece seal.
- 2. Receive  $H_2S$  safety training on location, or confirm prior training by certification that is one year within date.
- 3. Familiarize yourself with the rig's Contingency Plan.
- 4. Inspect and practice putting on your breathing apparatus.

- 5. Know the location of the "safe briefing areas".
- 6. Keep yourself "wind conscious". Be prepared to quickly move upwind and away in the event of any emergency involving release of H<sub>2</sub>S.
- D. Total Safety H<sub>2</sub>S Safety Technician or MRC Designee
  - 1. Conduct training as necessary to ensure all personnel working in well area are familiar with the contingency procedures and the operation of emergency equipment.
  - 2. Check all H<sub>2</sub>S safety equipment to ensure that it is ready for emergency use:
    - Check pressure weekly for each shift on breathing apparatus (both 30-minute and hippacks) to make sure they are charged to full volume.
    - Check pressure on cascade air bottles, if on location, to see that they are capable of recharging breathing apparatus.
    - Check oxygen resuscitator, if on location, to ensure that it is charged to full volume.
    - Check H<sub>2</sub>S detectors weekly for each shift (fixed and portable), and explosimeter, to ensure they are working properly.
  - 3. Provide a weekly report to MRC Energy Co.'s wellsite representative documenting:
    - Calibrations performed on H<sub>2</sub>S detectors.
    - Proper location and working order of H<sub>2</sub>S safety equipment.
    - Attendance of all personnel, trained or retrained, and their company.
    - Weekly drills, if held and a list of personnel participating and summary of actions.
      - 21

## OUT OF SCOPE PERSONNEL

MRC Energy Co. policy will not require Out of Scope Personnel to be clean shaven, have processed medical questionnaires, fit testing, or have certified H2S Training.

## SAFETY EQUIPMENT

## All respirators will be designed, selected, used and maintained in conformance with ANSI Z88.2, American National Standard for respiratory protection.

Personal protective equipment must be provided and used. Those who are expected to use respiratory equipment in case of an emergency will be carefully instructed in the proper use and told why the equipment is being used. Careful attention will be given to the minute details in order to avoid possible misuse of the equipment during periods of extreme stress.

Self-contained breathing apparatus provides complete respiratory and eye protection in any concentration of toxic gases and under any condition of oxygen deficiency. The wearer is independent of the surrounding atmosphere because he/she is breathing with a system admitting no outside air. It consists of a full face mask, breathing tube, pressure demand regulator, air supply cylinder, and harness. Pure breathing air from the supply cylinder flows to the mask automatically through the pressure demand regulator which reduces the pressure to a breathing level. Upon inhalation, air flows into the mask at a rate precisely regulated to the user's demand. Upon exhalation, the flow to the mask stops and the exhaled breath passes through a valve in the face piece to the surrounding atmosphere. The apparatus includes an alarm & gauge which warns the wearer to leave the contaminated area for a new cylinder of air or cylinder refill.

The derrickman is provided with a full face piece unit attached to a 5- minute escape cylinder. He will also have his own self-contained 30-minute unit breathing apparatus located on the drilling floor. He will use the 5-minute unit to exit the derrick to the floor, donning the 30-minute unit located on the floor, if needed.

All respiratory protective equipment, when not in use, should be stored in a clean, cool, dry place, and out of direct sunlight to retard the deterioration of rubber parts. After each use, the mask assembly will be scrubbed with soap and water, rinsed thoroughly, and dried. Air cylinders can be recharged to a full condition from a cascade system.

Personnel in each crew will be trained in the proper techniques of bottle filling.

The primary piece of equipment to be utilized, should anyone be overcome by hydrogen sulfide, is the oxygen resuscitator, if on location.

When asphyxiation occurs, the victim must be moved to fresh air and immediately given artificial respiration. In order to assure readiness, the bottles of oxygen will be checked at regular intervals and an extra tank kept on hand.

Hand-operated pump-type detectors incorporating detector tubes will give more accurate readings of hydrogen sulfide. The pump-type draws air to be tested through the detector tube containing lead acetate-silica gel granules. Presence of hydrogen sulfide in the air sample is shown by the development of a dark brown stain on the granules, which is the

scale reading of the concentration of hydrogen sulfide. By changing the type of detector tube used, this detector may also be used for sulfur dioxide  $(SO_2)$  detection when hydrogen sulfide  $(H_2S)$  is being burned in the flare area

Provisions must be made for the storage of all safety equipment as is evident from the foregoing discussion. All equipment must be stored in an available location so that anyone engaged in normal work situations is no more than "one breath away' from a mask.

## **V – TOXICITY OF VARIOUS GASES**

	Chemical	Specific			
Lethal Common Name ppm⁴	Formula	Gravity <sup>1</sup>	PEL (OS	SHA)²	STEL <sup>3</sup>
Hydrogen Cyanide 300	HCN	0.94	10		150
Hydrogen Sulfide 600	H₂S	1.18	20		k- 50ppm
Note: The ACGIH(7) red 15ppm.	commends a TW	A(6) value of 10	opm as the 11	LV(5) for H	H2S and an STEL of
Sulfur Dioxide 1000	SO <sub>2</sub>	2.21	2		5 ppm
Chlorine	CL <sub>2</sub>	2.45	1		
Carbon Monoxide 1000	СО	0.97	35		200/1 Hour
Carbon Dioxide 10%		1.52	500	00	5%
Methane	CH₄	0.55	900	000	
<sup>1</sup> Air = 1.0					

<sup>2</sup> **Permissible** - Concentration at which is believed that all workers may repeatedly be exposed, day after day, without adverse effect.

<sup>3</sup> **STEL** - Short Term Exposure Limit. A 15-minute time weighted average.

<sup>4</sup> Lethal - Concentration that will cause death with short-term exposure.

**TLV** – Threshold Limit Value; a concentration recommended by the American Conference of Governmental Industrial Hygienists (ACGIH)

**TWA** – Time Weighted Average; the average concentration of contaminant one can be exposed to over a given eight-hour period.

**ACGIH** – (American Conference of Governmental Industrial Hygienists) is an organization comprised of Occupational Health Professionals believed by many to be the top experts in the field of Industrial Hygiene. They are recognized as an expert rexource by OSHA. The ACGIH releases a biannual publication "Threshold Limit Values and Biological Indices" that many safety professionals consider to be the authoritative document on airborne contaminants.

Reference: API RP-49, September 1974 - Reissued August 1978

## VI. PROPERTIES OF GASES

## A. <u>CARBON DIOXIDE</u>

1. Carbon Dioxide (CO<sub>2</sub>) is usually considered inert and is commonly used to extinguish fires. It is 1.52 times heavier than air and will concentrate in low areas of still air. Humans cannot breathe air containing more than 10% CO<sub>2</sub> without losing conscience or becoming disorientation in a few minutes. Continued exposure to CO<sub>2</sub> after being affected will cause convulsions, coma, and respiratory failure.

2. The threshold limit of  $CO_2$  is 5000 ppm. Short-term exposure to 50,000 ppm (5%) is reasonable. This gas is colorless, odorless, and can be tolerated in relatively high concentrations.

## B. <u>HYDROGEN SULFIDE</u>

1. Hydrogen Sulfide (H<sub>2</sub>S) is a colorless, transparent, flammable gas. It is heavier than air and, hence, may accumulate in low places.

2. Although the slightest presence of  $H_2S$  in the air is normally detectable by its characteristic "rotten egg" odor, it is dangerous to rely on the odor as a means of detecting excessive concentrations because the sense of smell is rapidly lost, allowing lethal concentrations to be accumulated without warning. The following table indicates the poisonous nature of  $H_2S$ .

CONCENT		TRATION	EFFECTS
% H <sub>2</sub> S	PPM	GR/100 SCF <sup>1</sup>	
0.001	10	.65	Safe for 8 hours without respirator. Obvious and unpleasant odor.
0.0015	15	0.975	Safe for 15 minutes of exposure without respirator.
0.01	100	6.48	Kills smell in 3-15 minutes; may sting eyes and throat.
0.02	200	12.96	Kills smell quickly; stings eyes and throat.
0.05	500	32.96	Dizziness; breathing ceases in a few minutes; need prompt artificial respiration.
0.07	700	45.92	Rapid Unconsciousness; death will result if not rescued promptly.
0.1	1000	64.80	Instant unconsciousness, followed by death within minutes.

<sup>1</sup> Grains per 100 Cubic Feet

## VII. Treatment Procedures for Hydrogen Sulfide Poisoning

- A. Remove the victim to fresh air.
- B. If breathing has ceased or is labored, begin resuscitation immediately.
  Note: This is the quickest and preferred method of clearing victim's lungs of contaminated air; however, under disaster conditions, it may not be practical to move the victim to fresh air. In such instances, where those rendering first aid must continue to wear masks, a resuscitator should be used.
- C. Apply resuscitator to help purge  $H_2S$  from the blood stream.
- D. Keep the victim at rest and prevent chilling.
- E. Get victim under physician's care as soon as possible.

## C. <u>SULPHUR DIOXIDE</u>

- 1. Sulfur Dioxide (SO<sub>2</sub>) is a colorless, non-flammable, transparent gas.
- 2. SO<sub>2</sub> is produced during the burning of H<sub>2</sub>S. Although SO<sub>2</sub> is heavier than air, it can be picked up by a breeze and carried downwind at elevated temperatures. Since SO<sub>2</sub> is extremely irritating to the eyes and mucous membranes of the upper respiratory tract, it has exceptionally good warning powers in this respect. The following table indicates the toxic nature of SO<sub>2</sub>:

CONCEN	TRATION	EFFECTS
% SO2	PPM	
0.0005	3 to 5	Pungent odor, normally a person can detect $SO_2$ in this range.
0.0012	12	Throat irritation, coughing, constriction of the chest, tearing and smarting of eyes.
0.015	150	So irritating that it can only be endured for a few minutes.
.05	500	Causes a sense of suffocation, event with the first breath.

## VIII. BREATHING AIR EQUIPMENT DRILLS FOR ON & OFF DUTY PERSONNEL

An H<sub>2</sub>S Drill and Training Session must be given once a week to ALL on-duty personnel with off duty personnel. On-duty and Off-duty personnel will reverse roles on alternate drills.

An H2S drill and training session must be given once a week to all off-duty personnel in coincidence with on-duty personnel reversing roles on alternate drills.

The purpose of this drill is to instruct the crews in the operation and use of breathing air and  $H_2S$  related emergency equipment and to allow the personnel to become acquainted with using the equipment under working conditions. The crews should be trained to put on the breathing air equipment within one minute when required or requested to do so.

The following procedure should be used for weekly drills. The MRC supervisor must be satisfied that the crews are proficient with the equipment.

- 1. All personnel should be informed that a drill will be held.
- 2. The Total H2S Safety Technician or a designee assigned by the MRC Drilling Foreman should initiate the drill by signaling as he/she would if H2S was detected.
- 3. Personnel should don their breathing apparatus.
- 4. Once the breathing air equipment is on, the H2S Technician should check all personnel to insure proper operation.

A training and information session will be conducted after each drill to answer any H<sub>2</sub>S related questions and to cover any gaps identified from one of the following topics:

- Condition II, and III alerts and steps to be taken by all personnel.
- The importance of wind direction when dealing with H<sub>2</sub>S.
- Proper use and storage of all types of breathing equipment.
- Proper use and storage of oxygen resuscitators.
- Proper use and storage of H<sub>2</sub>S detectors (Mini Checks or equivalent).
- The "buddy system" and the procedure for rescuing a person overcome by  $H_2S$ .
- Responsibilities and duties.
- · Location of  $H_2S$  safety equipment.
- Other parts of the "H<sub>2</sub>S Contingency Plan" that should be reviewed.

NOTE: A record of attendance must be kept for weekly drills and training sessions.

## IX. HYDROGEN SULFIDE TRAINING CURRICULUM

(FOR EMPLOYERS, VISITORS, AND CONTRACTORS) EACH PERSON WILL BE INFORMED ON THE RESTRICTIONS OF HAVING BEARDS AND CONTACT LENS. THEY WILL ALSO BE INFORMED OF THE AVAILABILITY OF SPECTACLE KITS.

AFTER THE H2S EQUIPMENT IS RIGGED UP, ALL IN SCOPE PERSONNEL WILL BE H2S TRAINED AND PUT THROUGH A DRILL. ANY DEFICIENCIES WILL BE CORRECTED.

Training Completion cards are good for one year and will indicate date of completion or expiration. Personnel previously trained on another facility and visiting, must attend a "supplemental briefing" on H2S equipment and procedures before beginning duty. Visitors who remain on the location more than 24 hours must receive full H2S training given all crew members. A "supplemental briefing" will include but not be limited to: Location of respirators, familiarization with safe briefing areas, alarms with instruction on responsibilities in the event of a release and hazards of H2S and (SO2, if applicable). A training and drill log will be kept.

Topics for full H2S training shall include the following equipment if on location, but not be limited to the following:

## 1. **Brief Introduction on H2S**

- A. Slide or Computer presentation (If Available)
- B. H2S material will be distributed
- C. Re-emphasize the properties, toxicity, and hazards of H2S
- D. Source of SO2 (if applicable)
- 2. H2S Detection
  - A. Description of H2S sensors
  - B. Description of warning system (how it works & it's location)
  - C. Actual location of H2S sensors
  - D. Instruction on use of pump type detector (Gastec)
  - E. Use of card detectors, ampoules, or dosimeters
  - F. Use of combustible gas detector
  - G. Other personnel detectors used
  - H. Alarm conditions I & II,
  - I. SO2 alarms (if applicable)

## 3. **H2S Protection**

- A. Types of breathing apparatus provided (30-minute SCBA & 5-minute SCBA (with voice diaphragms for communication if supplied)
- B. Principle of how breathing apparatus works
- C. Demonstration on how to use breathing apparatus
- D. Location of breathing apparatus

## 4. Cascade System

- A. Description of cascade system
- B. How system works
- C. Cascade location of rig with reference to briefing areas
- D. How to use cascade system (with 5-minute hose work line units & refill, if supplied)
- E. Importance of wind direction and actual location of Windsocks
- F. Purpose of compressor/function (if one is on site)

## 5. H2S Rescue and First Aid

- A. Importance of wind direction
- B. Safe briefing area
- C. Buddy system
- D. H2S symptoms
- E. Methods of rescue

## 6. Hands on Training

- A. Donning/familiarization of SCBA 30-minue unit
- B. Donning/familiarization of SKADA 5- MIN. Packs
- C. Familiarization of cascades
- D. Use of O2 resuscitator
- E. Alarm conditions upwind briefing areas, etc...
- F. Duties and responsibilities of all personnel
- G. Procedures for evacuation
- H. Search and Rescue teams

## 7. Certification

A. Testing on material covered

## TOTAL SAFETY US INC., FIT TEST

X. EMPLOYEE INFORMATION	
-------------------------	--

	Employee Name	:			Date:	•	
	Date of Employe	e Medical	Evaluation:				
	Medical Status (o Authorized	circle):	Unrestricted	Limitat	ions on Use	Use	Not
	RESPIRATOR IN	FORMATIC	DIN				
	Respirator Type	(Dustmasl	k, SCBA, etc):				
	Brand:						
	Size: (circle):	XS	S	Μ	L		XL
	FIT TEST INFOR	MATION					
	Type of Fit Test		:				
	Quantital	t <u>ive</u> rta Count			Fit Factor:_		
		tester 3000	) .		Fit Factor:_		
	Isc Sa	itant Smok	ke tate (Banana Oil)		Passed / F Passed / F Passed / F Passed / F	ailed ailed	
	by certify that this cols found in App			cordanc	e with the OSH	IA Fit T	esting
Fit Te	ster Name (Print):						
	ture:						
			31				

## XI. H<sub>2</sub>S SAFETY SERVICES

HYDROGEN SULFIDE SAFETY PACKAGE – Contained on location in Total Safety H2S Equipment Trailer, unless otherwise noted:

## **RESPIRATORY SAFETY SYSTEMS**

## QTY DESCRIPTION

- 30-Minute Pressure Demand SCBA (4-Primary Safe Briefing Area, 4-Secondary Safe Briefing Area, 4-floor with one of these for derrick man)
- 9 Hose Line 5-minute Work Unit w/Escape Cylinder (1 in derrick, 6 on drill floor, 1 in mud pit wt area, 1 in shaker area)

The following shall be part of the package if requested by the MRC Foremen (at least one trailer with cascade system is required to be located in the MRC Magnolia asset for use as needed)

- 1 Breathing air cascade of 10 bottles w/regulator
- 2 Refill lines to refill 30-minute units on location
- 1 6-Man manifold that can be rigged up to work area on floor, if needed
- 6 25 foot hose lines
- 2 50 foot hose lines
- 100 Feet of hose line to rig cascade up to 12 man manifold on floor
- 12 30-minute Self Contained Breathing apparatus

## DETECTION AND ALARM SAFETY SYSTEM

- H2S Fixed Monitor w/8Channels (Loc determined at rig up) suggested.
   (Mud pit area, shaker area, bell nipple area, floor/driller area, & outside quarters)
- 5 H2S Sensors
- 3 Explosion Proof Alarms (Light and Siren) (1 on floor, 1 in work area, 1 in trailer area where quarters are located)
- 2 Personal H2S monitors
- 1 Portable Tri-Gas Hand Held Meter (O2, LEL, H2S)
- 1 Sensidyne/Gastech Manual Pump Type Detector
- 8 Boxes H2S Tubes Various Ranges
- 2 Boxes SO2 Tubes Various Ranges
- 1 Calibration Gas
- 1 Set Paper Work for Records: Training, Cal, Inspection, other

## ADDITIONAL SAFETY RELATED EQUIPMENT

## QTY DESCRIPTION

- 2 Windsocks with Pole and Bracket
- 1 Set Well Condition Sign w/Green, Yellow, Red Flags
- 1 Primary Safe Briefing Area Sign
- 1 Secondary Safe Briefing Area Sign
- 6 Operating Condition Signs for Work Areas & Living Quarters

## TRAILER WITH BREATHING AIR CASCADE WILL ALSO INCLUDE THE FOLLOWING:

This equipment will be part of the H2S equipment stored in the trailer, when on location

- 1 First aid kit
- 1 Fire Blanket
- 1 Eye wash station
- 2 Safety Harness w/150' safety line

## XII. EMERGENCY PHONE NUMBERS (Updated March 18, 2009)

## **EMERGENCY PHONE NUMBERS**

MRC Energy Co. Emergency Phone # MRC Energy Co. Permian Operations Phone------MRC Energy Co. Production 113 Daw Rd Mansfield LA 71052

Title	Names	Phone	Cell
Operations Manager			
Operation Supt.			*
Operations			
Supervisor			
Operations			
Supervisor			
Office Supervisor		-	
HSE		•	
Scheduler Planner			

## Hydrogen Sulfide Safety Consultants

Total Safety W. Bender	575-392-2973	After Hours 24 Hour Call
Blvd. Hobbs, NM		Center Through Office
		Number
Tommy Throckmorton	575-392-2973	940-268-9614
Operations Manager		
Rodney Jourdan Sales	575-392-2973	432-349-3928
Contact		

## MRC Energy Co. MEDICAL RESPONSE PLAN AND IT'S MEDICAL PROTOCOLS WILL BE FOLLOWED

## MEDICAL COORDINATOR # -----

**Emergency Numbers & Directions** 

## Hospitals (911)

Artesia General Hospital 702 N. 13 <sup>th</sup> St.	Main Phone Number	575-748-3333
Artesia, NM 88210	Main I none Mumber	373-740-3333
Nor-Lea General Hospital		
1600 N. Main Ave.	Main Phone Number	575-396-6611
Lovington, NM 88260		
Lea Regional Medical		
Center	Main Phone Number	575-492-5260
5419 N. Lovington Hwy		
Hobbs, NM 88240		
Carlsbad General Hospital		
2430 W. Pierce St.	Main Phone Number	575-887-4100
Carlsbad, NM		
Lovelace Regional Hospital		
117 E. 19 <sup>th</sup> St	Main Phone Number	575-627-7000
Roswell, NM 88201		
Winkler Co. Memorial		
Hospital	Main Phone Number	432-586-8299
821 Jeffee Dr.		
Kermit, Texas 79745		
<b>Reeves County Hospital</b>		
2323 Texas St.	Main Phone Number	432-447-3551
Pecos, Texas 79772		

State Police (911)		
Texas DPS Loving co.		
225 N.Pecos	Office Number	432-377-2411
Mentone, Texas 79754		
Texas DPS Winkler Co.		
100 E Winkler	Office Number	432-586-3465
Kermit, Texas 79745		
Texas DPS Pecos Co.		
148 N I-20 Frontage RD	Office Number	432-447-3532
Pecos, Texas 79772		
New Mexico State Police		
3300 W. Main St	Office Number	575-748-9718
Artesia, NM		
New Mexico State Police		
304 N. Canyon St	Office Number	575-885-3137
Carlsbad, NM 88220		
New Mexico State Police		
5100 Jack Gomez Blvd.	Office Number	575-392-5588
Hobbs, NM 88240		

## Local Law Enforcement (911) (Sheriff)

Reeves Co. Sheriff		
500 N. Oak ST	Office Number	432-445-4901
Pecos, Texas 79722		
Winkler Co. Sheriff		
1300 Bellaire St.	Office Number	432-586-3461
Kermit, Texas 79745		
Loving Co. Sheriff		
Courthouse	Office Number	432-377-2411
Mentone, Texas		
Lea Co. Sheriff		
1417 S. Commercial St.	Office Number	
Lovington, NM 88260		
Eddy Co. Sheriff		
305 N 7th St.	Office Number	575-766-9888
Artesia, NM 88210		
Eddy Co. Sheriff		
305 N 7th St.	Office Number	575-746-9888
Carlsbad, NM 88220		

## Federal & State Agencies

	1	
OSHA Lubbock Area Office 1205 Texas Av. Room 806 Lubbock, Texas 79401	Main Number	806-472-7681 EXT 7685
New Mexico Environment Department 400 N Pennsylvania Roswell, NM 88201	Joe Fresquez	575-623-3935
Texas Railroad Commission Midland, Texas	Main Number	844-773-0305
BLM Carlsbad, NM Field Office 620 E. Green ST Carlsbad, NM 88220	Main Number	575-234-5972
BLM Hobbs Field Station 414 W. Taylor Rd. Hobbs, NM 88240	Main Number	575-393-3612
BLM Roswell District Office 2909 W. Second St. Roswell, NM 88201	Main Number	575-627-0272
<b>TECQ Texas Commission</b> on Environmental Quality	Main Number	800-832-8224
New Mexico OCD		
U.S. Environmental Protection Agency Region 6 Texas/New Mexico	Main Number	214-655-2222
National Response Center Toxic Chemicals & Oil Spills	Main Number	800-424-8802

## **Rig Company**

The company		

## XIII. EVACUATION OF THE GENERAL PUBLIC

The procedure to be used in alerting nearby persons in the event of any occurrence that could pose a threat to life or property will be arranged and completed with public officials in detail, prior to drilling into the hydrogen sulfide formations.

In the event of an actual emergency, the following steps will be immediately taken:

- 1. The MRC Energy Co.'s representative will dispatch sufficient personnel to immediately warn each resident and transients down-wind within radius of exposure from the well site. Then warn all residence in the radius of exposure. Additional evacuation zones may be necessary as the situation warrants.
  - 2. The MRC Energy Co.'s representative will immediately notify proper authorities, including the Sheriff's Office, Highway Patrol, and any other public officials as described above and will enlist their assistance in warning residents and transients in the calculated radius of exposure.
  - 3. The MRC Energy Co.'s representative will dispatch sufficient personnel to divert traffic in the vicinity away from the potentially dangerous area. A guard to the entrance of the well site will be posted to monitor essential and non essential traffic.
  - 4. General:
    - A. The area included within the radius of exposure is considered to be the zone of maximum potential hazard from a hydrogen sulfide gas escape. Immediate evacuation of public areas, in accordance with the provisions of this contingency plan, is imperative. When it is determined that conditions exist which create an additional area (beyond the initial zone of maximum potential hazard) vulnerable to possible hazard, public areas in the additional hazardous area will be evacuated in accordance with the contingency plan.
    - B. In the event of a disaster, after the public areas have been evacuated and traffic stopped, it is expected that local civil authorities will have arrived and within a few hours will have assumed direction of and control of the public, including all public areas. MRC Energy Co. will cooperate with these authorities to the fullest extent and will exert every effort by careful advice to such authorities to prevent panic or rumors.
    - C. MRC Energy Co. will dispatch appropriate management personnel at the disaster site as soon as possible. The company's personnel

D.

will cooperate with and provide such information to civil authorities as they might require.

One of the products of the combustion of hydrogen sulfide is sulfur dioxide (SO<sub>2</sub>). Under certain conditions this gas may be equally as dangerous as  $H_2S$ . A pump type detector device, which determines the percent of SO<sub>2</sub> in air through concentrations in ppm, will be available. Although normal air movement is sufficient to dissipate this material to safe levels, the SO<sub>2</sub> detector should be utilized to check concentrations in the proximity of the well once every hour, or as necessary and the situation warrants. Also, if any low areas are suspected of having high concentrations, personnel should be made aware of these areas, and steps should be taken to determine whether or not these low areas are hazardous.

39

# Exhibit E-6: H2S Contingency Plan Emergency Contacts Matador Resources Company

Company Office			
Matador Resources Company	(972)-371-5200		
Key Personnel			
Name	Title	Office	Mobile
Billy Goodwin	Vice President Drilling	972-371-5210	817-522-2928
Gary Martin	Drilling Superintendent		601-669-1774
Dee Smith	Drilling Superintendent	972-371-5447	972-822-1010
Blake Hermes	Drilling Engineer	972-371-5485	713-876-8558
	Construction Superintendent		
	Construction Superintendent		
Artesia			
Ambulance		911	
State Police		575-746-2703	
City Police		575-746-2703	
Sheriff's Office		575-746-9888	
Fire Department		575-746-2701	
Local Emergency Planning Committee	e	575-746-2122	
New Mexico Oil Conservation Divisio	in	575-748-1283	
Carlsbad			
Ambulance		911	
State Police		575-885-3137	
City Police		575-885-2111	
Sheriff's Office		575-887-7551	
Fire Department		575-887-3798	
Local Emergency Planning Committee		575-887-6544	
New Mexico Oil Conservation Division		575-887-6544	
Santa Fe			
New Mexico Emergency Response Comission (Santa Fe)		505-476-9600	
New Mexico Emergency Response Comission (Santa Fe) 24 hrs		505-827-9126	
New Mexico State Emergency Opera	tions Center	505-476-9635	
National			
National Emegency Response Center	r (Washington, D.C.)	800-424-8802	
Medical			
Flight for Life- 4000 24th St.; Lubboo	k, TX	806-743-9911	
Aerocare- R3, Box 49F; Lubbock, TX		806-747-8923	
Med Flight Air Amb- 2301 Yale Blvd	S.E., D3; Albuquerque, NM	505-842-4433	
SB Air Med Service- 2505 Clark Carr	Loop S.E.; Albuquerque, NM	505-842-4949	
Other			
Boots & Coots IWC		800-256-9688	or 281-931-8884
Cudd Pressure Control		432-699-0139	or 432-563-3356
Haliburton		575-746-2757	
B.J. Services		575-746-3569	- 

## **Casing Design Criteria and Load Case Assumptions**

#### Surface Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

#### Intermediate #2 Casing

#### Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
  pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
  with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
  (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
  which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Production Casing**

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

#### Burst: DF<sub>b</sub>=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

#### Tensile: DFt=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Alternatives to Reduce Flaring**

Below are alternatives considered from a conceptual standpoint to reduce the amount of gas flared.

- Power Generation On lease
  - <u>Operating a generator will only utilize a Only a portion of the produced gas and is consumed operating the generator the</u>, remainder of gas would still need will to be flared.
  - O Power Company has to be willing to purchase gas back and if they are willing they require a 5 year commitment to supply the agreed upon amount of power back to them. With gas decline rates and unpredictability of markets it is impossible to agree to such long term demands. If the demands are not met then operator is burdened with penalty for not delivering.
- Compressed Natural Gas On lease
  - Gas flared would be minimal, Compressed Natural Gas is likely to but might be uneconomical to operate when the gas volume declines.
- NGL Removal On lease
  - <u>NGL Removal requires a pPlants and isare expensive on such a small scale rendering it uneconomic and still,</u> requires residue gas tois bestill flared, and uneconomical to operate when gas volume declines.

<b>WAFMSS</b> U.S. Department of the Interior BUREAU OF LAND MANAGEMENT			Data Repol 12/06/201
APD ID: 10400041094	Submission D	ate: 05/01/2019	Highlighted dat
Operator Name: MATADOR PRODUCTION COMPA	NY		reflects the mo
Well Name: BOROS FEDERAL	Well Number:	133H	recent changes Show Final Tex
Well Type: OIL WELL	Well Work Typ	e: Drill	<u></u>
Section 1 - Existing Roads			
Will existing roads be used? YES			
Existing Road Map:			
InkedBorosFed_Existing_Roads_Screenshot_LI_2019	0416132153.jpg		
Existing Road Purpose: ACCESS		Row(s) Exist? N	0
ROW ID(s)			
	1		
ID:			
Do the existing roads need to be improved? NO	· , , ,		
Existing Road Improvement Description:			
Existing Road Improvement Attachment:			
Section 2 - New or Reconstructe	ed Access Roads	· 	
Will new roads be needed? NO		I	
			,
Section 3 - Location of Existing	Wells		
Existing Wells Map? YES	La		
Attach Well map:			
······································		-	

Operator Name: MATADOR PRODUCTION COMPANY Well Name: BOROS FEDERAL

Well Number: 133H

Section 4 - Locatior	n of Existing and/or Prop	osed Production Facilities
Submit or defer a Proposed Product	ion Facilities plan? SUBMIT	
Production Facilities description:		
Production Facilities map:		
BO_BOROS_E2_FACILITY_SITE_S_2 BO_BOROS_W2_FACILITY_SITE_S_		
Section 5 - Location a	nd Types of Water Supply	/
Water Source Tab	le	
Water source type: GW WELL		
Water source use type:	SURFACE CASING	
	INTERMEDIATE/PRODUCTION CASING	
Source latitude:		Source longitude:
Source datum:		
Water source permit type:	WATER WELL	
Water source transport method:	TRUCKING	
Source land ownership: OTHER		Describe land ownership: Unknown-water source has
Source transportation land owner	ship: FEDERAL	
Water source volume (barrels): 20	0000	Source volume (acre-feet): 2.577862
Source volume (gal): 840000		
Water source type: RECYCLED		
Water source use type:	OTHER	Describe use type: Completion
Source latitude:		Source longitude:
Source datum:		
Water source permit type:	OTHER	
Water source transport method:	PIPELINE	

Operator Name: MATADOR PRODUCTIO	ON COMPANY	
Well Name: BOROS FEDERAL	Well Numb	er: 133H
Source land ownership: FEDERAL		
Source transportation land ownership	: FEDERAL	
Water source volume (barrels): 30000	0	Source volume (acre-feet): 38.66793
Source volume (gal): 12600000	· · · · · · · · · · · · · · · · · · ·	
Water source and transportation map:		
PossibleFreshwaterWells_BorosFederal_20	0190426151346.pdf	
Water source comments:	•	
New water well? NO		
New Water Well Info	)	
Well latitude:	Well Longitude:	Well datum:
Well target aquifer:		
Est. depth to top of aquifer(ft):	Est thickness of a	quifer:
Aquifer comments:		
Aquifer documentation:		
Well depth (ft):	Well casing type:	
Well casing outside diameter (in.):	Well casing inside d	iameter (in.):
New water well casing?	Used casing source:	
Drilling method:	Drill material:	
Grout material:	Grout depth:	
Casing length (ft.):	Casing top depth (ft.	):
Well Production type:	Completion Method:	
Water well additional information:		
State appropriation permit:		
Additional information attachment:		
Section 6 - Construction	Materials	
Using any construction materials: NO		
Construction Materials description:		
Construction Materials source location a	attachment:	
	·	

.

١

Well Name: BOROS FEDERAL

Well Number: 133H

# Section 7 - Methods for Handling Waste

Waste type: DRILLING

Waste content description: Drill cuttings, mud, salts, other chemicals, trash, human waste

Amount of waste: 1000 barrels

Waste disposal frequency : Daily

**Safe containment description:** Drill cuttings, mud, salts and other chemicals will be stored in steel tanks. Trash will be placed in portable trash cage. Human Waste will be disposed of in chemical toilets. **Safe containmant attachment:** 

Waste disposal type: OTHER

**Disposal location ownership: OTHER** 

Disposal type description: public/private

**Disposal location description:** Steel tanks to the BLM approved disposal site; trash cage to Carlsbad landfill; chemical toilets to Carlsbad wastewater treatment plant.

	Reserve Pit	1		
Reserve Pit being used? N	0			
Cemporary disposal of pro	duced water into reserve pit	?		
Reserve pit length (ft.)	Reserve pit width (ft.)			
Reserve pit depth (ft.)		Reserve pit vo	lume (cu	. yd.)
s at least 50% of the reser	ve pit in cut?			

Reserve pit liner

Reserve pit liner specifications and installation description

#### **Cuttings Area**

Cuttings Area being used? NO

Are you storing cuttings on location? YES

**Description of cuttings location** Cuttings will be stored in steel pits before being trucked to authorized disposal facility.

Cuttings area width (ft.)

Cuttings area length (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

Well Name: BOROS FEDERAL

### Well Number: 133H

## **Section 8 - Ancillary Facilities**

Are you requesting any Ancillary Facilities?: NO

**Ancillary Facilities attachment:** 

Comments:

Section 9 - Well Site Layout

#### Well Site Layout Diagram:

Boros\_Federal\_Slot\_\_3\_Location\_Layout\_20190423112940.pdf Comments:

# Section 10 - Plans for Surface Reclamation

Type of disturbance: No New Surface Disturbance Multiple Well Pad Name: SLOT 3

Multiple Well Pad Number: 11

**Recontouring attachment:** 

Drainage/Erosion control construction: crowned and ditched

Drainage/Erosion control reclamation: harrowed on the contour

	Well pad interim reclamation (a	acres):	Well pad long term disturbance
(acres): 0 Road proposed disturbance (acres): 0	Road interim reclamation (acre	es):	(acres): Road long term disturbance (acres):
Powerline proposed disturbance (acres): 0 Pipeline proposed disturbance	Powerline interim reclamation 0 Pipeline interim reclamation (a	(acres):	Powerline long term disturbance (acres): 0 Pipeline long term disturbance
(acres): 0 Other proposed disturbance (acres): 0	Other interim reclamation (acr	es):	(acres): Other long term disturbance (acres):
Total proposed disturbance: 0	Total interim reclamation:		Total long term disturbance:

**Disturbance Comments:** 

**Reconstruction method:** Interim reclamation will consist of shrinking well pads and facility sites by roughly a third. Disturbed areas will be recontoured. Stored soil and brush will be respreads and harrowed. Reseeding will be conducted per BLM requirements.

**Topsoil redistribution:** Stockpile topsoil will be retained along edges of pads, to be used to cover pads, facility site, and other disturbance when wells are plugged. Once last well is plugged pads and roads will be reclaimed within 6 months. Noxious weeds will be controlled.

Soil treatment: None

Existing Vegetation at the well pad:

Existing Vegetation at the well pad attachment:

Operator Name: MATADOR PRODUCTION COMPANY Well Name: BOROS FEDERAL

Well Number: 133H

Existing Vegetation Communi	ty at the road:		
Existing Vegetation Communi	ty at the road attachme	ent:	
Existing Vegetation Communi	ty at the pipeline:		
Existing Vegetation Communi	ty at the pipeline attac	hment:	
Existing Vegetation Communi	ty at other disturbance	:S:	
Existing Vegetation Communi	ty at other disturbance	s attachment:	
Non native seed used? NO			
Non native seed description:			
Seedling transplant descriptio	on:		
Will seedlings be transplanted			
Seedling transplant description	on attachment:		
Will seed be harvested for use	e in site reclamation ?		
Seed harvest description:			
Seed harvest description attac	chment:		
Seed Management			
Seed Table			
0		Total pounds/Acr	e:
Seed Su			
Seed Type	Pounds/Acre		
Seed reclamation attachment:	:		
<b>Operator Contact/R</b>	esponsible Offici	al Contact Info	
First Name:		Last Name:	
Phone:		Email:	
Seedbed prep:			

Seed BMP:

Well Name: BOROS FEDERAL

# Seed method:

Existing invasive species? NO

Existing invasive species treatment description:

Existing invasive species treatment attachment:

Weed treatment plan description: To BLM standards

Weed treatment plan attachment:

Monitoring plan description: To BLM standards

Monitoring plan attachment:

Success standards: To BLM satisfaction

Pit closure description: no pit

Pit closure attachment:

# Section 11 - Surface Ownership

Disturbance type: WELL PAD

**Describe:** 

Surface Owner: BUREAU OF LAND MANAGEMENT

Other surface owner description:

**BIA Local Office:** 

**BOR Local Office:** 

**COE Local Office:** 

DOD Local Office:

NPS Local Office:

State Local Office:

Military Local Office:

**USFWS Local Office:** 

Other Local Office:

USFS Region:

**USFS Forest/Grassland:** 

#### **USFS Ranger District:**

Well Name: BOROS FEDERAL

Well Number: 133H

# Section 12 - Other Information

Right of Way needed? NO

Use APD as ROW?

ROW Type(s):

**ROW Applications** 

**SUPO Additional Information:** 

Use a previously conducted onsite? YES

Previous Onsite information: Jesse B. conducted onsite on 1/23/19

# **Other SUPO Attachment**

MasterSUPO\_BorosFederalWellProject\_Plats\_20190501144238.pdf

