

NE MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 2-3-81	
Company MESA PETROLEUM CO. ✓		Connection TO BE DETERMINED	
Pool UNDESIGNATED ABO		Formation ABO	
Completion Date 2-3-81		Total Depth 3440' 3450'	Plug Back TD 3320'
		Elevation 4104'	Farm or Lease Name BARN FED
Csg. Size 4 1/2	Wt. 10.5	Set At 3440'	Perforations: From 2771' To 2891'
Tbg. Size 2 3/8	Wt. 4.7	Set At 2854	Perforations: From OPEN ENDED To
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE			Packer Set At NONE
Producing Thru TUBING		Reservoir Temp. °F 95° @ 3440	Mean Annual Temp. °F 60
		Baro. Press. - P _a 13.2	State NEW MEXICO
L 2854	H 2854	G _g .62	% CO ₂ 1
		% N ₂ 2	% H ₂ S -
		Prover 2"	Meter Run ORIFICE WELL TESTER

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1000		1000		72 hr.
1.	2" ORIFICE	1 1/4	9.5	-	50	920	80	930	-	-	1 hr.
2.	WELL	1 1/4	13	-	50	860	80	865	-	-	1/2 hr.
3.	TESTER	1 1/4	17.5	-	50	800	80	805	-	-	1/2 hr.
4.		1 1/4	23	-	50	670	80	685	-	-	3/4 hr.
5.											

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
2.	882	TESTER		1.0098	9837	-	876
3.	1063			1.0098	9837	-	1056
4.	1348			1.0098	9837	-	1339
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcft/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1000	P _c ² 1000	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.9683$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.3182$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1		930	865	135
2		865	748	252
3		805	648	352
4		685	469	531
5				

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2,000$

Absolute Open Flow 2,000 Mcfd @ 15.025 Angle of Slope θ 58.6° Slope, n .61

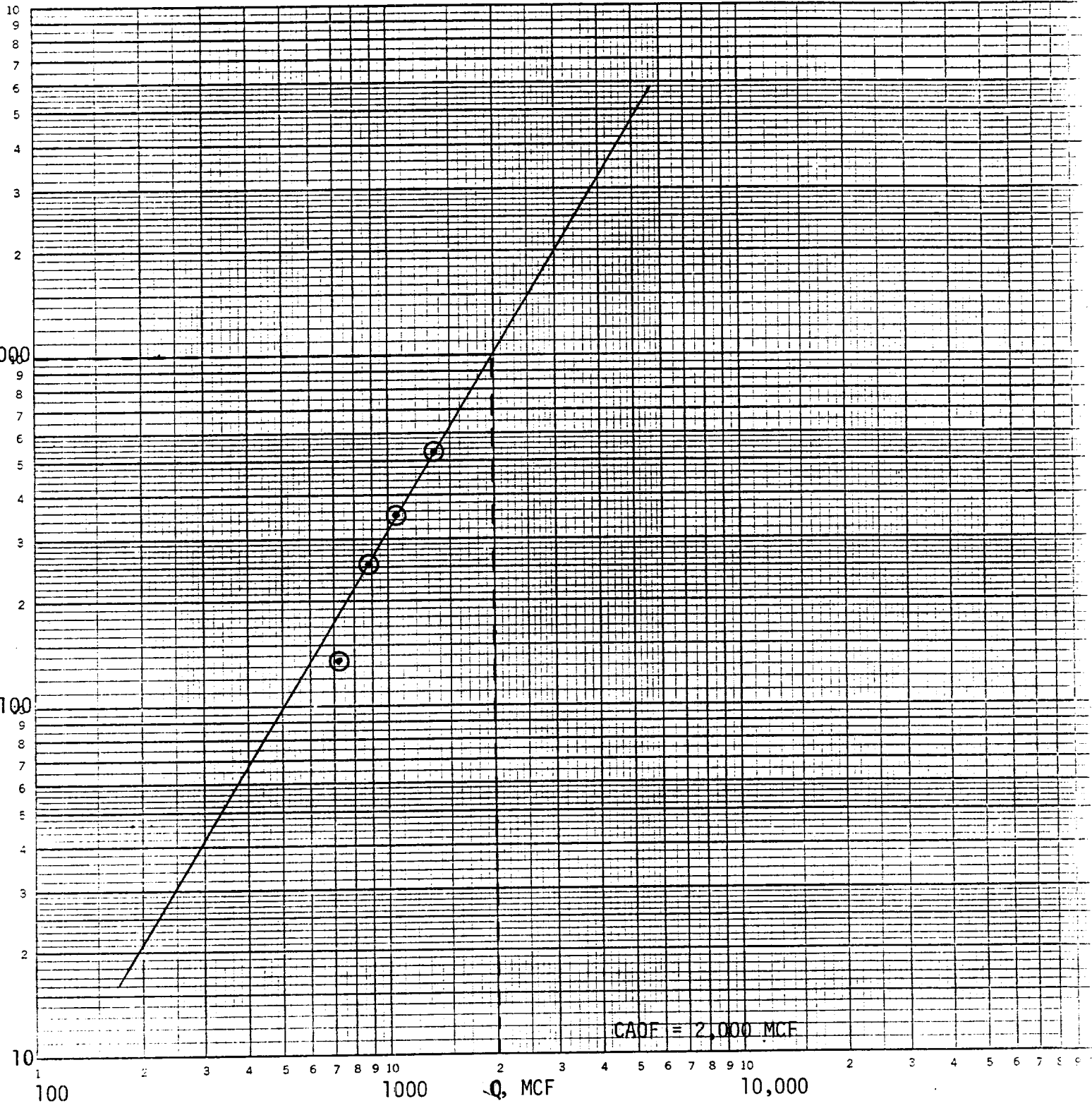
Remarks: _____

Approved By Commission:	Conducted By: E. L. BUTTROSS, JR.	Calculated By: E. L. BUTTROSS, JR.	Checked By:
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BARN FEDERAL NO.1
 S . 12, T8S, R22E
 CHAVES CO., NEW MEXICO
 2-3-81

46 7403

LOGARITHMIC 3 X 3 CYCLES
 KEUFFEL & ESSLER CO. MADE IN U.S.A.



CADF = 2,000 MCF

$$n = 1/\text{Slope} = \frac{\text{Log } Q_2 - \text{Log } Q_1}{\text{Cycle}} = \frac{\text{Log } 2000 - \text{Log } 500}{\text{Cycle}} = 330 - 2.69 = .61$$

$$\phi = 58.6^\circ$$