

97' File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

RECEIVED

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 6/17/83	
Company McClellan Oil Corporation ✓		Connection Air	
Pool Pecos Slope <i>Adir</i>		Formation ABO	
Completion Date 6/14/83		Total Depth 4128'	Plug Back TD 4081'
		Elevation 3848'	Edg. Pass. <i>3848'</i>
Coq. Size 4 1/2"	Wt. 10.5	Set At 4128'	Perforations: From 3800' To 3844'
Thq. Size 2-3/8"	Wt. 4.7	Set At <i>3951</i> 3760'	Perforations: From To
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		Packer Set At	County Chaves
Producing Thru Tubing	Reservoir Temp. °F P	Mean Annual Temp. °F 60	Baro. Press. - P <sub>a</sub> 13.2
L	H	G <sub>g</sub> .65	% CO <sub>2</sub> % N <sub>2</sub> % H <sub>2</sub> S
		Prover	Meter Run 4.026
			Taps FIG

JUL 05 1983

O. C. D.  
ANTHRA, OFFICE

MOC FEDERAL

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	4.026		1.875					985		985	
1.	4.026		1.875	205	12	70		900		900	1 hour
2.	4.026		1.875	220	24	76		800		800	1 hour
3.	4.026		1.875	250	48	80		550		550	1 hour
4.	4.026		1.875	260	62	74		355		355	1 hour
5.											

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcfd
2	22.9	72.66	220	.9850	1,240		2032
3	22.9	109.54	250	.9813	1,240		3052
4	22.9	126.96	260	.9868	1,240		3558
5							

NO.	P <sub>t</sub>	Temp. °R	T <sub>t</sub>	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P <sub>c</sub> 985	P <sub>c</sub> <sup>2</sup> 970.22	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.15$	(2) $\left[ \frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.09$		
NO	P <sub>i</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	AOF = Q $\left[ \frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 3,950$ <i>Post ID-2 7-8-83 Comp + BH</i>
1		900	810	160	
2		800	640	330	
3		550	302.5	668	
4		355	126.	844	

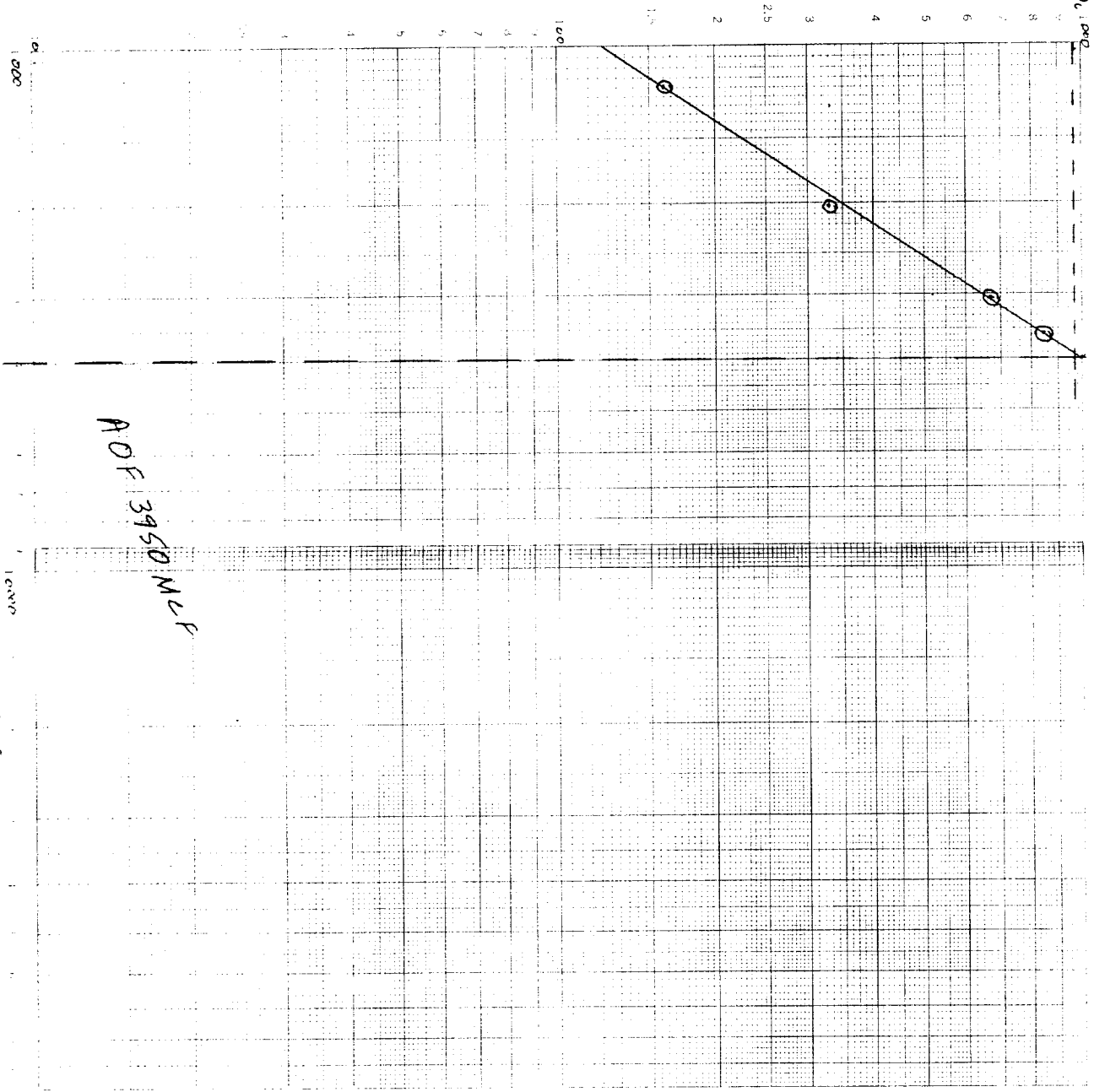
Absolute Open Flow	3,950	Mcfd @ 15.025	Angle of Slope θ	57	Slope, n	.649
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Remarks:

Approved By Division	Conducted By:	Calculated By: Rick Hipp	Checked By:
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$$P_c^2 - P_w^2$$

985  $R_{1000}$



ADP 3950 MCF

MCF

1000

10000

100000

KELTIC SERVICES INC

COMPANY McCLELLAN OIL CORP  
 LEASE MOC FED.  
 FIELD PECOS SLOPE  
 DEPTH 3820 FEET  
 TUBING PRESSURE 355 PSIG  
 FLOW RATE 2397 MSCFPD  
 BOMB NUMBER 792

DATE JUNE 17-18 1983  
 WELL NUMBER #6  
 FORMATION ABO  
 PRODUCTION TIME 3 HOURS  
 CASING PRESSURE 355 PSIG  
 TOTAL PRODUCTION 285 MSCF  
 OPERATOR CHUCK

POINT	TIME HOURS	PRESSURE PSIA	T+T1/T1
1	0.00	685.20	0.0000
2	.25	958.20	12.4143
3	.50	1010.20	6.7071
4	.75	1021.20	4.8048
5	1.00	1031.20	3.8536
6	1.25	1037.20	3.2829
7	1.50	1043.20	2.9024
8	1.75	1047.20	2.6306
9	2.00	1052.20	2.4268
10	2.50	1055.20	2.1414
11	3.00	1058.20	1.9512
12	4.00	1068.20	1.7134
13	5.00	1070.20	1.5707
14	10.00	1076.20	1.2854
15	15.00	1081.20	1.1902
16	20.00	1083.20	1.1427
17	24.00	1085.20	1.1189

THANK YOU

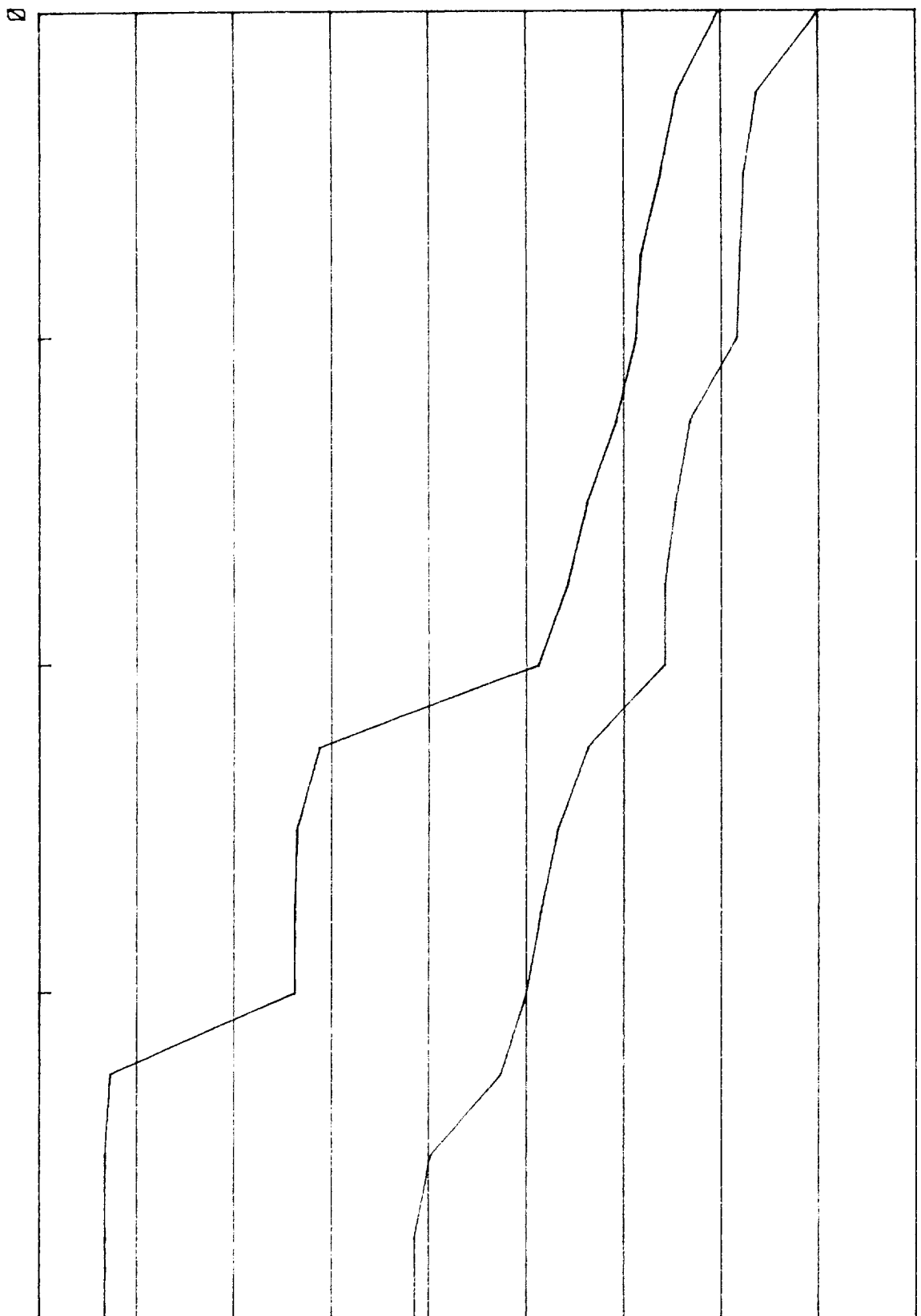
McCLELLAN OIL CORP

MOC FED. #6

JUNE 17 1983

PRESSURE PSIA

1200  
1100  
1000  
900  
800  
700  
600  
500  
400  
300  
0



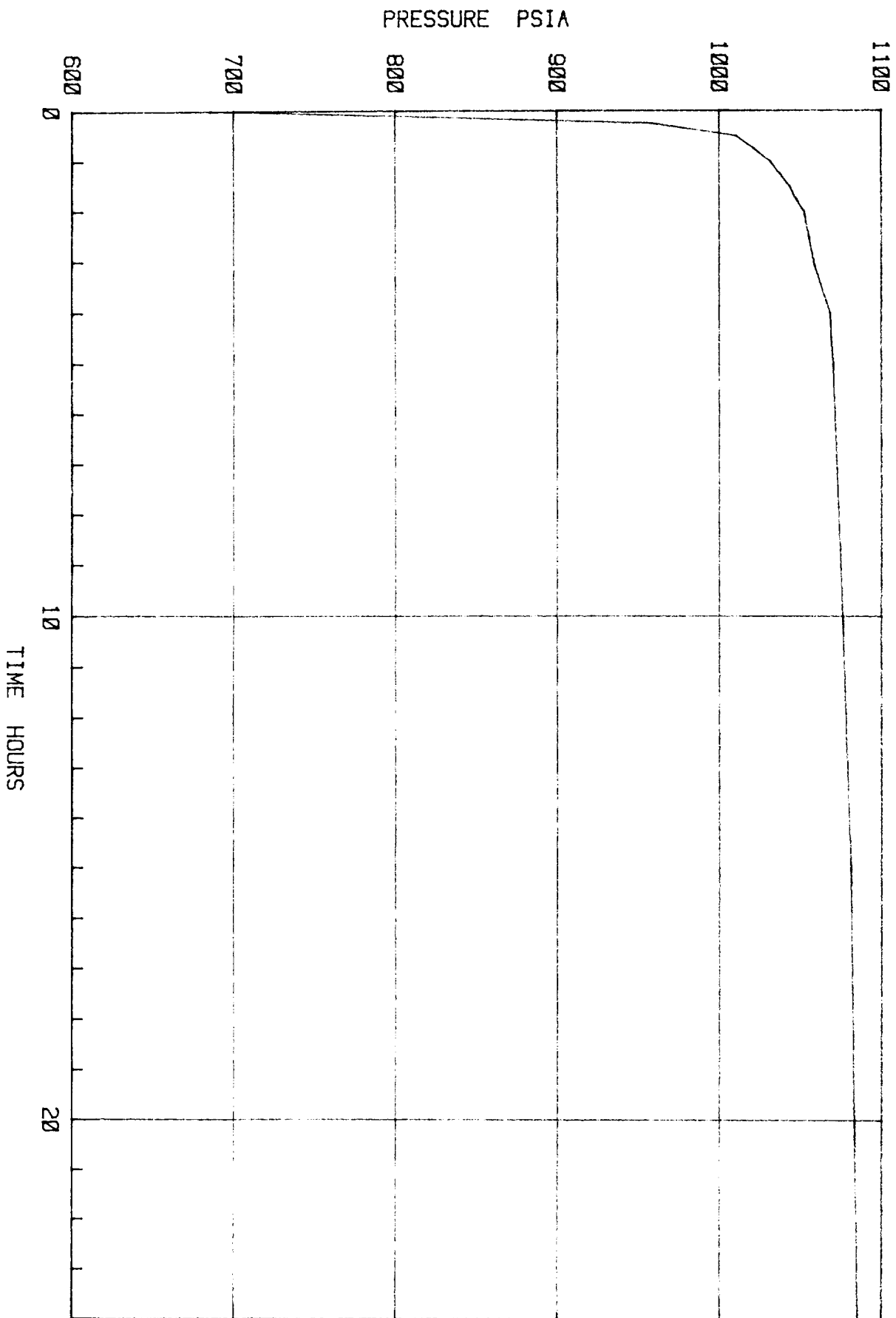
TIME HOURS

KELTIC SERVICES

McCLELLAN OIL CORP

MOC FED. #6

JUNE 17-18 1983



KELTIC SERVICES