

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122

RECEIVED

CISF File

82730

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 4/1/88		MAY 04 '88	
Company Yates Petroleum Corporation				Connection Transwestern Pipeline Company		O.C.D.	
Pool Pecos Slope				Formation Abo		Unit ARTESIA, OFFICE	
Completion Date 6/13/84		Total Depth 6456.0'		Plug Back TD 4950.0'		Elevation 3804.0'	
Csg Size 5.500"		Wt. 14.000#		d 5.012"		Set At 6454.0'	
Tbg Size 2.875"		Wt. 6.500#		d 2.441"		Set At 4800.0'	
Type Well Single				Packer Set At 4800.0'		County Chaves	
Producing Thru Tubing		Resv. Temp. °F 102 @ 4972'		Mean Temp. °F 62.0		Baro. Press. - Pa 13.2 psia.	
L 4800.0'		H 4800.0'		Gg .613		%CO2 .18	
				%N2 3.09		%H2S 0.00	
				Prover 0.000"		Meter Run 2.000"	
						Taps Flange	

NO	FLOW DATA			TUBING DATA		CASING DATA		Duration of Flow
	Prover Orifice Size X Size	Press. psig	Diff. hw	Temp. °F	Press. psig	Temp. °F	Press. psig	
SI	0.000 X 0.000	0	0.0	50	1028	0	0	0 hrs.
1.	2.067 X 1.250	195	42.2	50	778	62	0	24 hrs.
2.	2.067 X 1.250	160	57.7	50	753	62	0	24 hrs.
3.	2.067 X 1.250	160	70.6	50	643	62	0	24 hrs.
4.	2.067 X 1.250	160	100.0	50	590	62	0	24 hrs.
5.	0.000 X 0.000	0	0.0	0	0	0	0	0 hrs.

RATE OF FLOW CALCULATIONS

NO	Coefficient (24 HOUR)	$\sqrt{hwPm}$	Pressure Pm	Flow Temp Factor Ft.	Gravity Factor Fg	Super Compress. Fact. Fpv	Rate of Flow Q, Mcfd
1.	8.134	93.73	208.20	1.010	1.277	1.017	1000
2.	8.134	99.97	173.20	1.010	1.277	1.014	1063
3.	8.134	110.58	173.20	1.010	1.277	1.014	1176
4.	8.134	131.61	173.20	1.010	1.277	1.014	1400
5.	0.000	0.00	0.00	0.000	0.000	0.000	0

NO	Pr	Temp. °R	Tr	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.31	510	1.45	.967	1039.100 Mcf/bbl.	52.100 Deg.	.613	.616	667.2 PSIA	351.3°R
2.	.26	510	1.45	.973					667.1 PSIA	352.3°R
3.	.26	510	1.45	.973						
4.	.26	510	1.45	.973						
5.	0.00	0	0.00	0.000						

NO	Pt <sup>2</sup>	Pw	Pw <sup>2</sup>	Pc <sup>2</sup> -Pw <sup>2</sup> (1)	Pc <sup>2</sup> / (Pc <sup>2</sup> -Pw <sup>2</sup> )	(2) [Pc <sup>2</sup> / (Pc <sup>2</sup> -Pw <sup>2</sup> )] <sup>n</sup>
1.	626.0	794.5	631.3	452.8	1.5279	1.3731
2.	587.1	770.1	593.0	491.1		
3.	430.6	661.8	438.0	646.1		
4.	363.9	612.0	374.5	709.6		
5.	0.0	0.0	0.0	0.0		

ROF = Q [Pc<sup>2</sup> / (Pc<sup>2</sup>-Pw<sup>2</sup>)]<sup>n</sup> = 1922 Mcfd

Absolute Open Flow    1922 Mcfd @ 15.025    Angle of Slope, θ    37    Slope, n    .748

Remarks: \_\_\_\_\_

Approved By: \_\_\_\_\_    Conducted By: David Weaver    Calculated By: Andrea Carpenter    Checked By: \_\_\_\_\_