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Type Test [x] Initial [ ] Annual [ ] Special	Test Date 8/25/88	APR 10 '89
Company Yates Petroleum Corporation	Connection Transwestern Pipeline Company	
Pool FOUR RANCH PRE-PERMIAN ~~Ordovician~~	Formation Foor Ranch	Unit O.C.D. ARTESIA OFFICE

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
7/30/88	6410.0'	6135.0'	3806.5'	Witz VN State

Csg Size	Wt.	d	Set At	Perforations:	Well No.
5.500"	14.000#	5.012"	6410.0'	From 6054.0' To 6097.0'	3

Tbg Size	Wt.	d	Set At	Perforations:	Unit Sec Twp Rge
2.875"	6.500#	2.441"	5984.0'	From 0.0' To 0.0'	I 26 9S 26E

Type Well	Packer Set At	County
Single	5984.0'	Chaves

Producing Thru	Resv. Temp. °F	Mean Temp. °F	Baro. Press. - Pa	State
Tubing	180 @ 5890'	62.0	13.2 psia.	New Mexico

L	H	Gg	%CO2	%N2	%H2S	Prover	Meter Run	Taps
5984.0'	5984.0'	.648	1.08	4.06	0.00	0.000"	2.000"	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO	Prover Size X Orifice Size	Press. psig	Diff. hw	Temp. °F	Press. psig	Temp. °F	Press. psig	Temp. °F	Duration of Flow
SI	0.000 X 0.000	0	0.0	96	1980	0	0	0	0 hrs.
1.	2.067 X 1.375	255	46.4	92	1863	62	0	0	24 hrs.
2.	2.067 X 1.375	280	61.3	95	1829	62	0	0	24 hrs.
3.	2.067 X 1.375	295	79.1	96	1822	62	0	0	24 hrs.
4.	2.067 X 1.375	305	82.0	94	1780	62	0	0	24 hrs.
5.	0.000 X 0.000	0	0.0	0	0	0	0	0	0 hrs.

RATE OF FLOW CALCULATIONS

NO	Coefficient (24 HOUR)	$\sqrt{h_w P_m}$	Pressure Pm	Flow Temp Factor Ft.	Gravity Factor Fg	Super Compress. Fact. Fpv	Rate of Flow Q, Mcfd
1.	10.204	111.55	268.20	.971	1.242	1.018	1397
2.	10.204	134.06	293.20	.968	1.242	1.019	1677
3.	10.204	156.14	308.20	.967	1.242	1.020	1953
4.	10.204	161.53	318.20	.969	1.242	1.021	2026
5.	0.000	0.00	0.00	0.000	0.000	0.000	0

NO	Pr	Temp. °R	Tr	Z
1.	.40	552	1.54	.965
2.	.44	555	1.55	.962
3.	.46	556	1.55	.960
4.	.48	554	1.54	.959
5.	0.00	0	0.00	0.000

Gas Liquid Hydrocarbon Ratio Dry Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0.000 Deg.

Specific Gravity Separator Gas	.648	xxxxxxxxxxxxx
Specific Gravity Flowing Fluid	xxxxx	.648
Critical Pressure	668.2 PSIA	668.2 PSIA
Critical Temperature	358.7°R	358.7°R

Pc 1993.2 Pc² 3972.8

NO	Pt²	Pw	Pw²	Pc²-Pw²
1.	3520.1	1879.7	3533.2	439.6
2.	3393.7	1847.3	3412.6	560.2
3.	3368.0	1842.2	3393.6	579.3
4.	3215.6	1800.9	3243.2	729.6
5.	0.0	0.0	0.0	0.0

$$(1)\ \frac{P_c^2}{P_c^2-P_w^2} = 5.4559 \qquad (2)\ \left[\frac{P_c^2}{P_c^2-P_w^2}\right]^n = 3.4707$$

$$AOF = Q\left[\frac{P_c^2}{P_c^2-P_w^2}\right]^n = 7032\ \text{Mcfd}$$

Absolute Open Flow 7032 Mcfd @ 15.025	Angle of Slope, θ 36	Slope, n .733

Remarks:

Approved By:	Conducted By:	Calculated By:	Checked By:
	David Weaver	Andrea Carpenter	

ca

WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (Pw) C-122D

Adopted 9-1-65

DATE 4/6/89

COMPANY Yates Petroleum Corporation LEASE Witz VN State WELL NO. 3

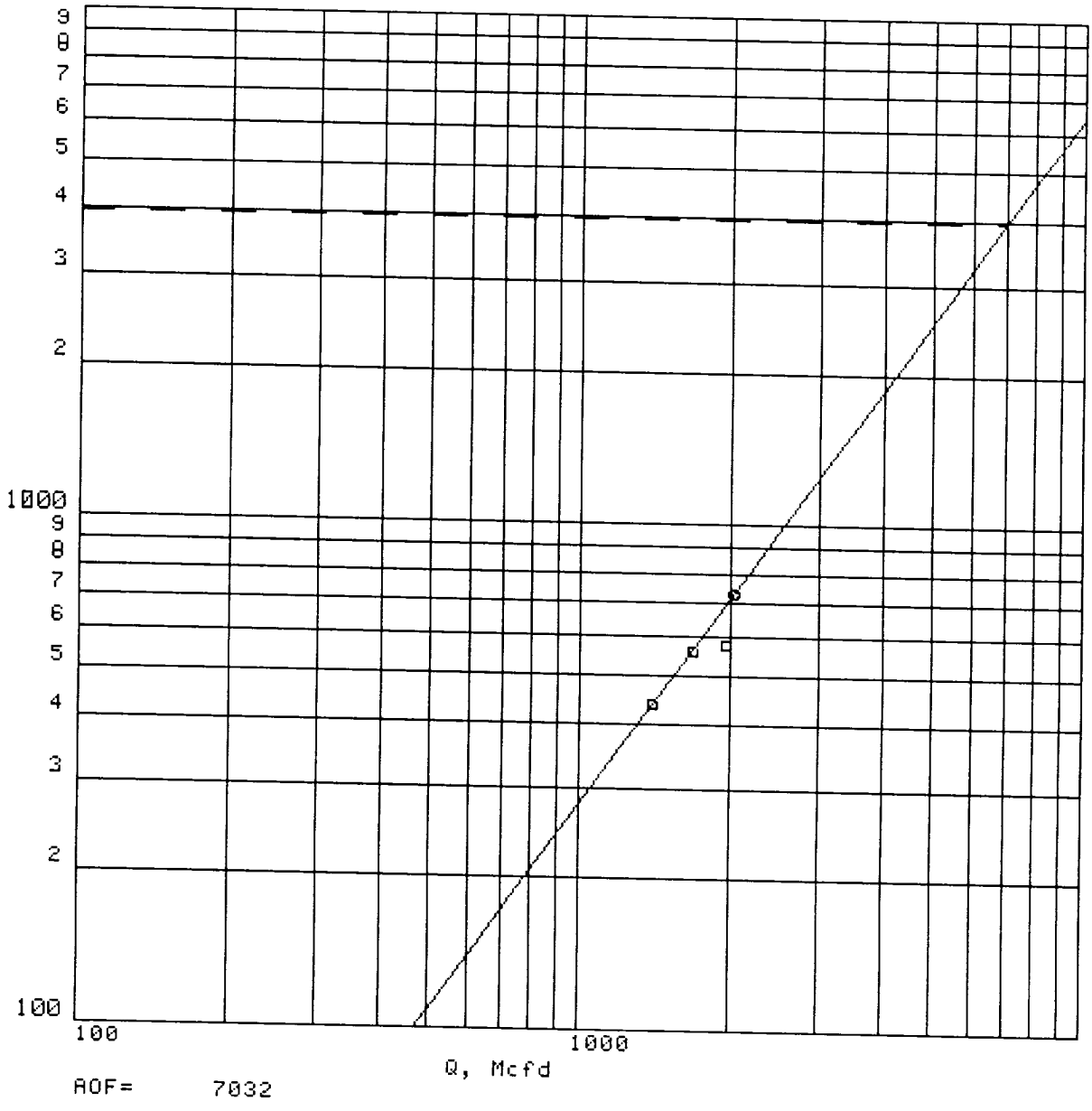
LOCATION: Unit I Section 26 Township 9S Range 26E

L 5984.0 H 5984.0 L/H 1.000 G .648 %CO2 1.08 %N2 4.06 %H2S 0.00

d 2.441 Fr .010495 GH 3877.6 Pcr 668.2 Tcr 358.7

LINE	1st Rate	2nd Rate	3rd Rate	4th Rate	5th Rate
1 Qm	1.397	1.677	1.953	2.026	0.000
2 Tw(W.H.°R)	522.0	522.0	522.0	522.0	0.0
3 Ts(B.H.°R)	640.0	640.0	640.0	640.0	0.0
4 T=(Tw+Ts)/2	581.0	581.0	581.0	581.0	0.0
5 Z(Est.)	.835	.836	.836	.837	0.000
6 TZ	485.0	485.5	485.6	486.4	0.0
7 GH/TZ	7.996	7.987	7.985	7.973	0.000
8 e^s(Table XIV)	1.349	1.349	1.349	1.348	0.000
9 $1-e^{-s}$(Table XIV)	.259	.259	.259	.258	0.000
10 Pt	1876.2	1842.2	1835.2	1793.2	0.0
11 $Pt^2/1000$	3520.1	3393.7	3368.0	3215.6	0.0
12 Fr(Table XV)	.010495	.010495	.010495	.010495	0.000000
13 Fc=FrTZ	5.094	5.100	5.096	5.104	0.000
14 FcQm	7.117	8.551	9.953	10.342	0.000
15 $L/H(FcQm)^2$	50.646	73.126	99.070	106.957	0.000
16 $Fw=L/H(FcQm)^2(1-e^{-s})$	13.111	18.913	25.636	27.640	0.000
17 $Pw^2=Pt^2+Fw$	3533.2	3412.6	3393.6	3243.2	0.0
18 $Ps^2=e^sPw^2$	4767.5	4603.1	4578.3	4373.4	0.0
19 Ps	2183.5	2145.5	2139.7	2091.3	0.0
20 P=(Pt+Ps)/2	2029.8	1993.9	1987.5	1942.2	0.0
21 Pr=(P/Pcr)	3.04	2.98	2.97	2.91	0.00
22 Tr=(T/Tcr)	1.62	1.62	1.62	1.62	0.00
23 Z(Table XI)	.835	.836	.836	.837	0.000

Company	Yates Petroleum Corporation
Well	Witz VN State No. 3
Location	I, 26-9S-26E
County	Chaves
Date	4/6/89



$P_c^2 - P_w^2$, THOUSANDS