

RECEIVED BY *BM c-12*
Revised 10-1-78
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O. C. D.
ARTESIA, OFFICE

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 12-12-83		O. C. D. ARTESIA, OFFICE	
Company MESA PETROLEUM CO. ✓			Connection UNCONNECTED		
Pool DIAMOND MOUND ATOKA-MORROW			Formation MORROW		Unit
Completion Date 11-26-83		Total Depth 9330	Plug Back TD 9137'	Elevation 3650	Farm or Lease Name DEPCO FEDERAL
Cq. Size 4 1/2	Wt. 11.6# & 13.5#	d 3.795	Set At 9234	Perforations: From 9022 To 9092	Well No. 2
Thq. Size 2 3/8	Wt. 4.7#	d 1.995	Set At 8888	Perforations: From OPEN ENDED To	Unit Sec. Twp. Rye. 1 4 16S 28E
Type Well - Single - Drivenhead - G.C. or G.O. Multiple SINGLE				Packer Set At 8888	County EDDY
Producing Thru TUBING		Reservoir Temp. °F 144 @ 9311	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2	State NEW MEXICO
L 8888	H 6888	Cq .640	% CO ₂ 1	% N ₂ 1	% H ₂ S
Prover 2" CRITICAL FLOW PROVER		Meter Run	Taps		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI							1320				+72 hr SI
1.	2" x 1/4"			490		86	1250	64			1 hr
2.	2" x 5/16"			500		100	1185	68			1 hr
3.	2" x 3/8"			457		85	1115	70			1 hr
4.	2" x 7/16"			300		68	1018	70			1 hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.087	FLOW PROVER	503	.9759	1.260		672
2	1.672	FLOW PROVER	513	.9636	1.260		1041
3	2.378	FLOW PROVER	470	.9768	1.260		1376
4	3.408	FLOW PROVER	373	.9924	1.260		1590
5.							

NO.	R _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ XXXXX XXXX
3.					Specific Gravity Flowing Fluid _____ XXXXX
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

NO.	P _c ²	P _w ²	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_w^2 - P_w^2} = 4.6084$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.1937$
1	1562	1262	1592	150	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4,400$	Post FO-2 12-23-83 Comp + RR
2	1404	1214	1473	269		
3	1243	1168	1364	378		
4	1036	1094	1196	546		
5						

Absolute Open Flow 4,400 Mcfd @ 15.025 Angle of Slope \ominus 52.7° Slope, n .76

Remarks: _____

Approved By Division	Conducted By: JIM CRAIG	Calculated By: <i>EB 12-14-83</i> E. L. BUTTROSS, JR.	Checked By:
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