

NEW MEXICO CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Form C-122
Revised 9-1-65

File

RECEIVED

MAY 12 1969

D. C. C.
ARTERIA OFFICE

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 4-23-69					
Company Kerr-McGee Corporation						Connection None					
Pool Permian Basin						Formation Permian		Unit			
Completion Date 1-22-69		Total Depth 9,672'		Plug Back TD 9,500'		Elevation 3300 GS		Farm or Lease Name			
Csg. Size 5 1/2"	Wt. 17	d	Set At 9,672'	Perforations: From 9,400' To 9,450'				Well No. 1			
Tbg. Size 2 3/8"	Wt. 4.7	d	Set At 9,672'	Perforations: From To				Unit	Sec. 11	Twp. 10N	Rge. 6E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At 2,300'		County			
Producing Thru Tubing		Reservoir Temp. °F 175 @ 9,370'		Mean Annual Temp. °F 50		Baro. Press. - P _a 30.0		State			
L 9,200'	H 9,360'	Gg 0.617	% CO ₂ 0.00	% N ₂ 0.00	% H ₂ S	Prover	Meter Run	Taps			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1	3" x 0.50"			450	6"	100	450	100	200	100	/
2	3" x 0.75"			725	10"	100	450	100			/
3	3" x 0.75"			810	10"	100	450	100			/
4	3" x 0.75"			1,017	10"	100	450	100			/
5											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	1.183	262.5	100.0	0.999	1.000	1.000	240
2	2.602	327.5	725.0	0.999	1.000	1.000	650
3	2.602	259.8	810.0	0.999	1.000	1.000	600
4	2.602	315.4	1,017.0	0.999	1.000	1.000	1,100
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.65	566	1.56	0.999	1.000	57.1	0.617	X X X X X X X X	100	100
2	1.07	580	1.52	0.999	1.000	57.1	0.617	X X X X X	100	100
3	1.23	586	1.51	0.999	1.000	57.1	0.617		100	100
4	1.53	553	1.53	0.999	1.000	57.1	0.617		100	100
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P_c 1600 P_c² 25600

NO.	P _f ²	P _w	P _w ²	P _c ² - P _w ²
1		1612	2599	0
2		1802	3246	2354
3		1960	3841	2719
4		1982	3928	2672
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 0.500$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.600$

ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1818$

Absolute Open Flow 1818 Mcfd @ 15.025		Angle of Slope θ	Slope, n
Remarks:			
Approved By Commission:		Conducted By:	Calculated By:
5-1-11		J. Carter	D. C. C.