

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 12-18-74		JAN 21 1975	
Company David Fasken				Connection		O. C. C.	
Pool Cemetery Morrow				Formation Morrow		Unit ARTESIA, OFFICE	
Completion Date 12-16-74		Total Depth 9704		Plug Back TD 9640		Elevation 3505	
Csg. Size 4 1/2		Wt. 11.6		Set At 9704		Perforations: From 9448-52 to 9474-80	
Tbg. Size 2 3/8		Wt. 4.7		Set At 9000		Perforations: From 9550-54 to	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 9000		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 173 @ 9301'		Mean Annual Temp. °F 70°		Baro. Press. - P _a 13.2	
L 9501		H 9501		G _g 0.610		% CO ₂	
						% N ₂	
						% H ₂ S	
						Prover Pos. Cks	
						Meter Run	
						Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI				2966			2966		Pkr		
1.	2"	X	8/64"	2749			2749	58°			45 min.
2.	2"	X	10/64"	2588			2588	58°			45 min.
3.	2"	X	13/64"	2253			2253	60°			45 min.
4.	2"	X	16/64"	1988			1988	61°			45 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	0.2618		2762.2	1.002	1.280	1.165	1080.5
2	0.4173		2601.2	1.002	1.280	1.170	1628.9
3	0.7208		2266.2	1.000	1.280	1.169	2444.2
4	1.1120		2001.2	0.999	1.280	1.164	3312.3
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.	4.12	518	1.43	0.737	A.P.I. Gravity of Liquid Hydrocarbons	Dry Gas	Deq.
2.	3.88	518	1.43	0.731	Specific Gravity Separator Gas	0.610	XXXXXXXXXX
3.	3.38	520	1.44	0.732	Specific Gravity Flowing Fluid	XXXXXX	
4.	2.98	521	1.44	0.738	Critical Pressure	671	P.S.I.A.
5.					Critical Temperature	362	R

NO.	P _r ²	P _s	P _s ²	P _r ² - P _s ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} =$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n =$
1	3445.2	11869	1941			
2	3287.2	10806	3004			
3	2875.2	8267	5543			
4	2563.2	6570	7240			
5						

Absolute Open Flow		5800	Mcf/d @ 15.025	Angle of Slope @	49° 35'	Slope, n	0.85126
Remarks:							

Approved By Commission:	Conducted By:	Checked By:
	Teffeller, Inc.	