

15 file  
122 file

RECEIVED

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 1-26-77		FEB 2 1977	
Company Monsanto Company ✓			Connection			
Pool Dagger Draw (Morrow Gas)			Formation Morrow		O. G. G. ARTESIA, OFFICE	
Completion Date 1-26-77		Total Depth 9460		Plug Back TD 9383	Elevation 3578 DF	Form or Lease Name CovertCom
Casing Size 5.50"	Wt. 20#	d. 4.778"	Set At 9453	Perforations: From 9292 To 9304		Well No. 1
Tub. Size 2.875EUE	Wt. 6.40#	d. 2.441"	Set At 9166	Perforations: From To		Unit Soc. Twp. Rge. F 6 20-S 25-E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Completion				Packer Set At 9166		County Eddy
Producing Thru Tubing		Reservoir Temp. °F 153 @ 9298		Mean Annual Temp. °F 60	Baro. Press. - P <sub>a</sub> 13.2	State New Mexico
L 9298	H 9298	Cg 0.595	% CO <sub>2</sub> 0.00	% N <sub>2</sub> 0.00	% H <sub>2</sub> S 0.00	Prover Meter Run X

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1689	48			156 Hr
1.	3.00		0.75	310	9.00"	78	892	66			1.00 Hr
2.	3.00		0.75	310	10.00"	76	480	68			1.00 Hr
3.	3.00		0.75	290	1.00"	74	299	68			1.00 Hr
4.	3.00		0.75	290	1.00"	72	295	64			1.00 Hr
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	2.67	53.933	323.20	0.9831	1.2964	1.0250	188
2	2.67	56.851	323.20	0.9850	1.2964	1.0260	199
3	2.67	17.413	303.20	0.9868	1.2964	1.0240	61
4	2.67	17.413	303.20	0.9887	1.2964	1.0240	61
5							

NO.	P <sub>f</sub>	Temp. °R	T <sub>f</sub>	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.48	538	1.50	0.951	None Produced	None Produced	0.595	0.595	671	358
2.	0.48	536	1.50	0.950						
3.	0.45	534	1.49	0.948						
4.	0.45	532	1.49	0.948						
5.										

NO.	P <sub>1</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>
1	905.3	820	2077	
2	493.5	243	2654	
3	311.8	97	2800	
4	308.4	95	2802	
5				

(1)  $\frac{P_c^2}{P_c^2 - P_w^2} = 1.05765$     (2)  $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.05765$

AOF = Q  $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 210$

Absolute Open Flow 210 Mcfd @ 15.025    Angle of Slope θ 45°    Slope, n 1.00

Remarks:

Approved by Commission:    Conducted By: West Texas Engr. Serv.    Calculated By: L.H. Hagler    Checked By: E.M. Scholl