

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 6-1-65

RECEIVED

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 3-5-74		MAR 13 1974				
Company Monsanto Company				Connection O.C.C.					
Well Burton Flat (Strawn)			Formation Strawn		Unit E				
Completion Date 3-5-74		Total Depth 11,540		Mud Back TD 11,482		Elevation 3229 KB		Farm or Lease Name Burton Flat Deep Unit	
Casing Size 7	Int. 26#	Set At 6.276	Set At 11,540	Perforations: From To		Well No. 9-UT			
Tubing Size 2 3/8 NuLoc	Int. 4.7	Set At 1.995	Set At 10,128	Perforations: 10,332 - 10,346 From 10,310 To 10,318		Unit E	Sec. 35	Twp. 20-S	Rge. 28-E
Type Well - Single - Stippled - G.G. or G.O. Multiple Single				Packer Set At 10,128		County Eddy			
Producing thru Tubing		Reservoir Temp. *F 142 @ 10,328		Mean Annual Temp. *F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 10,328	H 10,328	G _s .670	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run X	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.		Temp. *F
1.	4.0"		1.0	457	21	90	2578	43			1 Hr
2.	4.0"		1.0	450	31	94	2530	48			1 Hr
3.	4.0"		1.0	460	49	99	2476	65			1 Hr
4.	4.0"		1.0	465	62	98	2310	66			1 Hr
5.							1965	70			1 Hr

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super. Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	4.965	99.37	470.2	.9723	1.2217	1.043	611
2.	4.965	119.83	463.2	.9688	1.2217	1.041	733
3.	4.965	152.27	473.2	.9645	1.2217	1.042	928
4.	4.965	172.19	478.2	.9653	1.2217	1.042	1051

NO.	P _c	Temp. *R	T _c	Z	Gas Liquid Hydrocarbon Ratio	None Produced	Vel/Sec.
1.	.70	550	1.44	.919	A.P.I. Gravity of Liquid Hydrocarbons		Sec.
2.	.69	554	1.45	.922	Specific Gravity Separator Gas	.670	XXXXXXXXXX
3.	.71	559	1.46	.921	Specific Gravity Flowing Fluid	XXXXXXXXXX	
4.	.71	558	1.46	.921	Critical Pressure	669	P.S.I.A. 669 P.S.I.A.
5.					Critical Temperature	382	R 382 R

NO.	P _c ²	P _w	P _f	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{6714}{2773}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.55406$
1.		2546.0	6482	232		
2.		2492.0	6210	504		
3.		2321.1	5388	1326		
4.		1985.2	3941	2773		

AOF = Q	$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1632$
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Apparent Open Flow	1632	Mcf @ 15.025	Angle of Slope @	63 1/2	Slope, n	.499
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Shut-In	2-21-74
*ID of Meter Run	3.826"

Conducted By:	W T Hagler	Calculated By:	H L Hagler	Checked By:	
WEST TEXAS CONSULTING SERVICE, INC.					