

SEP 27 1982

Test No. 9-11-82										SEP 27 1982	
Company Perry R. Bass					Fluid AIR					O. C. D. ARTESIA, OFFICE	
Field Indian Flats Atoka					Formation ATOKA					Unit Big Eddy Unit	
Completion Date 9-11-82		Test Depth 12519		True Vertical Depth 12230		Elevation 3279		BIG EDDY UNIT			
Casing Size 5 1/2"		ID 12519		Perforations 11283		To 11494		Well No. 92			
Tubing Size 2 3/8		ID 11229		Perforations 11229		To 11494		Unit 14 T21S R26E			
Type Well - Single - Flow Meter - Gas or Gas Multiple					Pressure at At 11300		County EDDY				
Producing Unit TBG.		Reservoir Temp. °F 187 @ 11300		Mean Annual Temp. °F 60°		Mean Pressure - P _a 13.2		State NEW MEXICO			
L 11300		H 11300		G _g .5969		% CO ₂ .575		% N ₂ 1.146		Prover 4"	
								Meter Run 4"		FLG.	

FLOW DATA						TEMP. DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Pressure, psia	P.B., hg	Temp., °F	Pressure, psia	Temp., °F	Pressure, psia	Temp., °F	
1	4 x 2.000	500	3.5	96	5410					72 hrs.
2	4 x 1.000	503	14.0	99	5280					1 hr.
3	4 x 1.000	700	56.0	98	5000					1 hr.
4	4 x 2.000	690	7.0	100	3400					1 hr.
5	4 x 2.000	500	5.0	102	1975					4 hrs.

RATIO OF FLOW DATA CORRELATION							
NO.	Coefficient (24 hour)	$\sqrt{h_w P_m}$	Pressure P ₁	Flow Factor F ₁	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mscf/d
1	4.753	42.38	513.2	.9671	1.294	1.036	261
2	4.753	85.01	516.2	.9645	1.294	1.035	522
3	4.753	199.85	713.2	.9653	1.294	1.048	1243
4	19.81	70.16	703.2	.9636	1.294	1.048	1816
5	19.81	50.66	513.2	.9619	1.294	1.034	1292

NO.	F ₁	Temp. °R	T _g	Z	One Liquid Hydrocarbon Bubble	Two Liquid Hydrocarbon Bubbles	Three Liquid Hydrocarbon Bubbles	Four Liquid Hydrocarbon Bubbles	Five Liquid Hydrocarbon Bubbles	Rate of Flow Q, Mscf/d
1	.76	556	1.55	.932	268.155	61.6 @ 60	.5969	XXXXXX	XXXXXX	6.08
2	.77	559	1.56	.933	671	358	XXXXX	XXXXX	XXXXX	6.71
3	1.06	558	1.56	.910	671	358	XXXXX	XXXXX	XXXXX	6.71
4	1.05	560	1.56	.911	358	358	XXXXX	XXXXX	XXXXX	3.58
5	.76	562	1.57	.936	358	358	XXXXX	XXXXX	XXXXX	3.58

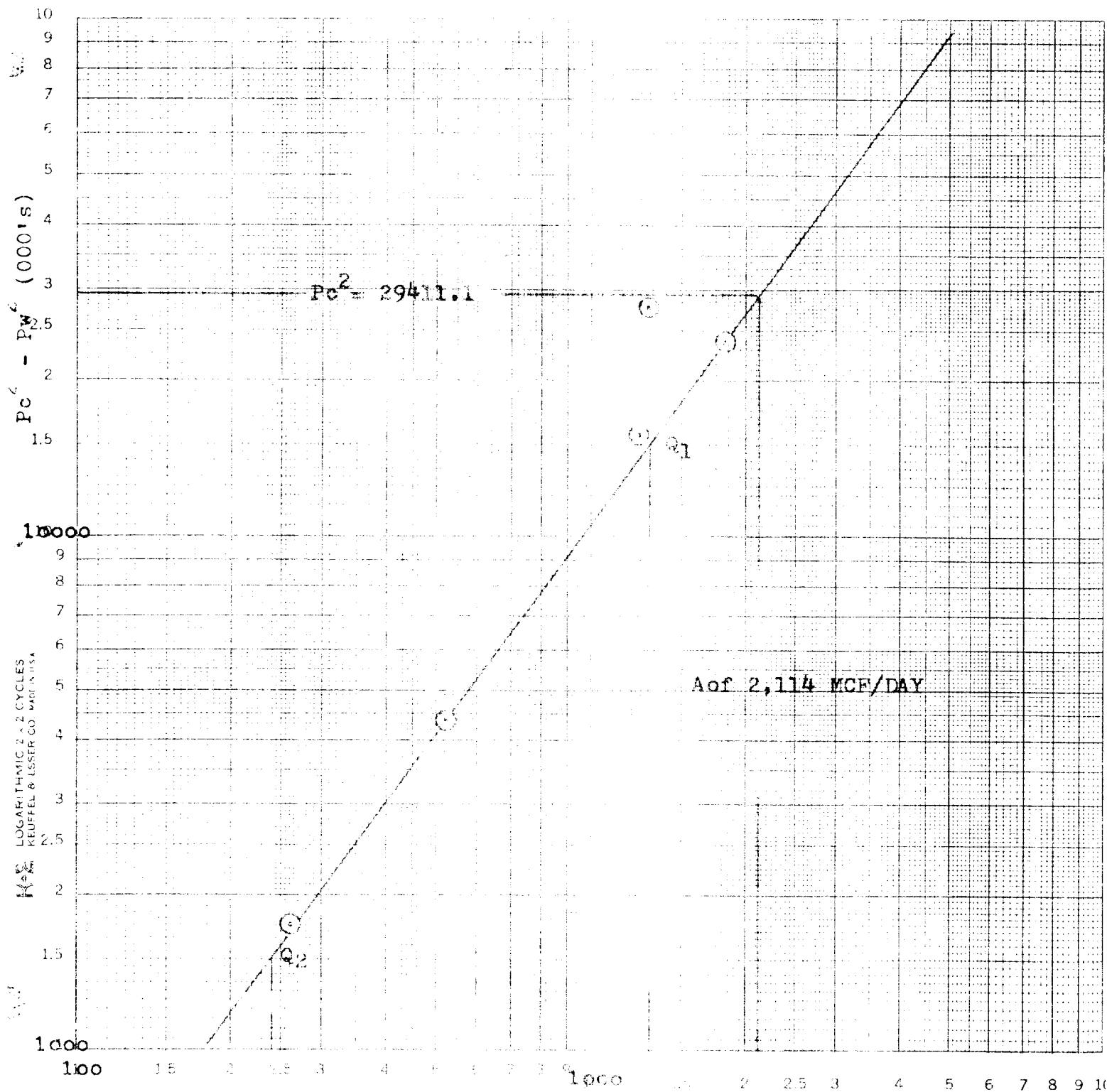
NO.	F ₁	Temp. °R	T _g	Z	One Liquid Hydrocarbon Bubble	Two Liquid Hydrocarbon Bubbles	Three Liquid Hydrocarbon Bubbles	Four Liquid Hydrocarbon Bubbles	Five Liquid Hydrocarbon Bubbles	Rate of Flow Q, Mscf/d
1	5423.2	29411.1			1.230	1.164				
2	6466.2	5258.3	27650.0	1761.1						
3	6180.2	5001.7	25016.9	4394.2						
4	4688.2	3696.7	13665.3	15245.8						
5	3043.2	2344.9	5499.0	23912.1						
6	1659.2	1290.5	1665.4	27745.7						

NO.	F ₁	Temp. °R	T _g	Z	One Liquid Hydrocarbon Bubble	Two Liquid Hydrocarbon Bubbles	Three Liquid Hydrocarbon Bubbles	Four Liquid Hydrocarbon Bubbles	Five Liquid Hydrocarbon Bubbles	Rate of Flow Q, Mscf/d
1	6635.2	S.I.P.			2.114	53.75°	.734			

Remarks: **BOTTOM-HOLE PRESSURES TAKEN FROM AN INSTRUMENT SET AT 11300 FT.**
THE WELL PRODUCED 1.4 bbls. of DISTILLATE AND 9.8 bbls. of H₂O.

Approved By: DAVIS SERVICES, INC.	Checked By: RICK PAGAN
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OPERATOR : Perry R. Bass
 LEASE : BIG EDDY UNIT
 WELL # : 92
 COUNTY : EDDY
 STATE : NEW MEXICO
 DATE : SEPTEMBER 11, 1982



Q = MCF/D
 Q1 LOG 1300 = 3.113941
 Q2 LOG 740 = 2.869211
 b = .734
 c = 53.750

NEW-TEX LAB

PHONE 505/393-3551

P. O. BOX 1161

611 W. SNYDER

HOBBS, NEW MEXICO 88240

ANALYSIS CERTIFICATE

CLIENT: ALCOHOL DISTILLERS ASSOCIATION
ADDRESS: 1000 N. 10TH ST.
CITY: ALBUQUERQUE, N.M. 87102
DATE: 8/27/81
TIME: 10:00 AM
ANALYST: J. J. KELLY

SAMPLE: 1000 N. 10TH ST.
SAMPLING METHOD: PERY, J. KELLY

ANALYSIS OF SAMPLE 1000 N. 10TH ST. (PERY, J. KELLY)

Component	Weight %	Volume %
NITROGEN	0.00	0.00
CARBON DIOXIDE	0.00	0.00
METHANE	0.00	0.00
ETHANE	0.00	0.00
PROPANE	0.00	0.00
ISOBUTANE	0.00	0.00
NORMAL BUTANE	0.00	0.00
ISOPENTANE	0.00	0.00
NORMAL PENTANE	0.00	0.00
HEXANES	0.00	0.00
HEPTANES	0.00	0.00
TOTAL	100.00	100.00

PROPANE 0.00% (0.00% of total)
ETHANE 0.00% (0.00% of total)

ISOBUTANE 0.00% (0.00% of total)
TOTAL 100.00%

Component	Weight %	Volume %
ISOBUTANE	0.00	0.00
ISOPENTANE	0.00	0.00
NORMAL PENTANE	0.00	0.00
HEXANES	0.00	0.00
HEPTANES	0.00	0.00

ANALYZED BY:

APPROVED BY:

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES (P_c or P_w)

Form C-122F
Adopted 9-1-65

FROM KNOWN BOTTOM HOLE PRESSURE (P_x or P_s)

COMPANY PERRY R. BASS WELL NO. 92 DATE 9-11-82

LOCATION: Big Eddy Unit Township Range

11300 11300 1.000 MIX .608 % CO₂ .575 1.146 1.146

GH 6870 Per 671 To 358

5th RATE

LINE	1	2	3	4	5	6	7	8
1	$T_w/(W.H. (R))$	534						
2	$T_s/(R.H. (R))$	647						
3	$T = (T_w + T_s)$	590.5	590.5					
4	Z (Per.)	.859	.868					
5	TZ	507.2	512.6					
6	GH/TZ	13.544	13.403					
7	c^2 (Table XIV)	1.662	1.653					
8	P_f or P_s	1659.2	1659.2					
9	P_f^2 or P_s^2	2752.9	2752.9					
10	$P_c^2 = P_f^2/es$ or $P_w^2 = P_s^2/es$	1656.6	1665.4					
11	P_c or P_w	1287.1	1290.5					
12	$P = \frac{P_w + P_s}{2}$ or $\frac{P_c + P_f}{2}$	1473.1	1474.9					
13	$P_f = (P/P_{cf})$	2.20	2.20					
14	$T_f = (T/T_{cf})$	1.65	1.65					
15	Z (Table XI)	.868	.868					

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES (P_w or P_w)

Form C-122F
Adopted 9-1-65

FROM KNOWN BOTTOM HOLE PRESSURE (P_b or P_b)

COMPANY PERRY R. BASS LEASE BIG EDDY UNIT WELL NO. 92 DATE 9-11-82

LOCATION: Unit L 11300 Section H 11300 Township L/H 1.000 Range G MIX .608

L 11300 H 11300 L/H 1.000 G MIX .608 % CO₂ .575 % N₂ 1.146 % H₂S

GH 6870 P_{cr} 671 T_{cr} 358

TABLE I & II

1st RATE 2nd RATE 3rd RATE 4th RATE

LINE	1	2	3	4	5	6	7	8
1	T_w (G.H. + B)	534	534	534	534	534	534	534
2	T_b (B.H. + B)	647	647	647	647	647	647	647
3	$T = \frac{T_w + T_b}{2}$	590.5	590.5	590.5	590.5	590.5	590.5	590.5
4	Z (Est.)	1.107	1.055	1.080	1.031	.918	.847	.837
5	TZ	653.7	623.0	637.7	608.8	562.7	500.2	494.2
6	GH/TZ	10.510	11.028	10.772	11.284	12.206	13.736	13.900
7	e^S (Table XIV)	1.483	1.512	1.498	1.527	1.581	1.674	1.4
8	P_f or P_s	6466.2	6466.2	6180.2	6180.2	4688.2	4688.2	3043.2
9	P_f^2 or P_s^2	41811.7	41811.7	38194.	38194.9	21979.2	21979.2	9261.1
10	$P_c^2 = P_f^2/e^S$ or $P_w^2 = F_s^2/e^S$	28192.4	27650.0	25501.9	25016.9	13905.7	13665.3	5499.0
11	P_c or P_w	5309.7	5258.3	5049.9	5001.7	3729.0	3696.7	2344.9
12	$P = \frac{P_w + P_s}{2}$ or $(\frac{P_s + P_f}{2})$	5887.9	5862.3	5615.1	5590.9	4208.6	4192.4	2694.1
13	$P_T = (P/P_{cr})$	8.78	8.74	8.37	8.33	6.27	6.25	4.02
14	$T_T = (T/T_{cr})$	1.65	1.65	1.65	1.65	1.65	1.65	1.65
15	Z (Table XI)	1.055	1.053	1.030	1.029	.918	.837	.837