

MULTIPOINT AND ONE POINT PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial FOUR POINT <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 7-10-82		RECEIVED 1980 PNL	
Company PENNZOIL Co.			Connection AIR NEW WELL		
Well WILDCAT			Formation WOLFCAMP		
Completion Date 7-8-82		Total Depth 11,400		Plug Back TD 11,350	
Elevation 3312.2 KB		Unit WINCHESTER FEDERAL		Office ARTESIA OFFICE	
Req. Size 4.50		Wt. 11.6		d 4.000	
Set At 11,390		Perforations: From 8849 To 9029		Well No. 1	
Req. Size 2.378		Wt. 4.7		d 1.995	
Set At 8774		Perforations: From OPEN To ENDED		Unit Sec. Twp. Rge. H 4 20S 28E	
Type Well - Single - Draddenhead - G.G. or G.O. Multiple SINGLE			Packer Set At 8774		County EDDY
Producing Thru TUBING		Reservoir Temp. °F 150 # 8939		Mean Annual Temp. °F 60°	
Baro. Press. - P <sub>a</sub> 13.2		State NEW MEXICO			
L 8939	H 8939	Gg 0.6717	% CO <sub>2</sub> .326	% N <sub>2</sub> 1.519	% H <sub>2</sub> S
Prover FLANGE		Meter Run 4.028			

FLOW DATA							TUBING DATA		B.H.P. DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	CHOKE	of Flow
51							3016	96	3000		48 HR 50MI
1.	4.00	X	1.500	600.	1.2	104	2735	80	2370	5/64	1 HR
2.	4.00	X	1.500	600.	2.1	100	2575	80	2420	7/64	1 HR
3	4.00	X	1.500	600.	5.8	90	2440	78	2385	9/64	1 HR
4	4.00	X	1.500	600.	21.0	76	2340	77	2290	13/64	1 HR
5.	4.00	X	1.500	700.	27.0	86	1753	63	1640	18/64	4 HR

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Fl	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>sp</sub>	Rate of Flow Q, Mcfd
1	11.1200	27.13	613.2	.9602	1.2199	1.0489	371
2	11.1200	35.88	613.2	.9636	1.2199	1.0500	493
3	11.1200	59.64	613.2	.9723	1.2199	1.0529	828
4	11.1200	113.48	613.2	.9877	1.2199	1.0600	1612
5	11.1200	138.77	713.2	.9759	1.2199	1.0630	1953

NO.	P <sub>t</sub>	Temp. °R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio	Mcl/Lbl.
1	.92	564	1.50	.909	9.6	
2	.92	560	1.49	.907	70:4 AT 60°	
3	.92	550	1.47	.902	Specific Gravity Separator Gas .670	XXXXXX
4	.92	533	1.42	.890	Specific Gravity Flowing Fluid XXXXX	
5	1.07	546	1.46	.885	Critical Pressure 668 P.S.I.A.	
					Critical Temperature 375 R	

NO.	P <sub>t</sub>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>t</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>
1	3821.3	3507.6	12303.3	2299.0
2	14602.3	3313.1	10976.6	3626.0
3		3151.9	9934.5	4668.0
4		3040.7	9245.9	5356.0
5		2316.6	5366.6	9236.0

$(1) \frac{P_t^2}{P_t^2 - P_w^2} = 2.7264$ 
 $(2) \left[ \frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 2.7264$

$AOF = Q \left[ \frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 4,394.9$

*Posted FD-2  
8-6-82  
Comp. + BK*

Absolute Open Flow <u>4,394.9</u> Mcfd @ 15.025		Angle of Slope $\theta$ <u>45.0</u>		Slope, n <u>1.000</u>	
Remarks:					
Approved By Commission:		Conducted By: DON BENNETT		Checked By:	
				Calculated By: BENNETT-CATHEY	