NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122 Revised 9-1-65

RECEIVED BY APR -4 1985 O. C. D. ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 3/7/85		
Company: TEXACO ~~USA~~ Producing Inc.			Connection: TO AIR			
Pool: Indian Basin Upper Penn			Formation: CISCO			Unit
Completion Date: 3-9-85	Total Depth: 8191		Plug Back TD: 8060	Elevation: 4295		Farm or Lease Name: IB 32 STATE
Csg. Size: 7.000	Wt.: 26.0	d: 6.276	Set At: 8060	Perforations: From 7802 To 7822		Well No.: I-Y
Tbg. Size: 2.875	Wt.: 6.5	d: 2.441	Set At: 7611	Perforations: From 0 To 0		Unit: M Sec.: 32 Twp.: 21S. Rge.: 24E
Type Well – Single – Bradenhead – G.C. or G.O. Multiple: SINGLE				Packer Set At: 7604		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 152 @ 7812		Mean Annual Temp. °F: 60.0	Baro. Press. – P_a: 13.2		State: NEW MEXICO
L: 7812	H: 7812	Gg: 0.633	% CO_2: 0.76	% N_2: 2.65	% H_2S: 0.07	Prover: 0 / Meter Run: 4.0 / Taps: FLANGE

NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	B.H.P. Press. p.s.i.g.	CHOKE	Duration of Flow
SI							1420		1771		72.0
1.	4.03	X	1.000	320	10.0	84	1420	0	1768	5/64	1.0
2.	4.03	X	1.000	300	26.0	96	1405	0	1750	8.64	1.0
3.	4.03	X	1.000	300	40.0	95	1030	0	1703	10/64	1.0
4.	4.03	X	1.000	300	56.0	98	520	0	1709	13/64	1.0
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	4.75	57.72	333.2	0.9777	1.2569	1.0258	346
2	4.75	90.24	313.2	0.9671	1.2569	1.0224	533
3	4.75	111.93	313.2	0.9680	1.2569	1.0225	662
4	4.75	132.44	313.2	0.9653	1.2569	1.0221	781
5							

NO.	P_r	Temp. °R	T_r	Z
1	0.50	544	1.51	0.950
2	0.47	556	1.54	0.957
3	0.47	555	1.54	0.956
4	0.47	558	1.55	0.957
5				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.

A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.

Specific Gravity Separator Gas 0.633 | XXXXXXXXXX

Specific Gravity Flowing Fluid XXXXX | 0.633

Critical Pressure 670 P.S.I.A. | 670 P.S.I.A.

Critical Temperature 360 R | 360 R

P_c 1463.4 P_c^2 2141

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	3173	1461	2134	7
2	3109	1447	2093	49
3	2945	1409	1985	156
4	2966	1414	1999	143
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 15.0136$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3.9012$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3045$

Post ID-2 9-5-86 Comp + BK

Absolute Open Flow 3045 Mcfd @ 15.025 | Angle of Slope θ 63.3 | Slope, n 0.503

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By: W A Baker III