

NEW MEXICO OIL CONSERVATION COMMISSION
 MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS

Form C-122
 Revised 9-1-65

DEC 10 1970

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 12-3-70		
Company Monsanto Company			Connection Transwestern		
Pool Lower Morrow			Formation Lower Morrow		
Completion Date 11-20-70		Total Depth 10,525	Plug Back TD 10,365	Elevation 4013 Gr	Farm or Lease Name Rock Tank Unit
Csg. Size 5 1/2	Wt. 17	d 4.892	Set At 10,405	Perforations: From 10,200 To 10,244	Well No. 4
Tbg. Size 2 3/8	Wt. 4.70	d 1.995	Set At 10,091	Perforations: From Open Ended To	Unit Sec. Twp. Rge. J 1 23-S 24-E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10,089	County Eddy
Producing Thru Tubing		Reservoir Temp. °F 160 @ 10,000'	Mean Annual Temp. °F	Baro. Press. - P _a 13.2	State New Mexico
L 10,222	H 10,222	G _g .617	% CO ₂	% N ₂	% H ₂ S
			Prover	Meter Run X	Taps F

NO.	FLOW DATA			TUBING DATA		CASING DATA		Duration of Flow	
	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2906	66	
1.	4.029	1.75	740	84	80	1771	72	85 Min	
2.	4.029	1.75	740	72	80	1962	72	60 Min	
3.	4.029	1.75	730	52	79	2218	74	35 Min	
4.	4.029	1.75	720	26	80	2540	74	35 Min	
5.									

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
2.	14.93	232.8	753.2	.9813	1.274	1.063	4619
3.	14.93	196.6	743.2	.9822	1.274	1.062	3901
4.	14.93	138.0	733.2	.9813	1.274	1.061	2733
5.							

NO.	P _r	Temp. °R	T _r	z	Gas Liquid Hydrocarbon Ratio		Mcf/bbl.
					A.P.I. Gravity of Liquid Hydrocarbons	53.4	
1.	1.12	540	1.48	.885	Specific Gravity Separator Gas	.616	XXXXXXX
2.	1.12	540	1.48	.885	Specific Gravity Flowing Fluid	XXXXX	.617
3.	1.11	539	1.47	.887	Critical Pressure	671	P.S.I.A.
4.	1.09	540	1.48	.888	Critical Temperature	365	R
5.							

NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	P _c	P _c ²	Equations	
							(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{8532}{4877}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4269$
1	3183	1912	3655	4877	2921	8532		
2	3901	2064	4609	3923				
3	4978	2300	5290	3242				
4	6519	2586	6687	1845				
5								

Absolute Open Flow 7107 Mcfd @ 15.025 Angle of Slope @ 57.5 Slope, n .636

Remarks: Started on High Rate - Anticipating Load Water Build-Up.

Approved By Commission: Noted 12-18-70 Conducted By: [Signature] Calculated By: [Signature] Checked By: