

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Other		Date: 9-13-78		STUD DATE: 7-28-78	
Company W. A. Moncrief, Jr. ✓		Connection To Air			
Pool Wildcat		Formation Morrow		Unit G	
Completion Date 9-13-78		Total Depth 11,258		Plug Back To 11,109	
Csg. Size 4 1/2		Wt. 11,210		Perforations: From 10789 To 10,807	
Thg. Size 2 3/8		Wt. 4.7		Perforations: From open To end	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packoff Set At 10,658		County Eddy	
Producing Thru Thg.		Reservoir Temp. °F 181 @ 10,658		Baro. Press. - P _a 13.2	
L 10,658		H 10,658		G _g .594	
		% CO ₂ .96		% N ₂ 1.90	
		% H ₂ S		Prover 6" Choke Nipple	
		Meter Run		Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	6" Positive Ck						3332				24 Hrs.
1.	1/8			2818		34	2818				1 hr.
2.	3/16			2270		42	2270				1 hr.
3.	7/32			1895		64	1895				1 hr.
4.	1/4			1795		60	1795				1 hr.
5.											

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ARTESIA, OFFICE

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor G _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mhd
1	.2618		2831.2	1.026	1.298	1.177	1162
2	.6101		2283.2	1.018	1.298	1.181	2174
3	.8419		1908.2	.9962	1.298	1.140	2368
4	1.112		1808.2	1.000	1.298	1.141	2978
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	4.21	494	1.40	.722	A.P.I. Gravity of Liquid Hydrocarbon	Deq.
2.	3.40	502	1.42	.717	Specific Gravity Separation	XXXXXXX
3.	2.84	524	1.48	.769	Specific Gravity Flooding	XXXXX
4.	2.69	520	1.47	.768	Critical Pressure	672 P.S.I.A.
5.					Critical Temperature	354 °R

P _c 3345.2 P _c ² 11190.4				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		2839.5	8062.8	3127.6
2		2315.3	5360.6	5829.8
3		1952.9	3813.8	7376.6
4		1882.1	3542.3	7648.1
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.463$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.463$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.357$

Post test
SD-34-18
11-3-78
PEH/EPB

Absolute Open Flow	4,357	Mcf/d @ 15.0°F	Scale of Slope	45	Slope, n	1.000
Remarks:						

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	R. E. Reston -EPNG	R. E. Reston	