Phone:(575) District II 811 S. First S Phone:(575) District III 1000 Rio Bra Phone:(505) District IV 1220 S. St F	azos Rd., Aztec, N 334-6178 Fax:(50	75) 393-0720 3210 75) 748-9720 IM 87410 05) 334-6170 Fe, NM 87505	E	inergy, l Oil Cor 1220	Min Re nsei S. 3	source	nc s D	d Natura Division is Dr.		MA		Form C-101 August 1, 2011 Permit 263907
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	3624 Oak Lawn Dallas, TX 7521		2							3. API Numb	er	9110
4. Property			roperty Na	ame oal Creek State	e 16					6. Well No.	001 H	
				7.	Surfa	ce Location						
UL - Lot F	Section 16	Township 23N	Range	11W Lot Idn		eet From 352	N/S	Line Feet Fr	rom 447	E/W Line	E County	SAN JUAN
				8. Propos	sed Bo	ottom Hole Lo	oca	tion				
UL - Lot E	E Section	Township 23N	Range	Lot Idn		Feet From 1407	N	and server a respectively server to the server of the serv	From 3	E/W Line	County	San Juan
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11. Work Ty	^{pe} New Well	12. Well Type GAS	6	13. Cable/Rotan	у			14. Lease Type State		15. Ground Le 62	evel Elevation	
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Depth to Gr				Distance from no							earest surface	water
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_				21. Proposed								
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				22. Proposed	Blow	out Preventio	on F	Program				
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I further certify I have complied with 19.15.14.9 (A) NMAC and/or 19.15.14.9 (B) NMAC , if applicable.	
Signature:	Brandon D-M
Printed Name: MUTT STRILKIEr	Approved By:
Title: Vice Prisident of Land	Title: INE SUDANISON
Email Address: must strickly @ moresources. com	Approved Date: 3 - 20 - 9 Expiration Date: 3 - 20 - 20
Date: 2/18/14 Phone:405-300-	Conditions of Approval Attached
(JO)	SEE ATTACHED NMOCD

CONDITIONS OF APPROVAL

DISTRICT I State of New Mexico Form C-102 1625 N. French Dr., Hobbs, N.M. 88240 Energy, Minerals & Natural Resources Department Revised August 1, 2011 Phone: (575) 393-6161 Fax: (575) 393-0720 Submit one copy to appropriate DISTRICT II OIL CONSERVATION DIVISION District Office 811 S. First St., Artesia, N.M. 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 1220 South St. Francis Dr. DISTRICT III Santa Fe, NM 87505 1000 Rio Brazos Rd., Aztec, N.M. 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 DISTRICT IV AMENDED REPORT 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462 WELL LOCATION AND ACREAGE DEDICATION PLAT ² Pool Code ³ Pool Name API Number US. 97232 BASIN MANCOS GAS POOL ⁶ Well Number Property Code ⁵Property Name 2 COAL CREEK STATE #16 1 H OGRID No. ⁸Operator Name ⁹ Elevation JUNIPER RESOURCES EXPLORATION COMPANY, LLC 6210 371654 ¹⁰ Surface Location Feet from the North/South line East/West line UL or lot no. Section Township Lot Idn Feet from the Range County P 16 23-N 11 - W352 SOUTH 447 EAST SAN JUAN ¹¹ Bottom Hole Location If Different From Surface UL or lot no. Section Township Lot Idn Feet from the North/South line Feet from the East/West line Range County WEST F 16 23-N 1407 NORTH 330 SAN JAUN 11-W ² Dedicated Acres ¹³ Joint or Infill ¹⁴ Consolidation Code 15 Order No. BMGP = SEC 16 640 ACRESNO ALLOWABLE WILL BE ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED FD. GLO "1942" BC OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DIVISION 16 S89°24'01"E 2644.05 '1942" 17 OPERATOR CERTIFICATION I hereby certify that the information contained herein is true and complete to the best of my knowledge and BASIS OF BEARING: belief, and that this organization either owns a working interest or unleased mineral interest in the DETWEEN FOUND MONUMENTS AT THE SOUTHEAST CORNER AND THE EAST QUARTER CORNER OF SECTION 16, TOWNSHIP 23 NORTH, RANGE 11 WEST, N.M.P.M. SAN JUAN COUNTY, NEW MEXICO. a working interest of attacks in the location or has a right to drill this well at this location or has a right to drill this well at this location pursuant to a contract with an owner of such a mineral or a working interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the -2621.35 407 LINE BEARS: N 02'38'13" E A DISTANCE OF 2627.16 FEET AS MEASURED BY G.P.S. LOCAL GRID NAD83. division BOTTOM HOLE 1407' FNL 330' FWL SEC. 16 330' VA-2966 LATITUDE: 36°13.8275' N S03°10'13"W LONGITUDE: 108°01.0218' W NAD27 Signature Matt STRICKLE LATITUDE: 36.230470° N Printed Name LONGITUDE: 108.017653° W Mutr. STrickler Dynprosour E-mail Address NAD83 FD. GLO "1942" BC FD. GLO SURVEYOR CERTIFICATION 1942" BC SURFACE STATE 352' FSL 447' FEL SEC. 16 I hereby certify that the well location shown on this plat LATITUDE: 36°13.2456' N was plotted from field notes of actual surveys made by 6 LONGITUDE: 108°00.1348' W me or under my supervision, and that the same is true 09°12' E and correct to the best of my belief. NAD27 2627 LATITUDE: 36.220772° N JANUARY 23, 2019 LONGITUDE: 108.002869° W RUSSE Date of Survey CLEEN ŵ NAD83 DECLINA m HW METC Signature and Seal of LANDING POINT 30 330' FSL 1185' FEL SEC, 16 N02° MAGNETIC LATITUDE: 36°13.2434' N 1185 15703 NORTH/ LONGITUDE: 108°00.2852' W 447 NAD27 VA-2959 m PROFESSION LATITUDE: 36.220734° N o. LANDING PT BORE) LONGITUDE: 108.005375° W â GLEN W. RUS FD. GLO NAD83 Certificate Number 15703 352 "1942" BC 330 FD. GLO "1942" BC N89'18'37"W 2666.74

APD Drilling Program

JUNIPER RESOURCES EXPLORATION CO. LLC.

3333 Lee Pkwy. Suite 210 Dallas, TX 75219

COAL CREEK STATE 16 1H

Surface Location: 352' FSL & 447' FEL Section 16, T23N, R11W Proposed GL Elev = 6210' Lat. = 36.220772° N Long. = 108.002869° W NAD83 San Juan County, New Mexico

Proposed Top of Production Location: 352' FSL & 447' FEL Section 16, T23N, R11W Proposed Bottom Hole Location (Pilot Hole): 352' FSL & 447' FEL Section 16, T23N, R11W Proposed Bottom Hole Location (Landing Point): 330' FSL & 1185' FEL Section 16, T23N, R11W Proposed Bottom Hole Location (Lateral #1): 1407' FNL & 330' FWL Section 16, T23N, R11W San Juan County, New Mexico

Drilling program written in compliance with onshore Oil and Gas Order No. 1 (III.D.3, effective May 2007) and Onshore Order No. 2 Dated November 18, 1988

1. ESTIMATED TOPS OF GEOLOGICAL MARKERS

Depths	are referenced to	GL of 6,210	ft
Formation	TVD (ft)	MD (ft)	Subsea (ft)
Kirtland Shale	0	0	6,219
Fruitland Coal	225	225	6,012
Pictured Cliffs Ss.	397	397	5,840
Lewis Shale	530	530	5,707
CliffHouse Ss.	1,070	1,070	5,167
Menefee Fn.	1,649	1,649	4,588
Point Lookout Ss.	2,742	2,742	3,495
Mancos Shale	2,895	2,895	3,342
Mancos Silt	3,472	3,472	2,765
Mancos 2A	3,722	3,722	2,515
El Vado	3,768	3,768	2,469
Gallup Fn.	3,892	3,892	2,345
Juana Lopez	4,309	4,309	1,928
Dakota	4,742	4,742	1,495

Pilot Hole TD	5,087	5,087	1,150	
Lateral TD	3,830	9,406	2,406	

Note: Geologic markers will be updated based on drilling and geology operations

Drilling Plan

Drill 17 ½" hole to 200' then set 13 3/8" casing. Surface casing may be preset before moving in the drilling rig. Drill 12 ¼" intermediate hole to 2,900' then set 9 5/8" casing. Drill 8 3/4" Pilot hole with fresh water potassium chloride mud from 2,900' MD to approximately 5,087'. Logs will be run to determine exact landing point for the horizontal wellbore.

The wellbore will be plugged back with cement to above kick off point (KOP) #1 approximately 3,160' MD/TVD. The plug will be dressed off and an 8 ³/₄" kick off assembly will be run to build the curve at 9-10 degrees per 100' to landing point at 89.49 degrees and 315 deg azimuth, 4,500' MD/ 3,785'TVD.

The lateral section will be drilled continuing with the 8 ³/₄" hole and holding an 89.49 deg inclination until TD is reached.

The Bottom hole location will be in a legal location at 9,406' MD / 3,830' TVD at 1407' FNL & 330' FWL of section 16. A total of 4,966' of horizontal hole will be drilled.

2. ESTIMATED DEPTHS OF POTENTIAL WATER, OIL, GAS & OTHER MINERAL BEARING ZONES

Depths	are referenced to	GL of 6,210 f	t
Formation	TVD (ft)	MD (ft)	Substance
Kirtland Shale	0	0	
Fruitland Coal	225	225	Water/Gas
Pictured Cliffs Ss.	397	397	Gas
Lewis Shale	530	530	Gas
CliffHouse Ss.	1,070	1,070	Gas
Menefee Fn.	1,649	1,649	Water/Gas
Point Lookout Ss.	2,742	2,742	Water
Mancos Shale	2,895	2,895	Oil/Gas
Mancos Silt	3,472	3,472	Oil/Gas
Mancos 2A	3,722	3,722	Oil/Gas
El Vado	3,768	3,768	Oil/Gas
Gallup Fn.	3,892	3,892	Oil/Gas
Juana Lopez	4,309	4,309	Oil/Gas
Dakota	4,742	4,742	Oil/Gas
Pilot Hole TD	5,087	5,087	
Lateral TD	3,830	9,406	Oil/Gas

Possible Aquifers: None

Oil Shale: None Expected.

Oil & Gas: Primary objective is the Mancos formation encountered first at 2,895' TVD. Landing point will be in the El Vado section of the Mancos at 3,786'TVD.

Protection of oil, gas, water, or other mineral bearing formations: Protection shall be accomplished by setting surface casing below base of possible aquifer and cementing surface casing to surface.

Intermediate casing will be set at 2,900' TVD and cemented to surface.

3. PRESSURE CONTROL

The Operator's minimum specifications for blowout prevention equipment and diverter systems to be used, including size, pressure rating, configuration and the testing procedure and frequency. Blowout prevention equipment must meet the minimum standards outlined in Order 2.

BOP equipment and accessories will meet or exceed BLM requirements outlined in 43 CFR Part 3160.

The working pressure of all BOPE shall exceed the anticipated surface pressure to which it may be subjected, assuming a partially evacuated hole with a pressure gradient of 0.22 psi/ft.

Bottom Hole pressure = 5087' TVD x 0.38 psi/ft = 1933 psi (based on measured offset bottom hole pressures).

Maximum Surface Pressure = 1933 psi - (5087' TVD x .22 psi/ft) = 1933psi - 1119 psi = 814 psi less than 2000 psi working pressure.

Therefore 2000 psi BOPE system required.

A 2000 psig double ram hydraulic BOP will be used (see attached diagram) accessories to the BOP will meet BLM requirements for a 2000 psig system, in accordance with Onshore Order #2 (111.A well requirements).

The accumulator system capacity will be sufficient to close all BOPE with a 50% safety factor. Fill line, kill line and line to the choke manifold will be 2".

BOPs will be function tested every 24 hours and will be recorded on an IADC log. Accessories to the BOPE will include upper and lower Kelly cocks with handles with a stabbing valve to fit drill pipe on the floor at all times, string float at bit, 3000 psig choke manifold with 2" adjustable and 2" positive chokes, and pressure gauge.

All BOP equipment will be hydraulically operated with controls accessible both on the rig floor.

The wellhead BOP equipment will be nippled-up on the 13 3/8" x 13 5/8" 2,000 psi WP casing head prior to drilling out from under surface casing. All ram preventers and related equipment will be tested to 2,000 psi for 10 minutes. Annular preventers will be tested to 50% of rated working pressure for 10 minutes. Surface casing will be tested to 70% of internal yield pressure. All preventers and surface casing will be tested before drilling out of surface casing. BOP equipment will be tested every 14 days, after any repairs are made to the BOP equipment, and after the BOP equipment is subjected to pressure. Annular preventers will be functionally operated at least once per week. Pipe rams will be activated daily and blind rams shall be activated each trip or at least weekly. The New Mexico Oil & Gas Conservation Commission and the BLM will be notified 24 hours in advance of testing of BOPE.

4. CASING AND CEMENTING PROGRAM

The proposed casing and cementing program has been designed to protect and/or isolate all usable water zones, potentially productive zones, lost circulation zones, abnormally pressured zones and any prospectively valuable mineral deposits. Any isolating medium other than cement shall receive approval prior to use.

Casing setting depth shall be calculated to position the casing seat opposite a competent formation which will contain the maximum pressure to which it will be exposed during drilling operations.

Included below is the Operator's proposed casing program which includes size, grade, weight, type of threading and coupling and setting depth for each string and its condition. Minimum design criteria and hole sizes are also included herein.

Casing	Depth (MD)	Hole Size	Csg Size	Weight	Grade	Coupling	Condition
Surface	0' - 200'	17 1/2"	13 3/8"	54.5 ppf	J or K55	STC	New
Intermediate	0' - 2,900'	12 1/4"	9 5/8"	36 ppf	J or K55	STC	New
Production	0' - 9,406'	8 3/4"	5 1/2"	20 ppf	P-110	LTC/BTC	New

	Casing	g String		Casing St	trenght Pr	roperties	Minimun	n Design	Factors
Size	Weight	Grade	Coupling	Collapse (psi)	Burst (psi)	Tensile (klbs)	Collapse	Burst	Tension
13 3/8"	54.5 ppf	J55	STC	1,130	2,730	514	1.125	1.1	1.2
9 5/8"	36 ppf	J55	STC	2,020	3,520	394	1.125	1.1	1.2
5 1/2"	20 ppf	P110	BTC	7,460	12,640	667	1.125	1.1	1.2

Casing strings below the conductor casing will be tested to .22 psi per foot of

casing string length or 1500 psi, whichever is greater, but not to exceed 70% of the minimum internal yield.

Surface casing shall have a minimum of 1 centralizer per joint on the bottom three (3) joints, starting with the shoe joint for a total of (4) minimum centralizers. Centralizers will be placed 10' above the shoe on the shoe joint, on the 1st, 2nd and 3rd casing collars.

The intermediate casing will be centralized using 1 centralizer the first 6 jts and then spaced +/- 1 centralizer / 4 jts through the remainder of the cement column.

The production casing will be centralized using 1 centralizer the first 6 jts and then spaced +/- 1 centralizer per 3 joints through the curve and into the intermediate casing.

*Surface casing maybe preset with a preset rig (MOTE).

The proposed cementing program is as follows:

Surface Casing Single Stage Job - (0-200'MD/TVD):

Excess – 50% over gauge hole – 17-1/2" hole and 13-3/8" casing (0.694638 ft3/ft) Top of Cement – Surface

Lead #1 - (0' – 200'): 176 sx – 15.8 ppg, conventional cement containing: HALCEM [™] CEMENT – PREMIUM CEMENT Calcium Chloride Pellet – Accelerates Thickening Time – 2.0% Poly-E-Flake – Lost Circulation Control Agent – 0.125 lbs/sx Yield – 1.175ft3/sx Water requirement – 5.14 gal/sx. Compressive strength: 24 hr – 2000 psi+ Total sacks of cement pumped = 170

Intermediate Casing Single Job - (0-2,900'MD/2,900'TVD): Excess - 50% over gauge hole - 12-1/4" hole and 9-5/8" casing (0.3132 ft3/ft)

Top of Cement – Surface.

Lead #1 - (0 - 2,900'): 1048 sx - 13.5 ppg, conventional cement containing: VARICEM [™] - Cement Kol-Seal - Lost Circulation Control Agent - 5 lbs/sx Poly-E-Flake - Lost Circulation Control Agent - 0.125 lbs/sx Yield - 1.30 ft3/sx Water requirement - 5.64 gal/sx. Compressive strength: 24 hr - 1000 psi+

Total sacks of cement pumped = 1048

Cement volumes are minimums and may be adjusted based on hole conditions.

Production Casing Single Stage Job – (2.700'MD – 9.518'MD/ 2.700'- 3.829'TVD): Excess – 30% over gauge hole – 8-3/4" hole and 5-1/2" casing (0.2526 ft3/ft) Top of Cement – 2700' MD (200' inside intermediate casing).

Lead #1 - (2,700' - 9,406') - 6,706': 1631 sx - 13.3 ppg, conventional cement containing: EXTENDACEM [™] - Cement Yield - 1.35 ft3/sx Water requirement - 5.94 gal/sx. Compressive strength: 24 hr - 1000 psi+ <u>Total sacks of cement pumped = 1658</u> Cement volumes are minimums and may be adjusted based on hole conditions.

Plug Back Cement - (2900' - 3900'MD/TVD):

Excess – 50% over gauge hole – 8-3/4" hole (0.4176 ft3/ft) Top of Cement – 200' above KOP Cement will be place in 2 equal plugs approximately 500' in length (312 sx each)

Lead #1 - (2900' - 3900') -1000': 624 sx - 15.8 ppg, conventional cement containing: HALCEM ™ CEMENT - PREMIUM CEMENT Poly-E-Flake - Lost Circulation Control Agent - 0.125 lbs/sx Yield - 1.175ft3/sx Water requirement - 5.14 gal/sx. Compressive strength: 24 hr - 2000 psi+ Total sacks of cement pumped = 624 sx

Actual volumes will be calculated and determined by conditions onsite. All cement slurries will meet or exceed minimum BLM and New Mexico Oil Conservation Division requirements. Slurries used will be the slurries listed above or equivalent slurries depending on service provider selected. Cement yields may change depending on slurries selected.

All waiting on cement times shall be a minimum of 8 hours or adequate to achieve a minimum of 500 psi compressive strength at the casing shoe prior to drilling out.

Other Cementing Notes:

- Pea Gravel or other material shall not be used to fill up around the surface casing in the event cement fall back occurs.
- The surface casing shall in all cases be cemented back to surface. In the event cement does not circulate to surface or fall back of the cement column occurs, remedial cementing shall be done to cement the casing back to surface. No more than the top 100' will be remediated with 1" line if fall back occurs. Anything more than 100' will require plan approval to remediate.
- If returns are lost and/or cement is not brought to surface and no fallback occurs, a cement bond log (CBL) will
 be required to determine the quality of the job prior to drilling ahead (see OO2).

- Top plugs shall be used to reduce contamination of cement by displacement fluid. A bottom plug or other acceptable technique, such as a pre-flush fluid, inner string cement method, etc. shall be utilized to help isolate the cement from contamination by the mud fluid being displaced ahead of the cement slurry.
- Production casing will be cemented.

5. DRILLING FLUIDS PROGRAM

Interval (MD)	Hole Section	Hole Size	Туре	MW	VIS	FL	PV	YP	PH
0'- 200'	Surface	17-1/2	FW/Gel	8.4-9.0	32-44	NC	8	12	9
200' - 2,900'	Intermedia te	12-1/4	KCL Polymer	8.4-9.5	38-42	6	10	14	9.5
2,900' - 5,087'	Pilot	8-3/4"	KCL Polymer	9.0-10.0	38-42	6-10	10-14	7-8	9.5
2,900' - 9,406'	Curve/ Lateral	8-3/4"	KCL Polymer	9.0-10.0	45-50	10-15	10-14	7-8	9.5

Sufficient weighting material will be on hand to weight mud up to 10.5 PPG, if required.

The formula for weight up with barite is listed below:

Sacks of Barite per 100 bbl of mud = $1470 \times (W2 - W1) \div (35 - W2)$

Where; W1 = current mud weight

W2 = new mud weight

Sacks = 1470 x (10.5 - 8.4)/ (35-10.5) = 126 sx * 5 (500bbls minimum) = 630sx

Pason Pit Volume Totalizer (PVT) equipment (or equilvant) will be on each pit to monitor pit levels. A trip tank equipped with a Pason PVT will be used to monitor trip volumes.

A closed-loop system will be used to recover drilling fluid and dry cuttings in both phases of the well and on all hole intervals, including fresh water and oil-based operations. Above-ground tanks will be utilized to hold cuttings and fluids for rig operations. A frac tank will be on location to store fresh water. Waste will be disposed of properly at an EPA-approved hazardous waste facility. Fresh water cuttings will be disposed of as outlined is surface use plane location will be lined in accordance with the Surface Use Plan of Operations.

6. TESTING, LOGGING AND CORING

- a) Drill stem testing none anticipated
- b) Coring none anticipated
- c) Mud Logging Mud loggers will be operational from 2,900' of the pilot hole to TD of the horizontal hole.
 - a. Gas detecting equipment will be installed and operational and hydrocarbon gas will be monitored for pore pressure changes from base of surface casing to TD.
 - b. Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume.
- d) Logging see below:

Open hole (pilot hole)

Triple Combo (2,900' to TD – GR to surface) DiPole Sonic (Top Mancos Sh. To TD) NMR (contingent – Top Mancos Sh. To TD) Dielectric Scanner (Top Mancos Sh. To TD) Image Log (Top Mancos Sh. To TD)

Minimum logging requirements for the entire well shall consist of a calibrated gamma ray (GR) log scaled in API units from total measured depth to surface, with a repeat section. Maximum logging speed 3,600 feet/hour in open hole and 2,000 feet/hour in cased hole. An MWD GR log is sufficient for this requirement in the curved and lateral portions of the well.

Minimum logging requirements above the kick off point (KOP) shall consist of:

- 1. Multiple depth-of-investigation resistivity log from surface casing to the KOP, and
- 2. Compensated density-neutron logs over potential hydrocarbon producing zones or,
- 3. A cased hole pulsed neutron log if there are open hole compensated density-neutron, gamma ray, and multiple depth-of-investigation resistivity logs (such as medium and deep induction and shallow laterlog, or array induction logs) suitable for calibration within one-half mile. The pulsed neutron log should be run from KOP to the base of surface casing no faster than 1,800 feet/hour.

BLM shall be provided with a directional survey to establish the location of the horizontal lateral and bottom of the well including the surface reference, inclination, horizontal angle, reference, and direction turned. If reduced data are provided, the algorithm, datum, and projection should also be provided.

Submission of digital logging data shall be in Log ASCII Standard (LAS) file format.

Cased Hole

CBL/CCL/GR will be run after the drilling of the well has been completed and as the start of the completion process. The CBL will confirm the quality of the cement bond and the actual TOC. If either of these two data points were not satisfactory per BLM, State and standard procedure, remedial cement work, if required, will be performed after consultation and approval of a plan from both the BLM and State agencies.

A cement bond log shall be run if the well is cased for production, injection, or disposal. The logged interval should extend from at least 50 feet below the KOP, if practical, to 200 feet above the top of cement. In no case shall the cement bond log begin above the KOP.

7. ABNORMAL PRESSURES & HYDROGEN SULFIDE

Normal to subnormal pressure gradient to TD.

MASP and casing design parameters determined using 0.38 psi/ft.

Bottom Hole pressure = 5087' TVD x 0.38 psi/ft = 1933 psi (based on measured offset bottom hole pressures).

Maximum expected BHP @ TD of pilot hole at 5087' TVD: 1933 psi

Maximum expected BHT @ 5087' TVD: ~160⁰ F

No hydrogen sulfide gas is anticipated, however, if H_{2S} is encountered, the guidelines in Onshore Order No. 6 will be followed.

8. OTHER FACETS OF PROPOSED OPERATION & ANTICIPATED START DATE

Directional Plans: Horizontal directional well, directional plans attached.

Completion: Completion design will be dependent on open-hole log evaluation from the pilot hole and the actual horizontal section drilled. Generally, the completion will consist of a plug and perf hydraulic fracturing operation consistent with best practices in the same area of the San Juan Basin. The frac job will likely consist of between 25 and 50 stages. Each stage will consist of approximately 300,000 lbs of 20/40 sand and 3,000 bbls of water. Pumping rates will be dependent on surface treating pressures but should be around 70 bpm down 5 ½" casing. All fracturing fluids will be water based and contain nitrogen foam. After the frac job, plugs will be drilled out within 10 days and production tubing will be run. Production tubing is expected to be 2 3/8" or 2 7/8".

Timing: Drilling is estimated to commence in late June, or early July 2019 depending on rig availability. The drilling rig has been identified and timing will depend on current operations for other Operators. It is anticipated that the drilling of this well will take 14-20 days and completion operations will begin within 30 days of rig release depending on fracture treatment schedules with various pumping service companies.

CLOSED-LOOP SYSTEM DESIGN PLAN

The closed-loop system will consist of a series of temporary above-ground storage tanks and/or haul-off bins suitable for holding the cuttings and fluids from drilling operations. The closed loop system will not entail temporary pits, below-grade storage tanks, below-grade sumps, or drying pads.

Design considerations include:

- The closed-loop system will be signed in accordance with 19.15.17.11 NMAC
- The closed-loop system storage tanks will be of adequate volume to ensure confinement of all fluids and provide sufficient freeboard to prevent uncontrolled releases.
- Topsoil will be salvaged and stored for use in reclamation activities
- The closed-loop system storage tanks will be placed in bermed secondary containment sized to contain a minimum of 110% of the volume of the largest storage tank.

CLOSED-LOOP SYSTEM OPERATING & MAINTENANCE PLAN

The closed-loop system will be operated and maintained to contain liquids and solids; minimize the amount of drilling fluids and cuttings that require disposal; maximize the amount of drilling fluid recycled and reused in the drilling process; isolate drilling wastes from the environment; prevent contamination of fresh water; and protect public health and the environment.

Operation and maintenance considerations include:

- Fluid levels will be maintained to provide sufficient freeboard to prevent over-topping.
- Visual inspections will be conducted on a daily basis to identify any potential leaks and to ensure that the closedloop system storage tanks have sufficient freeboard to prevent over-topping.
- Only drilling fluids or cuttings intrinsic to, used by, or generated from, drilling operations will be stored in the closed-loop system storage tanks. Hazardous waste, miscellaneous solid waste, and/or debris will not be stored in the storage tanks.
- The OCD District Office will be notified within 48 hours of discovery of a leak in the closed-loop drilling system. If
 a leak is discovered, all liquid will be removed within 48 hours and the damage repaired.

CLOSED-LOOP SYSTEM CLOSURE PLAN

The closed-loop system will be closed in accordance with 19.15.17.13 NMAC. Closure considerations include:

- Drilling fluids will be recycled and transferred to other permitted closed-loop systems or returned to the vendor for reuse, as practical.
- Residual fluids will be pulled from the storage tanks, mixed with saw dust or similar absorbent material, and disposed of at Industrial Ecosystem, Inc. waste disposal facilities.
- Remaining cuttings or sludges will be vacuumed from the storage tanks and disposed of at the Envirotech, Inc and/or Industrial Ecosystem, Inc. waste disposal facilities.
- Storage tanks will be removed from the well location during the rig move.
- The well pad will be reclaimed and seeded in accordance with subsections G, Hand I of 19.15.17.13 NMAC.

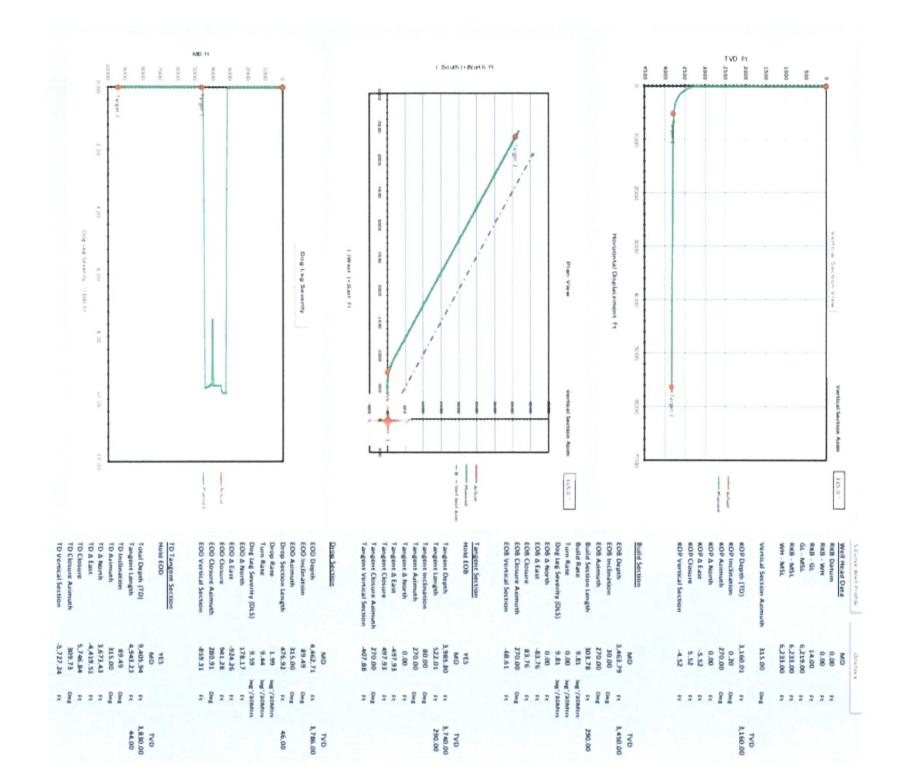


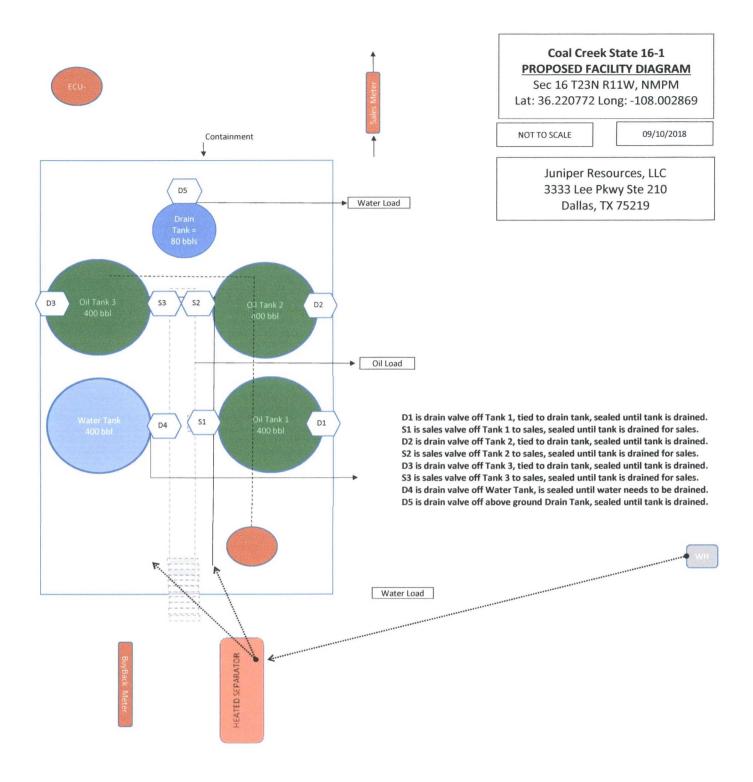
COAL CREEK STATE 16-1 SEC 16, T23N, R11W

PROPOSED DIRECTIONAL PLAN 9/10/2018

- #	# 158	a ANS QA	100			10.101.12	00.21010	10.0311	20.0	70.	141.000	0,141.0
		MD (ft) IN	INCL.	3	TVD (ft)	IVDSS (ft)		E/-W (ft)	DLS (100ft)		AZIM°	Vert Sect (ft)
	KB	0.00	00.00	0.00	0.00	-6233.00	0.00		0.00	00.00	0.00	0.00
1 1	1	00.00	0.00	00.00	0.00	-6233.	0.00	0.00		0.00	0.00	0.0
	2	60.00	0.00	270.00	60.00			0.00	0.01	0.00	270.00	0.00
	0	120.00	0.01	270.00	120.00	-6113.00	0.00	-0.01		0.01	270.00	0.0
	- 10		0.02	270.00	240.00			-0.03		0.03	270.00	0.0
	9		0.02	270.00	300.00	1		-0.05	0.01	0.05	270.00	0.0
	7		0.02	270.00	360.00	Ľ		-0.07		0.07	270.00	0.0
	00		0.03	270.00	420.00			-0.10		0.10	270.00	0.0
+	2 0F		0.03	2 2	540 00			-0.15		0.15	270.00	0.1
	11		0.04	270.00	600.00			-0.20		0.20	270.00	0.1
	12		0.04	270.00	660.00	-5573.00		-0.24	0.01	0.24	270.00	0.1
	13		0.05	270.00	720.00			-0.29		0.29	270.00	0.2(
	14		0.05	270.00	780.00			-0.34		0.34	270.00	0.2
	15		0.05	270.00	840.00	'	0.00	-0.39		0.39	270.00	0.2
	16		0.06	270.00	900.006			-0.45		0.45	270.00	0.3
	17		0.06	270.00	960.00	1		-0.51		0.51	270.00	0.3
	10		0.00	00.072	100000			1.5.0-		10.0	00.072	0.4
	50		0.07	270.00	1140 00	00 2605-		-0.04	10.0	0.72	270.00	0.5
	21		0.08	270.00	1200.00			-0.80		0.80	270.00	0.5
	22		0.08	270.00	1260.00	-4973.00		-0.88		0.88	270.00	0.6
	23		0.08	270.00	1320.00	-4913.00	0.00	-0.96		0.96	270.00	0.6
	24		60.0	270.00	1380.00	-4853.00		-1.05		1.05	270.00	0.7
	25		0.09	270.00	1440.00	-4793.00		-1.15		1.15	270.00	0.8
	97		0.09	00.072	1500.00	-4/33.00		1.24		47.T	00.072	0.0
	17		0.10	00.072	1560.00	46/3.00		-1.34 1 AE		1.34	00.072	0.9
	50		110	270.00	1680.00	4553 00		-1.56	10.01	1.56	270.00	1.1
	30		0.11	270.00	1740.00	ľ		-1.67		1.67	270.00	1.1
	31		0.11	270.00	1800.00	ľ		-1.79	0.01	1.79	270.00	1.2
	32		0.12	270.00	1860.00			-1.91		1.91	270.00	1.3
	33		0.12	270.00	1920.00	-4313.00		-2.04		2.04	270.00	1.4
	35		0.13	00.072	00.040 00	-4193.00		UE C-	T0.0	017.7	270.00	9 L
	36		0.13	270.00	2100.00	-4133.00		-2.44		2.44	270.00	1.7
	37		0.14	270.00	2160.00	-4073.00		-2.58	0.01	2.58	270.00	1.8
	38		0.14	270.00	2220.00	-4013.00		-2.72		2.72	270.00	1.92
	39		0.14	270.00	2280.00	-3953.00		-2.87		2.87	270.00	2.0
	40		0.15	00.0/2	2400.00	1		-3.02		3.02	270.00	1.7
	42		0.16	270.00	2460.00	-3773.00		-3.34		3.34	270.00	2.3(
	43		0.16	270.00	2520.00	ľ		-3.51	0.01	3.51	270.00	2.4
	44		0.16	270.00	2580.00	'		-3.68		3.68	270.00	2.6
	45		0.17	270.00	2640.00	-3593.00		-3.85		3.85	270.00	2.7
	46		0.17	270.00	2700.00	-3533.00		4.03		4.03	270.00	2.8
	41		0.17	00.072	2,760.00	-34/3.00		-4.21	10.0	4.21	270.00	2.7
	49		0.18	270.00	2880.00	-3353.00		-4.58		4.58	270.00	3.2
	50		0.19	270.00	2939.99	-3293.01	0.00	-4.77		4.77	270.00	3.3
	51		0.19	270.00	2999.99	-3233.01		-4.97		4.97	270.00	3.5
	52		0.19	270.00	3059.99	-3173.01		-5.17		5.17	270.00	3.6
VOD 3160	53		0.20	00.072	3170 08	-3113.01				5.38	2/0.00	3.8
	55		8.05	270.00	3239.71	-2093.29		-11.94	9.81	11.94	270.00	4.8
	56		13.93	270.00	3298.59	-2934.41		-23.37		23.37	270.00	16.5
	57		19.82	270.00	3355.98	-2877.02		-40.76		40.76	270.00	28.8
1 0000	58		25.70	270.00	3411.28	-2821.72	0.00	-63.94		63.94	270.00	45.2
EUB 3403./	PC 09		UE LE	00.072	3403.92	-2719 61		-17653		176 53	270.00	7 68
	61		43.05	270.00	3559.22	-2673.78		-165.19	9.58	165.19	270.00	116.8
	62		48.79	270.00	3600.94	-2632.06		-208.24		208.24	270.00	147.2
	63		54.54	270.00	3638.14	-2594.86		-255.24		255.24	270.00	180.48
	64		60.29	270.00	3670.44	-2562.56		-305.74	6	305.74	270.00	216.19
+	65	3,840.00	71.78	270.00	3719.10	-2535.48	0.00	-359.20	5 of	415.11	270.00	293.5
	67		77.53	270.00	3734.97	-2498.03	0.00	-472.90	9.58	472.90	270.00	334.3
KOP 2 3985.	68		80.68	273.23	3746.31	-2486.69	1.67	-531.75		531.76	270.18	377.18
	20		81.87	2/8.89	3/55.42	-24//.58	1.92	20.092-	9.54	540.10	11.012	423.20
	71		84.26	290.21	3769.91	-2463.09	37.79	-705.66	5	CT.640	273.07	525.6
	72	4,260.00	85.46	295.87	3775.29	-2457.71	61.15	-760.58	9	763.03	274.60	581.0
	73		86.65	301.53	3779.43	-2453.57	89.86	-813.01	9.62	817.96	276.31	638.4
	74		87.84	307.20	3782.31	-2450.69	123.65	-862.42	6	871.24	278.16	697.2
C 014 001	27		89.04	312.86	3/83.94	-7449.06	XL /YL	16/ XU6-		114110	1XII 1X/	755 4
1 / LAND	4/		89 49	315.00	3784 71	-7448.79	903 79	-951 49	n er	C0.226	282.09	816.9

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315.00 31	3803.94 3804.47 3805.01 3805.54 3806.68 3806.61 3807.68 3807.14 3807.14 3807.14 3807.28 3809.21 3809.28 3810.35 3810.35 3811.95 3812.48	-2428.53 -2427.99 -2427.46 -2426.92 -2426.92 -2426.39 -2425.86 -2425.86 -2425.82 -2424.79 -2424.79 -2424.72 -2424.72 -2423.19 -2423.19 -2422.16 -2422.15 -2422.15 -2422.15 -2422.15	1773.51 1815.93 1888.35 1900.78 1943.20 1943.20 1945.63 20208.05 20208.05 20208.05 20270.48 2112.90 2155.33 2197.75 2197.75 2197.75 22197.75 22197.75 2235.03 2235.03		2293.93 22436.35 22478.78 22521.20 22563.63 22563.63 22563.63 22563.63 22563.63 22563.63 22563.63 22690.90 22563.63 22690.90 22690.90 22775.75 22818.18 22860.60 22860.60 22903.03 22903.03 22903.03 20 3030.330 3030.30 30 3030.30 30 3037.757		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
315.00 31	3803.94 3805.01 3805.01 3806.08 3806.61 3807.68 3807.68 3807.68 3807.68 3807.68 3807.68 3807.88 3809.28 3809.28 3809.28 3809.28 3809.28 3809.28	-24285-53 -24277-59 -24277-69 -2426-59 -2426-59 -2425-86 -2425-86 -2425-86 -2425-86 -2425-72 -2424,79 -2423,72 -2423,72 -2423,72 -2423,72 -2423,72 -2423,72 -2423,72 -2422,65 -2422,65 -2422,75 -2425,75 -245,75 -245,75 -245,75 -245,75 -245,75 -245,75 -245,75 -245,75	1773.51 1815.93 1815.93 188.35 1900.78 1943.20 1945.63 2028.05 2070.48 2112.90 2112.90 2117.53 2197.75 2197.75 2232.60 2327.45		2293.93 2436.35 2478.78 2521.20 2521.20 2563.63 2563.63 2566.05 2666.05 2668.48 2690.90 22648.48 22648.48 22648.48 22648.48 22648.4526 22648.45 22648.45 26648.4526		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
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315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00	3803.94 3804.47 3805.01 3805.01 3805.54 3806.61 3806.61 3807.14 3807.68 3808.21	-2428.53 -2427.99 -2427.46 -2426.92 -2426.39 -2425.86 -2425.86 -2425.32 -2424.79	1773.51 1815.93 1858.35 1900.78 1943.20 1943.20 1985.63 2028.05 2070.48		-2393.93 -2436.35 -2478.78 -2478.78 -2521.20 -2563.63 -2606.05 -2648.48 -2609.90 -2648.48 -2690.90 -2773.33 -2775.75 -22818.18		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00	3803.94 3804.47 3805.01 3805.54 3805.54 3806.61 3807.14 3807.68	-2428.53 -2427.99 -2427.46 -2426.92 -2426.39 -2425.86 -2425.32	1773.51 1815.93 1858.35 1900.78 1943.20 1985.63 2028.05		-2393.93 -2436.35 -2478.78 -2478.78 -2563.63 -2563.63 -2563.63 -2666.05 -2648.48 -2660.90 -2690.90 -2773.33 -2775.75		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
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315.00 315.00 315.00 315.00 315.00 315.00 315.00 315.00	3803.94 3804.47 3805.01	-2428.53 -2427.99	1773.51 1815.93		-2393.93 -2436.35 -2478.78 -2521.20 -2563.63		0.00 0.00 0.00 0.00
315.00 315.00 315.00 315.00 315.00 315.00 315.00	3803.94 3804.47	-2428.53	1773.51		2393.93 2436.35 2478.78 2521.20		0.00 0.00 0.00
315.00 315.00 315.00 315.00 315.00 315.00	3803.94				2393.93 2436.35 2478.78		0.00
315.00 315.00 315.00 315.00 315.00	0000-14	-2429.06	1731.08		2393.93		0.00
315.00 315.00 315.00	3803 41	-2429.59	1688.66	-2	393.93		0.00
315.00 315.00	3802.87	-2430.13	1646.23	-73	U		0.00
315.00	102 CU85	-2431.20	1603 81	-23	51 50		0.00
100 210	3801.27	-2431.73	1518.96	-22	66.65		0.00
315.00	3800.74	-2432.26	1476.53	-22	24.23		0 00
315.00	3800.20	-2432.80	1434.11	-218	1.80		0.00
315.00	3799.67	-2433.33	1391.68	-213	39.38		0.00
315.00	3799.13	-2433.87	1349.26	-209	96.96		0.00
315.00	3798.60	-2434.40	1306.83	-20	54.53		0.00
315.00	3798.06	-2434.94	1264.41	-20	12.11		0.00
315.00	3797.53	-2435.47	1221.98	-10	69.68		0.00
215 00	2707.40	-2436.00	1170 56	-10	177 76		0.00
315.00	3795.93	-2437.07	1094.71	. L	842.41		0.00
315.00	3795.39	-2437.61	1052.28	-1	799.98		0.00
315.00	3794.86	-2438.14	1009.86	-17	57.56		0.00
315.00	3794.33	-2438.67	967.44	-17	15.13		0.00
315.00	3793.79	-2439.21	925.01	-	672.71		0.00
315.00	3793.26	-2439.74	882.59		1630.28		0.00
315.00	3792.72	-2440.28	840.16		1587.86		0.00
315.00	3792.19	-2440.81	797.74		1545.43		0.00
315.00	3791.66	-2441.34	755.31		-1503.01		0.00
315.00	3791.12	-2441.88	712.89		1460.58		0.00
315.00	3790.59	-2442.41	670.46		1418 16		0.00
315.00	3700.05	-2443.48	T0.525	4	333.31		0.00
315.00	3700 57	2444.UI	543.19	77-	90.89		0.00
315.00	3788.45	-2444.55	500.76	-12	48.46		0.00
315.00	3787.92	-2445.08	458.34	-120	6.04		0.00
315.00	3787.38	-2445.62	415.91	-11	63.61		0.00
315.00	3786.85	-2446.15	373.49	-112	21.19		0.00
315.00	3786.32	-2446.68	331.06	-107	8.76		0.00
315.00	3785.78	2447.22	88.64	-103	6.34	0.00	0.00
ິ ພຸມ ພູພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ ພ	315.00 315.00 315.00 315.00	TVD (ff) 3785.78 3785.88 3785.78 3785.78 3785.38 3787.38 3787.38 3788.45 3789.52 3789.52 3791.66 3792.19 3791.66 3792.19 3792.26 3792.3791.42 3793.79 3794.86 3795.39 3795.39 3794.86 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.39 3795.93 3795.93 3795.93 3795.93 3795.93 3795.93 3797.00 3798.66	TVD (ft) TVDSS (ft) 3785.78 -2447.82 3785.88 -2446.15 3786.85 -2445.62 3787.92 -2445.62 3787.92 -2445.62 3787.92 -2445.62 3787.92 -2445.62 3788.99 -2444.91 3790.95 -2442.94 3791.12 -2441.88 3792.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3793.79 -2440.81 3795.70 -2439.74 3795.39 -2437.61 3795.46 -2437.61 3795.93 -2437.61 3795.46 -2435.60 3797.53 -2435.40 3797.53 -2435.40 3798.60 -2434.40 3799.60 -2433.87	TVD (Å) TVDS (Å) V/-S (Å) 3785.78 -2447.22 328.6 3785.78 -2445.62 331.0 3786.82 -2445.62 312.0 3786.82 -2445.62 415.93 3787.92 -2445.02 458.3 3787.92 -2445.02 458.3 3787.92 -2444.01 543.12 3788.45 -2442.95 500.7 3788.52 -2443.01 543.12 3789.52 -2443.24 58.6 3791.66 -2441.34 755.3 3792.72 -2440.28 82.5 3792.72 -2440.28 82.5 3792.72 -2439.74 82.5 3792.72 -2439.74 82.5 3792.72 -2439.74 82.5 3792.72 -2439.74 82.5 3792.73 -2439.71 1002.28 3795.30 -2437.61 1052.28 3795.48 -2435.47 1137.13 3795.53 -2435.47 1137.13	TVD (ft) TVDSS (ft) $V-SS$ (ft) $V-SS$ (ft) $E/-W$ (ft) 3785.37 -2447.22 288.64 -1036.34 3786.82 -2445.62 331.06 -1078.76 3786.82 -2445.62 331.06 -1036.34 3787.92 -2445.02 331.06 -1036.34 3787.92 -2445.02 331.06 -1026.34 3787.92 -2445.02 415.91 -1163.61 3787.92 -2444.01 543.19 -1290.89 3789.52 -2442.41 545.31 -1290.89 3790.51 -2441.24 575.31 -1375.73 3791.56 -2441.34 795.31 -1503.01 3792.72 -2440.28 840.16 -1487.86 3793.79 -2439.74 -1545.43 3794.43 3794.43 -2435.01 1052.28 -1757.56 3795.39 -2437.71 -1842.41 1799.98 3795.46 -2435.01 1157.13 -1842.41 3795.46 -2435.01 1157.15	$\begin{tabular}{ c c c c c } \hline \begin{tabular}{ c c c c c } \hline \hline \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	





WELL NAME: Coal Creek State 16-1

Casing Data - SURFACE - Evacuated / Max SICP (Collapse/Burst), 100k Overpull (Tension)

Casing	WT	Connection	Grade	Burst Rating	Collapse Rating	MinYield Rating
13 3/8	54.5	STC	J-55	2,730	1,130	514,000

ole Data							Completion Info		Design Info)	
TD	TD Next Hole Section	Mud Weight	Max Pore Pressure Next Hole Section	Shoe Pore	Pressure	Gas Gradient	Frac Pressure	Frac Fluid WT	Collapse SF	Burst SF	Tensio SF
200	2,900	9.0	8.3	8.	3	0.2	N/A	N/A	1.125	1.1	1.2
ollapse @ shoe wit	h das gradien	t	126	psi							
ollapse SF			8.95	• /////							
urst during kick at	next hole sect	tion TD	672	psi	(Evac hole with ga	as gradient)				
urst SF			4.06	OK							
leight of string in fl	uid		9,402	lbs							
verpull			100,000	lbs							
otal Weight on slip	S		109,402	lbs							
ension SF			4.70	OK							

Casing	WT	Connection	Grade	Burst Rating	Collapse Rating	MinYield Rating
9 5/8	36.0	STC	J-55	3,520	2,020	394,000

Hole Data							Completion Info		Design Info)	
				Max Pore							
	TD Next Hole			Pressure Next			Frac	Frac Fluid	Collapse	Burst	Tension
TD	Section	Mud	Weight	Hole Section	Shoe Pore Pressure	Gas Gradient	Pressure	WT	SF	SF	SF
2900	5,100	1	0.0	8.3	8.0	0.2	N/A	N/A	1.125	1.1	1.2

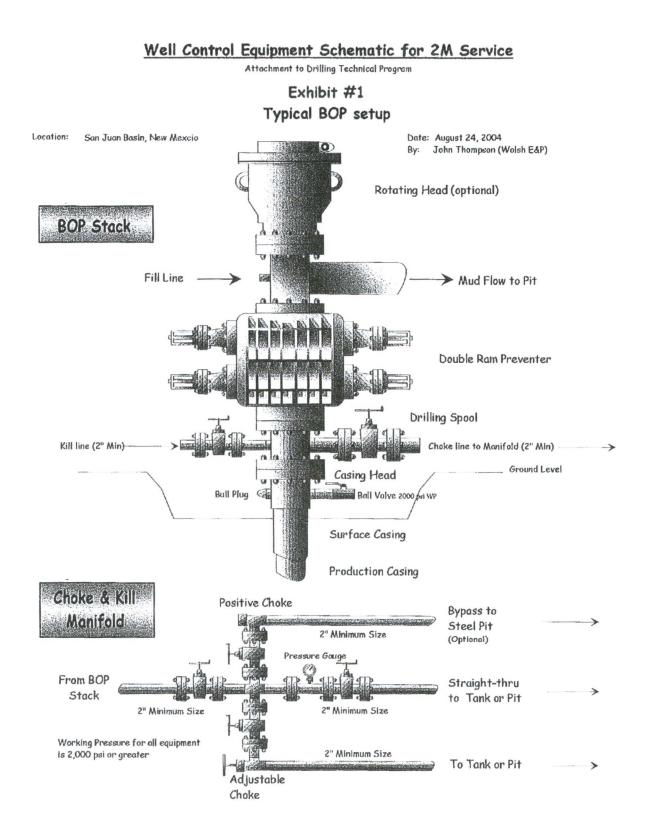
1,786 psi 1.13	ОК	
1,181 psi 2.98	ОК	(Evac hole with gas gradient)
88,461 lbs 100,000 lbs		
188,461 lbs	OK	
	1.13 1,181 psi 2.98 88,461 lbs 100,000 lbs	1.13 OK 1,181 psi 2.98 OK 88,461 lbs 100,000 lbs 188,461 lbs

Casing Data - PRODUCTION - Evacuated / Max SICP (Collapse), Max Frac Press. (Burst), 100k Overpull (Tension)

Casing	WT	Connection	Grade	Burst Rating	Collapse Rating	MinYield Rating
5 1/2	20.0	LTC & BTC	P-110	12,640	7,460	548,000

Hole Data						Completion Info		Design Info	D	
TD - TVD	TVD Next Ho Section	le Mud Weight	Max Pore Pressure Next Hole Section	Shoe Pore Pressure	Gas Gradient	Frac Pressure	Frac Fluid WT	Collapse SF	Burst SF	Tension SF
9518	9,518	10.4	8.3	8.0	0.2	10,000	8.4	1.125	1.1	1.2
Collapse @ shoe Collapse SF	with gas gradie	ent	5,863 1.27							
Burst at shoe dur Burst SF	ing frac		9,703 1.30		(Assumes 9# grad	lient on backside)				
Burst during kick Burst SF	at next hole se	ction TD	2,204 5.73	 COV 10 	(Evac hole with ga	as gradient)				
Weight of string i Overpull Total Weight on s Tension SF			160,135 100,000 260,135 2.11	lbs						

DATE: 9/5/2018 LOCATION: COAL CREEK 16 1H JUNIPER RESOURCES EXPLORATION CO. LLC RIG: TBD COUNTY: SAN JUAN COUNTY GLE: 6219 WELL: COAL CREEK 16 1H WELL SUMMARY **RKBE:** 6233 **OPEN HOLE** DEPTH CASING / CEMENTING MWD / LWD HOLE SIZE MUD SPECS **DEVIATION INFO.** FORMATION WELLBORE SCHEMATIC LOGGING TVD MD SPECS Vertical 0' None Kirtland Shale 0' Fresh Wtr. Survey every None 13 3/8", 54.5 ppf, J55, ST&C 8.4 - 9 ppg < 1 deg 100' Cement to Surface 200' 17 1/2" 13 3/8" Casing 200' Fruitland 225' 225' **Pictured** Cliffs 397' 397' 9 5/8", 36 ppf, J55, ST&C No OH Logs Cement w/ 1048 sx VARICEM (or similar) Vertical Cement to Surface < 1 deg None Lewis Shale 530' 530' Survey every 120' WBM Cliffhouse 8.4 - 9.5 ppg 1,070' 1,070' Mud Logger on at 1,625' 1,649' Menefee 1,649' Point Lookout 2,742' 2,742' Mancos 2,895' 2,895' 9-5/8" Casing 2,900' 2,900' 12-1/4" KOP 3,160' 3,160' KO Plug f/ 2,900' to OH Log Suite: 3,472' 3,900' Build / Turn Mancos Silt 3,472' Triple Combo 8 - 10 deg/100' w/ Spectral GR DLS 8-3/4" MWD/LWD **Dipole Sonic** GR, Inc. Azi. NMR Mancos 2A 3,722' 3,722' Dielectric FMI Survey every 30' in curve 200' Cement into 9 5/8" Csg 60' in lateral El Vado 3,768' TD = 9,406' MD 4.966' Drilled Lateral Hz Target 3,830' 9,406' 5 1/2", 20 ppf, P110, LTC/BTC WBM Gallup 3,892' 3,892' Long Sting 9 - 10 ppg Juana Lopez 4,309' 4,309' Cement w/ 1658 sx - 1 stage Dakota 4,742' 4,742' Planned Cmt top - 2700' MD 5,087' 5,087' 8-3/4" Pilot Hole TD



Michelle Lujan Grisham Governor •

Sarah Cottrell Propst Cabinet Secretary

Todd E. Leahy, JD, PhD Deputy Secretary **Gabriel Wade**, Acting Director Oil Conservation Division



New Mexico Oil Conservation Division conditions of approval C-101 Application for Permit to Drill

Operator Signature Date: <u>2/18</u>2019 Well information; Operator <u>Janiper</u>, Well Name and Number <u>Coal Creek State 16</u>#/H

API# <u>30.045.35910</u>, Section <u>16</u>, Township <u>230</u>/S, Range <u>11</u> E/

Conditions of Approval: (See the below checked and handwritten conditions)

- ★ Notify Aztec OCD 24hrs prior to casing & cement.
- ★ Hold C-104 for directional survey & "As Drilled" Plat
- Hold C-104 for NSL, NSP, DHC
- Spacing rule violation. Operator must follow up with change of status notification on other well to be shut in or abandoned
- Regarding the use of a pit, closed loop system or below grade tank, the operator must comply with the following as applicable:
 - A pit requires a complete C-144 be submitted and approved prior to the construction or use of the pit, pursuant to 19.15.17.8.A
 - A closed loop system requires notification prior to use, pursuant to 19.15.17.9.A
 - A below grade tank requires a registration be filed prior to the construction or use of the below grade tank, pursuant to 19.15.17.8.C
- Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string

• Submit Gas Capture Plan form prior to spudding or initiating recompletion operations

Regarding Hydraulic Fracturing, review EPA Underground Injection Control Guidance 84

✓ Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system.

✓ Well-bore communication is regulated under 19.15.29 NMAC. This requires well-bore Communication to be reported in accordance with 19.15.29.8.