UNITED STATES DEPARTMENT OF THE INTERIOR **BUREAU OF LAND MANAGEMENT**

FORM APPROVED OMB No. 1004-0136 Expires November 30, 2000

7.5	٥.	Lease Tali No.	
1	j	NMSF-078146	Α

APPLICATION FOR PE	EDMIT TO DI		ENTED		6. If Indian, Allottee or To	ribe Name	
APPLICATION FOR PE		NILL ON NI	2003 F	<u> </u>	N/A		
1a. Type of Work: ORILL					7. If Unit or CA Agreemen	271/	
,,	_		070 F	arminothe	N/A 8. Dease Name and Well N	<u> 5016</u>	
1b. Type of Well: Oil Well Gas Well	Other	🗹 Si	ngle Zone 🔲 Mult	iple Zone	HORTON 4 B		
2. Name of Operator		202107		\DZ	9. API Well No.	117	
QUESTAR EXPLORA					30-045-	11/	
7a. Address 1331 17th ST., SUITE DENVER, CO 80202	∃ 800		572-6916	er i de tradicione en medicionalità de l'approprie	10. Field and Pool, or Exploratory BLANCO MESA VERDE		
4. Location of Well (Report location clearly and i	n accordance with	h any State requi	irements.*)		11. Sec., T., R., M., or Blk.	and Survey or Area	
At surface 1872' FSL &	1906' FWL				∠ 27-32n-12w ∣	NMPM	
At proposed prod. zone SAME				/	<		
14. Distance in miles and direction from nearest tow 6 AIR MILES		_aPLATA			12. County or Parish SAN JUAN	13. State	
15. Distance from proposed*			Acres in lease	17. Spacing	Unit dedicated to this well		
location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any)	734'	320		320 A	CRES (W2)		
18. Distance from proposed location*		19. Propose	ed Depth	20. BLM/BI	A Bond No. on file		
to nearest well, drilling, completed, applied for, on this lease, ft.	128'	5,400			6308873, BLM ES0019		
21. Elevations (Show whether DF, KDB, RT, GL, 6,138' GL	etc.)		imate date work will s	tart*	23. Estimated duration 30 DAYS		
0,130 GL			chments]	JUDATO		
					1		
The following, completed in accordance with the requ	uirements of Onsr	nore Oil and Gas	Orger No.1, snan be	attached to this	orm:		
1. Well plat certified by a registered surveyor.			4. Bond to cover Item 20 above		unless covered by an exist	ing bond on file (see	
 A Drilling Plan. A Surface Use Plan (if the location is on National 	Forest System 1	ands the	5. Operator certif	fication.			
SUPO shall be filed with the appropriate Forest S		ands, the	6. Such other site authorized offi	•	ation and/or plans as may b	be required by the	
Comments			<u> </u>		4104174		
Archaeology report LAC 2000	-51 filed 7.	-24-01		19/1	3 10 11 18 7930		
Alchaeology report EAO 2000	-or mear	-2-4-01		12.	1. 4		
				15 1	MARON		
This action is subject to technical and	DRILLING OPERA	ATIONS AUTHOR	RIZED ARE				
procedural review pursuant to 43 CFR 3165.8 and appeal pursuant to 43 CFR 3165.4	SUBJECT TO CO. *GENERAL REQL	MPLI ANCE WITH HIRF MENTS".	H ÀI IAONED	(a)			
	GENERAL HEAV			1			
				60.			
a 1				~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	12 Caller		
_ () /		cc: l	BLM, Lovsetl	h, Nelsen	, NMOCD (via B	LM), Ohlma	
25. Signature		Name	e (Printed/Typed)		Da	te	
(Show		1		BRIAN	1 MOOD	2-15-0	
Title	PHONE:	505 466-8	120	FAX: 50	5 466-9682		

Date MAR Name (Printed/Typed) Office Title

Application approval does not warrant or certify the the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct

Conditions of approval, if any, are attached.

CONSULTANT

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

State of New Mexico Energy. Minerals & Mining Resources Department OIL CONSERVĂTION DIVISION 2040 South Pacheco Santa Fe. NM 87505

MENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

APA Number	Pool Code	Pool Nome		
30-045-314	7 72319	BLANCO MESA VERDE		
Property Code	Prope	rty Name	Well Number	
132167	· HOR	TON	·4 B	
OGRID No.	Opera	tor Name	Devation	
23846	QUESTAR EXPLORA	TION & PRODUCTION	6138	

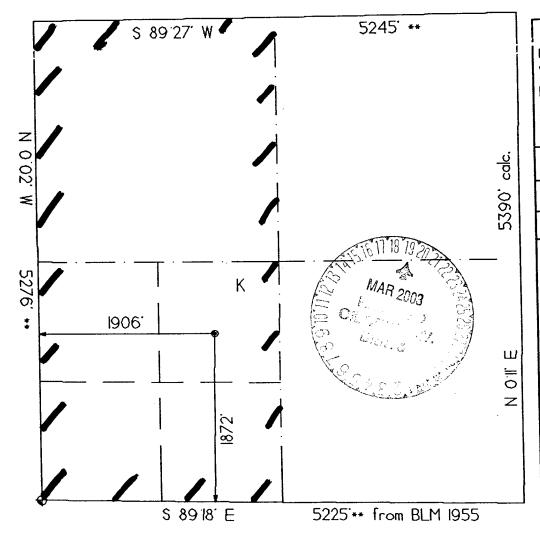
Surface Location

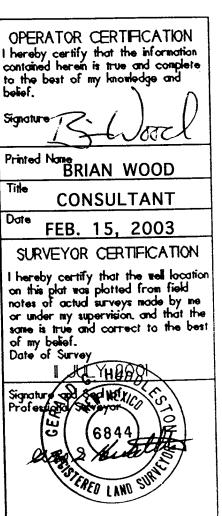
I	UL or Lot	Sec.	Tup.	Rge.	Lot lan.	Feet from>	North/South	Feet from>	East/West	County
	K	27	32 N.	12 W.		1872	SOUTH	1906	WEST	SAN JUAN

Bottom Hole Location if Different From Surface

UL or Lot	Sec	Тир	Rge.	Lot kh.	Feet from>	North/South	heer from>	Fost/ Hest	County
Dedication 320	Joi	nt?	Consolida	tion			Orde	r No.	

NO ALLOWABLE WILL ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DMISION





Oil and gas shows will be tested and evaluated for commercial potential as determined by the company geologist. Goal is the Mesa Verde.

3. PRESSURE CONTROL (Also see PAGES 3 - 5)

The drilling contract has not yet been awarded, thus the exact type of BOP to be used is not now known. Diagrams of a typical 2,000 psi BOP stack and manifold are on PAGES 3 and 4.

Call BLM at (505) 599-8900 >24 hours before testing. BOP system will be installed and pressure tested before drilling the surface casing shoe. It will be retested if a pressure seal is broken or is 30 days have elapsed since the last successful test of the equipment. Test pressures are ...

Pipe rams	2,000 psi (high)	250 psi (low)
Choke manifold & lines	2,000 psi (high)	250 psi (low)

Will initially pressure test BOP and ancillary equipment to 250 psi for 5 minutes, followed by by a test to 2,000 psi for 10 minutes. Casing will be tested for 30 minutes. BOP equipment will remain in use until the well is completed or abandoned. Safety valve and sub with a full opening valve to fit the drill pipe and collars will be available on the rig floor in the open position at all time for use when the kelly is not in use.

All BOP mechanical and pressure tests will be recorded on the driller's log. BOPs will be inspected and opened and closed at least daily to assure good mechanical working order. These inspections will also be recorded on the daily drilling report.



4. CASING & CEMENTING

Design factors are:

Collapse = 1.125

Burst = 1.00

Tension = 1.80

Area Fracture Gradient = 0.83 psi/foot

Casing Integrity Tests: test to 0.22 psi/foot or 1,500 psi whichever is more (not to exceed 70% of the rated burst pressure of the casing)

Surface Casing: Test to 1,500 psi

(drill out surface casing \leq 10' & test shoe to 12 ppg [estimate 75 psi with fresh H₂0 in hole])

Intermediate Casing: Test to 1,500 psi (with 8.5 pounds per gallon fluid in hole)
Production Casing: Test to 1,200 psi (with 8.5 pounds per gallon fluid in hole)

Hole Size	O. D.	#/ft Grade Thread Age	Collapse Burs	<u>t Tensile</u>	<u>Depth</u>
20"	14"-16"	Corrugated Conductor Used			0' - 40'
12-1/4"	9-5/8"	32 H-40 ST & C New	1,370 2,27	0 254,000	0' - 200'
8-3/4"	7"	23 J-55 ST & C New	3,270 4,36	0 284,000	0' 2,920 ' 100 m
6-1/4"	4-1/2"	9.5 J-55 ST&C New	3,310 4,38	0 101,000	0' - 200' 0' 2,920 ' 100' MIN 2,620' - TD Overlap

Conductor pipe will be cemented to the surface with ≈45 cubic feet of construction cement.

Surface casing (0' - 200') will be run as follows:

- a) Guide shoe
- b) One joint
- c) Insert float
- d) Remainder of casing
- e) Three bow spring centralizers (10' above shoe joint, middle of the second joint, and one on the second to last joint)
- f) Thread lock bottom joint of casing and float equipment. Reciprocate casing 20' while cementing. Land casing so casing head flange will be at ground level and the shoe joint is as near bottom as possible.



Surface casing will be cemented to the surface as follows:

- a) Circulate and condition the hole until the returns are clean ($\geq 1-1/2$ times bottoms up or one internal casing volume, whichever is greater)
- b) Pump ≈10 barrels fresh water
- c) Slurry = 125 sacks Class G + 2% CaCl₂ + 1/4 lb/sk Cello Flake. Weight = 15.8 pounds per gallon. Yield = 1.16 cubic feet per sack. Mix water = 4.95 gallons per sack. Volume = 144 cubic feet based on 18 cubic feet for 40' of shoe joint + 63 cubic feet for annulus + 100 cubic feet excess (100%).
- d) Use top wiper plug. Displace with water. Casing capacity = 12.6 barrels to the float collar.
- e) Have ≈100 sacks Class G cement, 5 joints 1" line pipe, and enough CaCl₂ to mix 2% by volume with the top off cement to circulate top 100' of casing annulus if cement drops from surface. W. O. C. = 6 hours before cutting off and nipple up. Casing head flange= 9-5/8" x 11" 2,000 psi.

Intermediate casing (0' - 2,920') will be run as follows:

- a) Float shoe
- b) One joint
- c) Float collar
- d) Ten centralizers (two centralizers placed on joints 1, 6, 7, and 8 in the hole (10' from each end) and the third to the last joint run in the hole)
- e) Lock shoe joint and float equipment with thread lock compound

Intermediate casing will be cemented to surface as follows:

- a) Reciprocate casing ≈20' during cementing
- b) Circulate and condition the hole until the returns are clean ($\geq 1-1/2$ times bottoms up or one internal casing volume, whichever is greater)
- c) Pump ≈20 barrels fresh water
- d) Lead slurry = 235 sacks 35/65 Poz-G + retarder for 2-1/2 hours pumpability at 95° F + friction reducer for turbulent flow at 5 barrels per minute + fluid loss additive. Weight =11.4 pounds per gallon. Yield = 2.90 cubic feet per sack. Mix water = 17.78 gallons per sack. Volume = 681.5 cubic feet.



- e) Tail slurry = 165 sacks Class G + friction reducer + fluid loss additive. Weight = 13.5 pounds per gallon. Yield = 1.30 cubic feet per sack. Mix water = 5.48 gallons per sack. Volume = 214.5 cubic feet
- f) Total intermediate casing cement volume = 893 cubic feet (9 cubic feet for shoe joint + 409 cubic feet open hole annulus + 33 cubic feet cased hole annulus + 442 cubic feet for 60% excess). Final volume calculations will be calculated from caliper log results.
- g) Displacement volume to float collar = 113.5 barrels (displace with 10 barrels fresh water followed by mud)
- h) After displacement, check to insure floats are holding. If they hold, then release pressure and start to nipple down. If not, hold 200 psi over plug, bumping pressure until floats hold, then start to nipple down.

Production liner (5,400' to 2,620') will be run as follows:

- a) Float shoe
- b) One joint
- c) Float collar
- d) Ten centralizers (two centralizers placed on joint 1 (10' from each end) and one on the third to the last joint in the hole placement of the remaining centralizers will be determined from log analysis)
- e) Lock shoe joint and float equipment with thread lock compound
- f) Remainder of line (enough liner to overlap intermediate casing by 300')
- f) Liner hanger and setting tool
- g) drill pipe to TD

Production liner will be cemented by ...

- a) Blow hole clean
- b) Pump ≈20 barrels fresh water
- c) Slurry = 393 sacks 50/50 Poz-G + retarder for 2-1/2 hours pumpability at 110° F + friction reducer for turbulent flow at 5 barrels per minute + fluid loss additive. Weight = 13.5 pounds per gallon. Yield = 1.30 cubic feet per sack. Mix water = 5.48 gallons per sack. Volume = 511 cubic feet (4 cubic feet for shoe joint + 254 cubic feet for open hole annulus + 33 cubic feet overlap annulus + 44 cubic feet for 200' on top of liner + 102 cubic



feet for 40% excess open hole annulus)

- d) Final cement volume calculations will be based on caliper log results. Estimated top of cement will be 200' above the top of the liner (i. e., $\approx 2,420$ ' since top of line will be $\approx 2,620$ ')
- e) Displace with 10 barrels of fresh water followed by 2% KCl water

5. MUD PROGRAM

Will circulate water through reserve pit, flocculate with lime, and run gel and/or polymer sweeps as needed to clean hole from surface to 200'. Will continue to circulate water through the reserve pit and running gel and polymer sweeps as necessary from the base of the surface casing to 100' above the Fruitland. Before entering the Fruitland coal, will lightly mud up with adequate viscosity and density to maintain a stable well bore. Estimated mud density = 9.0 - 9.5 pounds per gallon. Mud additives on location will include: barite (bulk and sack), gel, polymer, caustic soda, and lost circulation material.

Will air drill bottom 2,300'. Dust as long as possible before misting. If hole becomes too wet, may mud up.

Based on adjacent wells, all formations are expected to be sub-normally pressured. If virgin pressures are encountered, the maximum bottom hole pressure would be 2,338 psi (5,400' x 0.433 psi per foot).

6. CORES, TESTS, & LOGS

No cores, drill stem tests, or mud logs are planned. First logging run from intermediate casing TD to surface casing will be DIL/GR/SP/Neut./Den. Second logging run from final TD to intermediate casing will be DIL/GR/Neut/Den/Temp. CAL/TEN curves on all logs.

