

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 6-2-84	
Company Robert L. Bayless		Connection	
Pool Ballard Pictured Cliffs		Formation Pictured Cliffs <i>E_{xt}</i>	
Completion Date 5-22-84		Total Depth 2660'	
Plug Back TD 2573'		Elevation 7038'	
Fam or Lease Name Jicarilla 393		Well No. B #3	
Csg. Size 2-7/8"		Wt. 7.9#	
Set At 2653'		Perforations: From 2492' To 2549'	
Trg. Size None		Wt. --	
Set At --		Perforations: From -- To --	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At None	
Producing Thru Casing		Reservoir Temp. °F #	
Mean Annual Temp. °F		Baro. Press. - P _a 12 psia (est)	
State New Mexico		County Sandoval	
L		H	
G _g .65		% CO ₂	
% N ₂		% H ₂ S	
Prover		Meter Run	
Taps			

FLOW DATA

TUBING DATA

CASING DATA

Duration

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	8 days								480		
1.	2" X 1/2"			31					31	60°	3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	5.4315		43	1.000	.9608	1.009	226
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P_c 492		P_c^2 242,064			(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.0086}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.0073}$
NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$		
1		46	2075	239,989	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{228}$	
2						
3						
4						
5						

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 228$$

Absolute Open Flow 228 Mcfd @ 15.025 Angle of Slope θ Slope, n .85

Remarks:

Approved By Division Conducted By: Walsh Engineering Calculated By: Kevin H. McCord Checked By: Robert L. Bayless