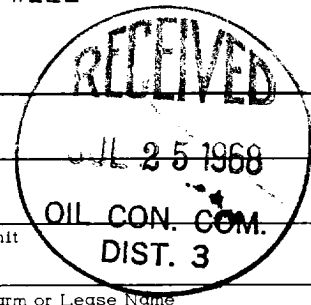


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65



Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 7-20-68						
Company Morrison & Bayless			Connection El Paso								
Pool Ballard			Formation Pictured Cliffs								
Completion Date 7-11-68		Total Depth 2271		Plug Back TD 2228							
Csg. Size 4 1/2		Set At 4.090		Elevation 6706 KB							
Farm or Lease Name Backhouse Canyon			Well No.								
Tbg. Size None		Set At 2259		Performations: From 2275 To 2200							
Unit 1 Sec.			Twp. 11								
Range 24			County 7								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At						
Producing Thru Csg.		Reservoir Temp. °F 90° @ 2200		Mean Annual Temp. °F 12							
Baro. Press. - P _a 12		State New Mexico		City Rio Arriba							
L 2187	H 0.7	G _g 0.7	% CO ₂	% N ₂	% H ₂ S						
Prover		Meter Run		Taps							
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	2"	X	3/4	278			451	278	50	3 hrs.	
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1.	12.2		290	1.0098	0.9258	1.039	3,436				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
$P_c = 463$ $P_c^2 = 214,369$					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.683$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5566$						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5,348$						
1.	84,100	295	87,025	127,344							
2.											
3.											
4.											
5.											
Absolute Open Flow 5,348 Mcfd @ 15.025					Angle of Slope θ _____			Slope, n 0.85			
Remarks: P_a = 1.45 (1-e⁻⁵) = 0.106											
Approved By Commission:			Conducted By:			Calculated By:			Checked By:		
Marie Klussner			J. C. Morrison			X					