

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 8-18-75	
Company Skelly Oil Company				Connection Not connected		
Pool Basin				Formation Dakota		Unit
Completion Date 8-1-75		Total Depth 6894 K.B.		Plug Back TD 6862 K.B.		Elevation 6561 G.L.
Farm or Lease Name Jicarilla "B"						
Csq. Size 4.500	Wt. 11.6	d 3.875	Set At 6893 K.B.	Perforations: From 6753 G.L. To 6803 G.L.		Well No. 24
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 6758 G.L.	Perforations: From Open To Ended		Unit Sec. Twp. Rge. P 6 24N 5W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas				Packer Set At 6721 G.L.		County Rio Arriba
Producing Thru Tubing		Reservoir Temp. °F 165 °		Mean Annual Temp. °F 12.2		State New Mexico
L 6758	H 6758	Gg .720	% CO ₂	% N ₂	% H ₂ S	Prover 2.000
Meter Run		Taps				

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1961		PKR.		168 HR.
1.	2.000	X	.750			40	260				1
2.	2.000	X	.750			45	204				1
3.	2.000	X	.750			50	152				1
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		272.2	1.0198	.9129	1.039	2896
2.	11.00		216.2	1.0147	.9129	1.029	2267
3.	11.00		164.2	1.0098	.9129	1.021	1700
4.							
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

$P_c = 1972.2$ $P_c^2 = 3889573$				
NO	P_f^2	P_w	P_w^2	$P_c^2 - P_w^2$
1				
2				
3	26961	321	103091	3786482
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0272$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.021$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1736$$

Absolute Open Flow _____ 1736 _____ Mcfd @ 15.025	Angle of Slope @ _____
Remarks: _____	

Approved By Commission:	Conducted By: Paul D. Berhost	Calculated By: Paul D. Berhost	Checked By:
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