

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date <u>12/1/77</u>	
Company <u>Continental Oil Company</u>			Connection <u>None</u>		
Pool <u>Ballard</u>			Formation <u>Pictured Cliff</u>		Unit
Completion Date <u>11/19/77</u>		Total Depth <u>2790'</u>	Plug Back TD <u>2751'</u>	Elevation <u>6685'</u>	Farm or Lease Name <u>AXI APACHE "D"</u>
Csg. Size <u>4.5</u>	Wt. <u>10.5</u>	d <u>2790'</u>	Set At <u>2790'</u>	Perforations: <u>From 2460' To 2517'</u>	Well No. <u>5</u>
Tbg. Size <u>1 1/4</u>	Wt. <u>2.40</u>	d <u>2445</u>	Set At <u>2445</u>	Perforations: <u>From OK To</u>	Unit Sec. Twp. Rge. <u>E 19 24N 4W</u>
Type Well - Single - Brdenhead - G.G. or G.D. Multiple <u>Single B</u>				Packer Set At <u>None</u>	County <u>Rio Arriba</u>
Producing Thru <u>Thru</u>		Reservoir Temp. °F <u>109° @ 2751</u>	Mean Annual Temp. °F <u>50°</u>	Baro. Press. - P _a <u>12.2</u>	State <u>N. Mex.</u>
V <u>2460</u>	H <u>2460</u>	G _g <u>.69</u>	% CO ₂	% N ₂	% H ₂ S Prover Meter Run Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	<u>3/4" choke nipple</u>			<u>38</u>		<u>46°</u>	<u>650</u>	<u>32°</u>	<u>650</u>	<u>32°</u>	<u>3 hr.</u>
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	<u>11.00</u>		<u>50</u>	<u>1.014</u>	<u>1.204</u>	<u>1.00</u>	<u>6.71</u>
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c <u>672</u>	P _c ² <u>451584</u>			
NO.	P _t	P _w	P _w ²	P _c ² - P _w ²
1.		<u>44</u>	<u>1916</u>	<u>440000</u>
2.				
3.				
4.				
5.				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{451584}{451584 - 1916} = 1.004$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.003$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6.73$

Absolute Open Flow <u>6.73 MCFO</u>	Mcf/d @ 15.025	Angle of Slope θ _____	Slope, α <u>.85</u>
Remarks: _____			

Approved By Commission: _____	Conducted By: <u>D.L. Moore</u>	Calculated By: <u>D.L. Moore</u>	Checked By: _____
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NMOCC, AZTEC (2), USGS, DURANGO (2), BEA, FILE