Initial Deliversbility

NEW MEXICO OIL CONSERVATION COMMISSION GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA EXCEPT BARKER DOME STORAGE AREA)

			Formation			y Rio Arrib a	
Purchasing P	ipeline El Pass	Lateral 6	ne Co	Date	Test Filed	1/14/	5-8
Operator S	he Chile Cill Cr		Lease	erilla Apache		ell No.	
		-		Pay Zone: From			
							2070.0
Casing: OD_				Tubing: OD			
				Gas Gravity: Meas			d
Oate of Flow	Test: From	T	o	_* Date S.I.P. Measure	ed 1/10/	<u> </u>	
Meter Run Siz	ze	0	rifice Size	Туре	Chart	Туре Т арѕ	<u> </u>
			OBSERV	ED DATA			
lowing casing	pressure (Dwt)			psig	+ 12 =	p	sia (
lowing tubing	pressure (Dwt)			psig +	- 12 =	р	sia (
lowing meter	pressure (Dwt)	· · · · · · · · · · · · · · · · · · ·		psig 4	12 =	р	sia (
-	pressure (meter read rt readina	_		n: psig +	- 12 =	n	sia (
Square root	chart reading () ² x sprin	g constant			p	•
leter error (c)	- (d) or (d) - (c)		±			-	si (
-	Flowing column to me						
	w through tubing: (a		-			p	si (
	age static meter pres rt average reading			psig +	- 12 =	a	sia (
	chart average readin				=		sia (
Corrected se	even day avge, meter	r press. (p _f) (g)	+ (e)		=	All alternation	sia (
t = (h) + (f)	_	•	25		=		sia (
Wellhead casing shut-in pressure (Dwt)						537	sia (
	-			psig f		847	•
ellhead tubing	g shut-in pressure (D	wt)	25	• •	12 =	137 p	sia (
Vellhead tubing C = (j) or (k) v	g shut-in pressure (D whichever well flowe	wt)	25	psig -	- 12 =	937 p	sia (
ellhead tubing c = (j) or (k) v lowing Temp.	g shut-in pressure (D whichever well flowe (Meter Run)	ed through	\$5 °F + 4€	psig f	- 12 =	967 p 937 p 938 p	sia (
Tellhead tubing $_{c}$ = (j) or (k) volume Temp. $_{d}$ = ½ $_{c}$ = ½	g shut-in pressure (D whichever well flowe (Meter Run) (1)	ed through	● F + 46 OW RATE CAL	psig f	- 12 =	187 p 187 p 180 p	sia (sia (Abs (
Vellhead tubing $P_C = (j)$ or (k) volume $P_C = (j)$ or (k) volume $P_C = \frac{1}{2}$ $P_C = \frac{1}{2}$	g shut-in pressure (D whichever well flowe (Meter Run) (1)	ed through FL V(d)	● F + 46 OW RATE CAL	psig f	- 12 =	187 p 187 p 180 p	sia (sia (Abs (sia (MCF/da
/ellhead tubing $P_c = (j)$ or (k) v $P_c = (j)$ or (k) v $P_c = \frac{1}{2}$ $P_c = \frac{1}{2}$ (integrated) $P_c = Q_c$ SUMMA	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d)	ed through FL V(d)	● F + 46 OW RATE CAL	psig +	- 12 =	226	sia (sia (Abs (sia (MCF/da
/ellhead tubing $P_C = (j)$ or (k) v $P_C = (j)$ or (k) v $P_C = (k)$ or (k) or (k) v $P_C = (k)$ or (k)	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d)	$\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{DE}}{\text{D}^2 - \text{P}^2 \text{d}} = \frac{2}{\text{D}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^$	OW RATE CAL	psig +	- 12 =	226	sia (sia (Abs (sia (MCF/da
/ellhead tubing $P_C = (j)$ or (k) v $P_C = (j)$ or (k) v $P_C = (k)$ or (k) or (k) v $P_C = (k)$ or (k)	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d)	$\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{DE}}{\text{Pc}^2 - \text{Pd}^2} = \frac{\text{DE}}{\text{Pc}^2 - \text{Pw}^2} = \frac{\text{DE}}{\text{Pc}^2 - \text{Pc}^2 - \text{Pw}^2} = \frac{\text{DE}}{\text{Pc}^2 - \text{Pw}^2} = \frac{\text{DE}}{\text{Pc}$	OW RATE CAL	Company By	- 12 =	226	sia (sia (Abs (sia (MCF/da
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SUMMA	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d)	$\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{DE}}{\text{D}^2 - \text{P}^2 \text{d}} = \frac{2}{\text{D}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 - \text{P}^2 \text{w}} = \frac{2}{\text{D}^2 - \text{P}^2 - \text{P}^$	OW RATE CAL = LIVERABILITY LIVERABILITY Mcf/day psia psia psia psia	Company By Title Witnessed by	=	226	sia (sia (Abs (sia (MCF/da
Cellhead tubing Cellhead t	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d)	FL V(a V(d) DE D2 - P2 D2 - P2 D2 - P2 D3 - P2 D4 - P2 D5 - P3	OW RATE CAL LIVERABILITY LIVERABILITY Mcf/day psia psia psia psia psia psia	COMPANY Company By Title Witnessed by Company	=	226	sia (sia (Abs (sia (MCF/da
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Cellhead tubing Cellhead t	g shut-in pressure (D whichever well flowe (Meter Run) (1) X d) ARY fraction factor	$\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{FL}}{\text{V(d)}}$ $\frac{\text{DE}}{\text{D}^2 \text{C} - \text{P}_d^2} = \frac{\text{DE}}{\text{D}^2 \text{C} - \text{P}_w^2} = \frac{\text{DE}}{\text{D}^2 \text{C}}$ REMA	OW RATE CAL SELIVERABILITY LIVERABILITY Mcf/day psia psia psia Mcf/day RKS OR FRICTI	COMPANY By Title Witnessed by Company Company 2 (1-e^-s)	-12 =	236 190 M	sia (sia (Abs (Sia (Abs (Sia (Abs (Abs (Abs (Abs (Abs (Abs (Abs (Abs

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