

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9-7-78																																																																																														
Company Caulkins Oil Company				Connection																																																																																															
Pool South Blanco				Formation Pictured Cliffs		Unit																																																																																													
Completion Date 8-30-78		Total Depth 4016		Plug Back TD 4016		Elevation 6655 Gr																																																																																													
Csg. Size 4 1/2		Wt. 10.5	d 4.00	Set At 4016	Perforations: From 2926 To 3002																																																																																														
Tbg. Size 1 1/4		Wt. 2.3	d 1.350	Set At 3910	Perforations: From 3910 To																																																																																														
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Commingle Single Gas				Packer Set At		Well No. 343																																																																																													
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a																																																																																													
L		H	Gg	% CO ₂	% N ₂	% H ₂ S																																																																																													
Prover		Meter Run		Taps																																																																																															
State New Mexico																																																																																																			
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="5">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td colspan="4">7 Day</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>1.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>582</td> <td></td> <td>441</td> <td></td> <td></td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>22</td> <td></td> <td>298</td> <td></td> <td></td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>							FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI	7 Day											1.							582		441			2.							22		298			3.												4.												5.											
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RATE OF FLOW CALCULATIONS																																																																																																			
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																																																																												
1.																																																																																																			
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NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ Specific Gravity Flowing Fluid _____ Critical Pressure _____ P.S.I.A. Critical Temperature _____ R																																																																																														
1.																																																																																																			
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P _c 594 P _c ² 352,836					(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____																																																																																														
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²																																																																																															
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AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ 1.37					SEP 10 1978 OH. DIST.																																																																																														
Absolute Open Flow 610 Mcfd @ 15.025 Pictured Cliffs - 70% of 610 = 427 McFPD Angle of Slope @ .75 Slope, n 1.2693																																																																																																			
Remarks:																																																																																																			
Approved By Commission: Conducted By: Calculated By: Checked By:																																																																																																			