

NEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA  
EXCEPT BARKER DOME STORAGE AREA)

Pool Basin Formation Dakota County Rio Arriba  
Purchasing Pipeline El Paso Natural Gas Co. Date Test Filed February 7, 1963

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Operator Consolidated Oil & Gas, Inc. Lease Tribal "C" Well No. 10-7  
Unit J Sec. 7 Twp. 26N Rge. 3W Pay Zone: From 7798 To 8006  
Casing: OD 5-1/2 WT. 17&15.5 Set At 3283-000' Tubing: OD 1-1/2" WT. 2.90 T. Perf. 7650  
Produced Through: Casing \_\_\_\_\_ Tubing X Gas Gravity: Measured .702 Estimated \_\_\_\_\_  
Date of Flow Test: From 1-3-63 To 1-10-63 \* Date S.I.P. Measured December 4, 1962  
Meter Run Size 4.000 Orifice Size 0.750 Type Chart L-10 Type Taps Flange

OBSERVED DATA

Flowing casing pressure (Dwt) Pictured Cliffs psig + 12 = \_\_\_\_\_ psia (a)  
Flowing tubing pressure (Dwt) 547 psig + 12 = 559 psia (b)  
Flowing meter pressure (Dwt) 544 psig + 12 = 556 psia (c)  
Flowing meter pressure (meter reading when Dwt. measurement taken):  
Normal chart reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (d)  
Square root chart reading (7.36)<sup>2</sup> x spring constant 10 = 542 psia (d)  
Meter error: (c) - (d) or (d) - (c) \_\_\_\_\_ = 14 psi (e)  
Friction loss, Flowing column to meter: \_\_\_\_\_ = 3 psi (f)  
(b) - (c) Flow through tubing: (a) - (c) Flow through casing  
Seven day average static meter pressure (from meter chart):  
Normal chart average reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (g)  
Square root chart average reading (7.35)<sup>2</sup> x sp. const. 10 = 540 psia (g)  
Corrected seven day avge. meter press. (P<sub>f</sub>) (g) + (e) = 554 psia (h)  
P<sub>t</sub> = (h) + (i) = 557 psia (i)  
Wellhead casing shut-in pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (j)  
Wellhead tubing shut-in pressure (Dwt) 1992 psig + 12 = 2004 psia (k)  
P<sub>c</sub> = (j) or (k) whichever well flowed through = 2004 psia (l)  
Flowing Temp. (Meter Run) \_\_\_\_\_ °F + 460 = \_\_\_\_\_ °Abs (m)  
P<sub>d</sub> = 1/2 P<sub>c</sub> = 1/2 (l) = 1002 psia (n)

$$Q = \frac{353}{(\text{integrated})} \times \left( \frac{\text{FLOW RATE CALCULATION}}{\frac{556}{\sqrt{(a)}} = 23.5796 = 1.013} \right)^* = 363 \text{ MCF/da}$$

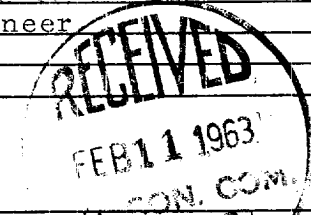
$$\frac{542}{\sqrt{(d)}} = 23.2809$$

DELIVERABILITY CALCULATION

$$D = Q \frac{363}{\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n} = \frac{3,012,012}{3,692,255} = .859 = 312 \text{ MCF/da.}$$

SUMMARY

P<sub>c</sub> = 2004 psia Company Consolidated Oil & Gas, Inc.  
Q = 363 Mcf/day By W. D. Williams  
P<sub>w</sub> = 569 567 psia Title Chief Engineer  
P<sub>d</sub> = 1002 psia Witnessed by \_\_\_\_\_  
D = 312 Mcf/day Company \_\_\_\_\_



- \* This is date of completion test.
- \* Meter error correction factor

REMARKS OR FRICTION CALCULATIONS

GL	(1-e <sup>-S</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> ) R <sup>2</sup>	P <sub>t</sub> <sup>2</sup> (Column i)	P <sub>t</sub> <sup>2</sup> + R <sup>2</sup>	P <sub>w</sub>
5370	0.323	35.641	12.938	310.249	323.187	569 567

OK

