

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 6-6-69					
Company Jerome P. M'Hugh					Connection					
Pool Ballard					Formation Pictured Cliffs					
Completion Date 5-21-69			Total Depth 2310		Plug Back TD		Elevation 6465		Farm or Lease Name Nordhaus	
Csg. Size 4 1/2	Wt. 9.5	d	Set At 2308	Perforations: From 2230 To 2249			Well No. 4			
Tbg. Size 1 1/4	Wt. 2.4	d	Set At 2250	Perforations: From open ended To			Unit Sec. Twp. Rge. K 17 25N 7W			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas					Packer Set At		County Rio Arriba			
Producing Thru Tbg		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico		
L	H	Gg 0.630	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							531		569	
1.										
2.										
3.	2	5/8		33		62			203	3 hrs
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							
2.							
3.	8.5417		45	9981	9759	1.000	374
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 581	P _c ² 337,561	(1) $\frac{\bar{P}_c^2}{P_c^2 - P_w^2} = 1.1586$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.133$
NO.	P _c ²	P _w	P _w ²
1.			
2.			
3.		215	46,225
4.			
5.			

Absolute Open Flow 424 Mcfd @ 15.025		Angle of Slope _____	Slope, n 0.85
Remarks: Light spray water			
Approved By Commission:	Conducted By: I. A. Dugan	Calculated By:	JUN 12 1969 By:

