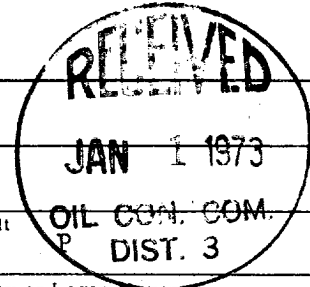


NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65



Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 12/19/72		
Company Pubco Petroleum Corporation			Connection El Paso Natural Gas		
Pool Otero Chacra			Formation Chacra		Unit P
Completion Date 11/27/72		Total Depth 3850'		Plug Back TD 3816'	Elevation 6444' GL
Csg. Size 3-1/2"	Wt. 9.2#	d 2.992	Set At 3846	Perforations: From 3518 To 3622	
Tbg. Size 1-1/4"	Wt. 2.3	d 1.380	Set At 3566'	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None	
Producing Thru Casing		Reservoir Temp. °F @		Baro. Press. - P <sub>g</sub> 12.00	
L		H		G <sub>g</sub> 0.6	
				% CO <sub>2</sub>	
				% N <sub>2</sub>	
				% H <sub>2</sub> S	
				Prover	
				Meter Run	
				Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							855		855		7 days
1.	1.995 x 0.75						340		124	60	1 hr.
2.	1.995 x 0.75						301		111	59	2 hrs.
3.	1.995 x 0.75						278		93	58	3 hrs.
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcfd
1.							
2.							
3.	9.604		105	1.002	1.291	1.013	1321
4.			1008.42	1010.44	1304.47	1321.43	
5.							

NO.	P <sub>t</sub>	Temp. °R	T <sub>f</sub>	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P <sub>c</sub> 867	P <sub>c</sub> <sup>2</sup> 751,689	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1259$	(2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1062$		
NO.	P <sub>t</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	$AOF = Q \left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1461$
1					
2					
3		290	84,100	667,589	
4					
5					

Absolute Open Flow 1461 Mcfd @ 15.025      Angle of Slope  $\theta$  \_\_\_\_\_      Slope, n .85

Remarks: \_\_\_\_\_

Approved By Commission:	Conducted By: R. J. Flaker	Calculated By: <i>J. C. Johnson</i>	Checked By:
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J. C. Johnson, Vice President Production