

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12/20/76																																																																																											
Company AMOCO PRODUCTION COMPANY				Connection Gas Company of New Mexico																																																																																													
Pool Tapacito				Formation Pictured Cliffs				Unit																																																																																									
Completion Date 12/12/76		Total Depth 3860		Plug Back TD 3826		Elevation 6963		Farm or Lease Name Jicarilla Apache 102																																																																																									
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 3859	Perforations: From 3734 To 3792				Well No. 17																																																																																									
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 3792	Perforations: From Open To Ended				Unit Sec. Twp. Rge. H 3 26 4																																																																																									
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None				County Rio Arriba																																																																																									
Producing Thru Thg.		Reservoir Temp. °F @		Mean Annual Temp. °F 90		Baro. Press. - P _a 12 psi		State New Mexico																																																																																									
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps																																																																																									
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td>8 days</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>952</td> <td></td> <td>955</td> <td></td> </tr> <tr> <td>1.</td> <td>2.375-inch</td> <td></td> <td>0.750</td> <td></td> <td></td> <td></td> <td>220</td> <td>60°</td> <td>350</td> <td></td> </tr> <tr><td>2.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>3.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>4.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>5.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> </table>										FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI	8 days						952		955		1.	2.375-inch		0.750				220	60°	350		2.											3.											4.											5.										
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NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																																																																										
1	12.365		232	1.000	.9608	1.023	2820																																																																																										
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NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P_c **967** P_c² **935,089**

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		362	131,044	804,045
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.1630}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.1369}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{3206}$

Absolute Open Flow 3206 Mcfd @ 15.025	Angle of Slope @ _____	Slope, n .85
Remarks: _____		
Approved By Commission:	Conducted By: T. M. Oliver	Calculated By: Oliver/Lindsley
		Checked By: P. C. Ellison