

Form C-122
Revised 10-1-78

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-14-80																																																																																															
Company SUPRON ENERGY CORPORATION		Connection Gas Company of New Mexico																																																																																															
Pool Blanco		Formation Mesaverde																																																																																															
Completion Date 6-25-80		Total Depth 8300	Plug Back TD 8230																																																																																														
		Elevation 7218	Form or Lease Name Jicarilla "G"																																																																																														
Csg. Size 7.625 5.500	Wt. 26.40 15.50	d 6.969 4.950	Set At 4130 3913-8247																																																																																														
Perforations: From 5474 To 6171		Well No. 7-M																																																																																															
Csg. Size 2.0625	Wt. 3.25	d 1.750	Set At 5854																																																																																														
Perforations: From 5783 To 5789		Unit Sec. Twp. Rge. 0 11 26N 5W																																																																																															
Type Well - Single - Brodenhead - G.C. or G.O. Multiple Dual - Gas - Gas			Packer Set At 7980																																																																																														
Producing thru Tubing		Reservoir Temp. °F p	Mean Annual Temp. °F 12																																																																																														
County Rio Arriba		State New Mexico																																																																																															
L 5774	H	Gg 0.650	% CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps																																																																																														
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td>2"</td> <td></td> <td>3/4"</td> <td></td> <td></td> <td></td> <td>780</td> <td></td> <td>780</td> <td></td> <td>14 days</td> </tr> <tr> <td>1.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>71</td> <td>58°</td> <td>624</td> <td></td> <td></td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>				FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI	2"		3/4"				780		780		14 days	1.							71	58°	624			2.												3.												4.												5.											
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RATE OF FLOW CALCULATIONS																																																																																																	
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																																																																										
1	12.3650		83	1.0019	0.9608	1.000	988																																																																																										
2.																																																																																																	
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NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ Specific Gravity Flowing Fluid _____ Critical Pressure _____ P.S.I.A. Critical Temperature _____ R																																																																																												
1					X X X X X X X X																																																																																												
2					X X X X X																																																																																												
3																																																																																																	
4																																																																																																	
5																																																																																																	
NO.	P _r	P _w	P _w ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 2.8158$ (2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2.1737$																																																																																												
1		636	404,496	222,768																																																																																													
2																																																																																																	
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4																																																																																																	
5																																																																																																	
Absolute Open Flow 2148 Mcfd @ 15.025					Angle of Slope 0.75		Slope, n 0.75																																																																																										
Remarks:																																																																																																	
Approved By Division		Conducted By		Calculated By		Checked By																																																																																											
				Kenneth E. Roddy																																																																																													