OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

JUL 23 1982
OIL CON. DIV.
DIST. 3

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: XX Initial ☐ Annual ☐ Special				Test Date: 7-15-82	
Company: Caulkins Oil Company		Connection:			
Pool: Basin Dakota		Formation: Dakota		Unit: M	
Completion Date: 7-8-82	Total Depth: 7489	Plug Back TD: 7489	Elevation: 6628	Farm or Lease Name: Sanchez	
Csg. Size: 5½ / Wt.: 17# / 15.5# / d: 4.950 / 4.892 / Set At: 7489		Perforations: From 7410 To 7159		Well No.: 4-E	
Tbg. Size: 2 1/16 / Wt.: 3.25 / d: 1.750 / Set At: 7342		Perforations: From 7342 To		Unit: M / Sec.: 25 / Twp.: 26N / Rge.: 6W	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Gas - Gas Multiple		Packer Set At: 5589		County: Rio Arriba	
Producing Thru: Tubing	Reservoir Temp. °F: @	Mean Annual Temp. °F:	Baro. Press. – P_a:	State: New Mexico	
L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI							1653		617		7-Days
1.							213		1209		3-Hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	14.1605		225	1.000	1.000	1.000	3,186
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1665 P_c^2 2,772,225

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	50,625		579,021	2,193,204
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.264$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1921$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3,798$

Absolute Open Flow 3,798 Mcfd @ 15.025 | Angle of Slope θ 75 | Slope, n

Remarks:

Approved By Division	Conducted By:	Calculated By:	Checked By: