

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		7-23-74		
Company				Connection								
Universal Resources Corp												
Pool				Formation				Unit				
Basin - Dakota				Dakota 2								
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name				
7-12-74		2228'		6190'		6403' RKB		Grigsby - Federal				
Csg. Size		Wt.		d		Set At		Perforations:		Well No.		
4 1/2"		10.5#		4.052		6228'		From 6009' To 6060'		2		
Tbg. Size		Wt.		d		Set At		Perforations:		Unit Sec. Twp. Rge.		
1 1/4"		2.4#		1.380		6031' RKB		From Open End To		N 7 25N 10W		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County				
Single G.O.								San Juan				
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State				
Tbg.		@						New Mexico				
✓		H		Gg		% CO ₂		% N ₂		% H ₂ S		
				.620 Est						Prover		
										Meter Run		
										Taps		
FLOW DATA					TUBING DATA			CASING DATA			Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F		
SI							1785		1770		7 days	
1.									960		21 Hrs	
2.									630		65 Hrs	
3.												
4.												
5.												
RATE OF FLOW CALCULATIONS												
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd					
1							2105					
2							1450					
3												
4												
5												
NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.							
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.							
2					Specific Gravity Separator Gas _____ X X X X X X X X							
3					Specific Gravity Flowing Fluid _____ X X X X X							
4					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.							
5					Critical Temperature _____ R _____ R							
P _c 1797 P _c ² 3,229,209												
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.4135^{(2)}}{1.1012^{(4)}}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.2963^{(2)}}{1.0750^{(4)}}$							
1												
2	972	744,784	2,234,425		[$\frac{P_c^2}{P_c^2 - P_w^2} $] ⁿ = $\frac{2729^{(2)}}{1559^{(2)}}$							
3												
4	630	396,900	2,232,899									
5												
Absolute Open Flow 2729 ⁽²⁾ 1549 ⁽⁴⁾					Mcf @ 15.025					Angle of Slope @ _____		Slope, n .75
Remarks: _____												
Approved By Commission: _____ Conducted By: _____ Calculated By: _____ Checked By: _____												
Cresc & Ivic Jacobs												