

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date					
Company <i>Universal Resources Corp.</i>					Connection					
Pool <i>Basin - Dakota</i>					Formation <i>Dakota</i>					
Completion Date <i>10-16-74</i>			Total Depth <i>6375'</i>		Plug Back TD		Elevation		Farm or Lease Name <i>Griffin Fed</i>	
Csg. Size	Wt.	d	Set At	Perforations: From To				Well No. <i>3</i>		
Tbg. Size	Wt.	d	Set At	Perforations: From To				Unit Sec. Twp. Rge. <i>D 8 25N 10W</i>		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At		County <i>San Juan County</i>			
Producing Thru		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State <i>New Mexico</i>		
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Tcps		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							<i>1766</i>		<i>1797</i>		<i>7 days</i>
1.									<i>705</i>		<i>21 Hrs</i>
2.									<i>535</i>		<i>45 Hrs</i>
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2							<i>1734</i>
3							
4							<i>1300</i>
5							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

NO.	P _t ²	P _w ²	P _w ²	P _c ² - P _w ²	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.1764^{(2)}}{1.1006^{(2)}} \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^{n^{.75}} = \frac{1.1367^{(2)}}{1.0745^{(2)}}$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1971^{(2)}}{1397^{(2)}}$
1					
2		<i>717</i>	<i>514,069</i>	<i>2,758,392</i>	
3					
4		<i>547</i>	<i>299,209</i>	<i>2,973,272</i>	

Absolute Open Flow <i>1971</i> ⁽²⁾ <i>1397</i> ⁽²⁾ Mcfd @ 15.025		Angle of Slope θ _____	Slope, n _____
Remarks: _____			
Approved By Commission:		Conducted By: <i>Crane</i>	Calculated By: <i>Jaco 63</i>
		Checked By:	