

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 7-14-80						
Company El Paso Natural Gas Company					Connection						
Pool Basin					Formation Dakota					Unit San Juan	
Completion Date 6-26-80			Total Depth 8535'		Plug Back TD 8541		Elevation 7229'G1		Farm or Lease Name San Juan 27-4		
Csg. Size 9.625	Wt. 40.0	d 8.835	Set At 4500'		Perforations: From *8302 To 8530'				Well No. Unit #132 (DK)		
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 8520		Perforations: From To				Unit Sec. Twp. Rge. B 27 27 4		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G.G. Dual					Packer Set At 6713'				County Rio Arriba		
Producing Thru Tbg.		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a			State New Mexico		
L 8520'	H	G _g .670	% CO ₂		% N ₂		% H ₂ S		Prover	Meter Run 4"	Taps Flg.

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1920				18 Days
1.	4"	X	2.75			60	82				3 Hr.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	41.10	18.59	44	1.000	1.222	1.000	934
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	0.123	520	1.36	1.000	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1932 P _c ² 3,732,624				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	1936	168	28244	3704380
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0076$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 939$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0057$

Absolute Open Flow 939 Mcfd @ 15.025		Angle of Slope θ _____		Slope, n .75	
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Remarks: * 4 1/2" Liner (6749' to 8549')

Gas Vented During Test - 154 MCF Produced - 5.0 Bbls Oil 12.2 Bbls Water

Approved By Commission:	Conducted By: R. Hardy	Calculated By: B. Clark	Checked By:
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