

OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENTP. O. BOX 2088
SANTA FE, NEW MEXICO 87501Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 1-5-85	
Company Consolidated Oil & Gas, Inc.				Connection NW	
Pool Basin Dakota				Formation Dakota	
Completion Date 11-17-84		Total Depth 8320		Plug Back TD 8271	
				Elevation 7064 GR	
Farm or Lease Name Champlin					
Csg. Size 5 1/2		Wt. 15.5#		Set At 4.950	
				Perforations: From 8051 To 8240	
Trg. Size 1 1/2"		Wt. 2.76		Set At 1.610	
				Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual gas				Packer Set At 7732	
Producing Thru Tbg.		Reservoir Temp. °F 182 @ 8146		Mean Annual Temp. °F 12.0	
				Baro. Press. - P _a New Mexico	
L		H		Gg	
				.650 Est.	
				% CO ₂	
				% N ₂	
				% H ₂ S	
				Prover 2" critical flow prover	
				Meter Run	
				Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	15 days						1337		1434		
1.	2" X 3/4"						31	71			3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	9.453		43	0.9896	1.240	1.000	499
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1349	P _c ² 1819801		
NO.	P _t	P _w	P _c ² - P _w ²
1		27131	1792670
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0151$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0112$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 505$$

Absolute Open Flow	505	Mcf @ 15.025	Angle of Slope @	53.13°	Slope, n	.75
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Remarks:

Approved by Division	Conducted By: R. Housh	Calculated By: N. Tefteller	Checked By:
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