NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JAN 10 1969
OIL CON. COM.
DIST. 3

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 1-8-69	
Company: Skelly Oil Company	Connection: Unconnected			Unit
Pool: Undesignated	Formation: Fruitland			
Completion Date: 12-30-68	Total Depth: 5175	Plug Back TD: 1158	Elevation: 5994	Farm or Lease Name: Navajo "L"
Csg. Size: 5.500 / Wt.: 14# / d: 5.012 / Set At: 5175		Perforations: From 1130 To 1147		Well No.: #1
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 1145		Perforations: From 1131 To 1135		Unit: I / Sec.: 11 / Twp.: 26N / Rge.: 12W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: —		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F: 60 @	Mean Annual Temp. °F	Baro. Press. – P_a: 12.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
1131	1131	60				2.000		

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					373		373		
1.	2 x 3/4				118	60	140	60	1 hr
2.					98		135		2 hr
3.					87		122		3 hr
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		130.2	1.0000	1.291	1.010	1849
2.	11.00		110.2	1.0000	1.291	1.010	1565
3.	11.00		99.2	1.0000	1.291	1.010	1409
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 385.2 P_c^2 148379

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1				
2				
3	9840	134.2	18009	130370
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1381$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1162$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1573$

Absolute Open Flow 1573 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .85

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	R.P. Hergenreter	R.P. Hergenreter	M.C. Mahnell