## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

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Revised	12	-]	L <del>-</del> 55

Pool	Basin D	akota		Fc	ormation	Da	kota		_County	San	Jud	
Initial XX Annual Special Date of Test 1-8-64												
Unit P Sec. 6 Twp. 26-M Rge. 8-W Purchaser Mi Pase Natural Gas Go.												
Casing <u>k-1/2</u> Wt. <u>10.50 I.D. k.052 Set at 6620 Perf. 6318 To 6578</u>												
Tubing 1-1/2 Wt. 2.90 I.D. 1.610 Set at 6543 Perf. 6533 To 6543												
Gas Pay: From 6318 To 6578 L 6533 xG .740 -GL 4834 Bar. Press. 12.0												
Producing Thru: Casing Tubing IX Type Well Single Ges  Single-Bradenhead-G. G. or G.O. Dual												
rrou	ucing inru:	. vas	stuß	-0 /h	1 (1)	o).tig	Sing	lype we gle_Brade	nhead-G.	G. or G	.O. Dual	
Date	of Complet	ion:_	12	-10-6	Packer		-	Keservo	ir Temp			
						OBSERV.	ED DATA					
Test	ed Through	(Prov	<u>rer) ((</u>	Choke)	(Meter)				Туре Тар	8		
			low Da					Tubing Data		ata		
Na	(Prover) (Line)				Diff.	Temp.	Press.	Temp.	Press.	Temp.	Duration of Flow	
No.	(Line) Size			psig	h <sub>w</sub>	°F.	psig	o <sub>F</sub> ,	psig	op.	Hr.	
SI					†		2110		2086		21 days	
1.	2 <sup>tt</sup>	3/	4	212		78	273	780	1115		3 hre.	
2.		ļ		<u> </u>				7.				
3. 4.		<del> </del>								<u> </u>		
5.												
						OT CHE CAT	CULATION:					
<u>-</u>	Coeffici	ent		Pı					Compre	55.	Rate of Flow	
No.						Fac	tor	<b>Factor</b>	Facto	r	Q-MCFPD	
	(24-Hour) 7		√ h <sub>w</sub> i	p <sub>f</sub> psia		F	<u> </u>	Fg	Fpv		● 15.025 psia	
1.	12.3650	<b>)</b>			224	.9831		.9005	1.026		2516	
2.								- <del></del>				
3. 4.										<del>-</del>		
5.		<del>****                                 </del>										
<u> </u>						DOCUME O	A C OVER A SET	ONG				
					PR	ESSURE C	ALCUIATIO	UNS				
	iquid Hydro					cf/bbl.					erator Gas	
Gravity of Liquid Hydrocarbons					deg.			Speci	Specific Gravity Flowing Fluid Pc 4502.9			
Fc	. <u></u>		(;	1-e <sup>-8</sup> )			•	Pc	6.14.6	_ <sup>P</sup> c	4,70247	
	$P_{\mathbf{W}}$		, _		()2	/_	2	<b>D</b> 0	$P_c^2 - P_w^2$	0.		
No.	D. (main)	P	F F	cQ	$(F_cQ)^2$	(1	cQ) <sup>2</sup> -e <sup>-s</sup> )	$P_{\mathbf{w}}^2$	Pc-Pw		Property Pc	
1.	Pt (psia)				<del></del>		<del></del>	1270.1	3232.8		OT THE STATE OF TH	
2.									32,32,44		INVEN	
<b>  3.</b>										/ Ki	CHITCH	
4. 5.											AN 28 1964	
					<del></del>				<del></del>	<del>-14</del>	COM.	
Absolute Potential: 3226 MCPPD; n .75 CON. COM. COM. COMPANY Southern Union Production Company												
	PANY Sout	nera O. B.	WILLIAM .	Far	mington,	New Max	de	Original Sign	ed By		<u> </u>	
AGENT and TITLE Verne Rockhold - Jr. Engineer VERNE ROCKHOLD												
WITNESSED Herren Hearelly												
COMPANY El Pago Natural Gas Company  (3) N. Mor. O.C.C. REMARKS												
(3) N. Mex. O.C.C. REMARKS (1) Hr. Paul J. Clote												
(1) Kl Paso Natural Gas Co., Proration Dept.												
P.O. Box 1492, Kl Paso, Texas												
		H.	L. Kin	dricks	, Box 9	yu, far	arngron,	# ofic				

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q Tactual rate of flow at end of flow period at W. H. working pressure  $(P_w)$ . MCF/da. @ 15.025 psia and 60° F.
- $P_c$  72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw- Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{W}$  cannot be taken because of manner of completion or condition of well, then  $P_{W}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{t}$ .