

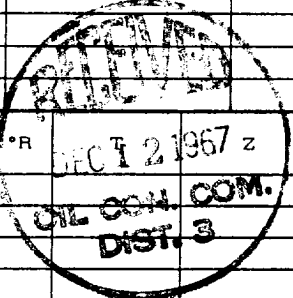
NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 12/7/67	
Company Southern Union Production Co.				Connection El Paso Natural Gas Company		
Pool Basin				Formation Dakota		Unit
Completion Date 11/17/67		Total Depth 7350		Plug Back TD 7331		Elevation 7022
Farm or Lease Name Nickson						
Csg. Size 4-1/2"	Wt. 10.50#	d	Set At 7349	Perforations: From 7098 To 7318		Well No. 12
Tbg. Size 1-1/2"	Wt. 2.90	d	Set At 7203	Perforations: From 7195 To 7203		Unit Sec. Twp. Rge. F 35 26N 8W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At		County San Juan
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12
State New Mexico						
L 7185	H	G _g .700	% CO ₂	% N ₂	% H ₂ S	Prover
Meter Run		Taps				

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"				2362		2358		14 days
1.							240	62	1037		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		252	.9981	.9258	1.030	2,966
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R		Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
1.				A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
2.				Specific Gravity Separator Gas _____ X X X X X X X X			
3.				Specific Gravity Flowing Fluid _____ X X X X X			
4.				Critical Pressure _____ P.S.I.A. _____ P.S.I.A.			
5.				Critical Temperature _____ R _____ R			

P _c 2374	P _c ² 5,635,876		
NO.	P _c ²	P _w	P _w ²
1	63,504	1049	1,100,401
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.2426}{1.2426 - 1.1004} = 1.2426$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.1768}{1.1768 - 1.1004} = 1.1768$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3,490$$

Absolute Open Flow 3,490 Mcfd @ 15.025	Angle of Slope θ _____	Slope, n .75
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Remarks: Witnessed by Don Norton	
ORIGINAL SIGNED BY WAYNE WARRINGTON	
Approved By Commission:	Conducted By: W. Warrington
Calculated By: W. Warrington	Checked By: W. Warrington