STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

1 - El Paso, Clark

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [XX] Initial [ ] Annual [ ] Special				Test Date: 6-4-81	
Company: Dugan Production Corp.			Connection:		
Pool: Bisti			Formation: Dakota ~~& Mancos~~		Unit:
Completion Date: 5-22-81	Total Depth: 5800'		Plug Back TD: 5761'	Elevation: 6142 GL	Farm or Lease Name: Windfall
Csg. Size: 5½" / Wt.: 20# / d: 4.778 / Set At: 5800			Perforations: From 4704 To 5736		Well No.: #10
Tbg. Size: 2-3/8" / Wt.: 4.7# / d: 1.995 / Set At:			Perforations: From open end To		Unit: F / Sec.: 31 / Twp.: 26N / Rge.: 11W
Type Well – Single – Bradenhead – G.C. or G.O. Multiple: downhole comingled Dakota & Mancos gas			Packer Set At: ---		County: San Juan
Producing Thru: tubing	Reservoir Temp. °F: 163° @ 5736'	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.2		State: NM

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
		.65						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						1250	90	2510	90	305 hrs.
1.										
2.										
3.	3/4"					175	96	810	90	3 hrs.
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							
3.	12.365		187	.9671	.9608	1.01	2,170
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXX
Specific Gravity Flowing Fluid _____ XXXXX
Critical Pressure _____ P.S.I.A.
Critical Temperature _____ R

RECEIVED
JUN 12 1981
OIL CON. COM.
DIST. 3

P_c 2522 P_c^2 6,360,464

NO	P_t	P_w	P_w^2	$P_c^2 - P_w^2$
1				
2				
3		822	675,684	5,684,800
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1189$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^{\cdot} = 1.0879$

OR $Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2361$

Absolute Open Flow 2361 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n .85

Remarks: heavy mist of 60% wtr. & 40% oil

Approved By Division	Conducted By: Crane	Calculated By: Donovan	Checked By: