

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 04-01-77						
Company Merrion & Bayless				Connection							
Pool N.I.I.P.				Formation Picture Cliff		Unit					
Completion Date 03-14-77		Total Depth 1260'		Plug Back TD 1215'		Elevation 5958'					
Csg. Size 2-7/8"		Wt. 6.5#/ft.	d 2.441	Set At 1252'	Perforations: From 1133' To 1139'						
Tbg. Size		Wt.	d	Set At	Perforations: From To						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single (no tubing)				Packer Set At		Well No. 2					
Producing Thru Casing		Reservoir Temp. °F 77° @ 1136'		Mean Annual Temp. °F 60°F		Baro. Press. - P _a 12.2 PSIA					
L 1136		H 1136	Gg 0.65 est	% CO ₂	% N ₂	% H ₂ S					
				Prover 2"	Meter Run	Taps					
FLOW DATA				TUBING DATA		CASING DATA					
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	8 day		1/4"	66					231	58°	
2.	2"								66	58°	.50 Hrs.
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1.	1.087		78.2	1.002	1.240	1.008	107				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ Specific Gravity Flowing Fluid _____ Critical Pressure _____ P.S.I.A. P.S.I.A. Critical Temperature _____ R R						
1.					X X X X X X X X						
2.					X X X X X						
3.											
4.											
5.											
P _c 243.2 P _c ² 59146					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{59,146}{53,008} = 1.116 \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.098$						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 118$						
1.	6.12	78.35	6139	53,008							
2.											
3.											
4.											
Absolute Open Flow <u>118</u> Mcfd @ 15.025 Angle of Slope <u>0.85</u>					Slope, n <u>0.85</u>						
Remarks:											
Approved By Commission:		Conducted By: Steven S. Dunn		Calculated By: <i>Steven S. Dunn</i>		Checked By: Robert L. Bayless					