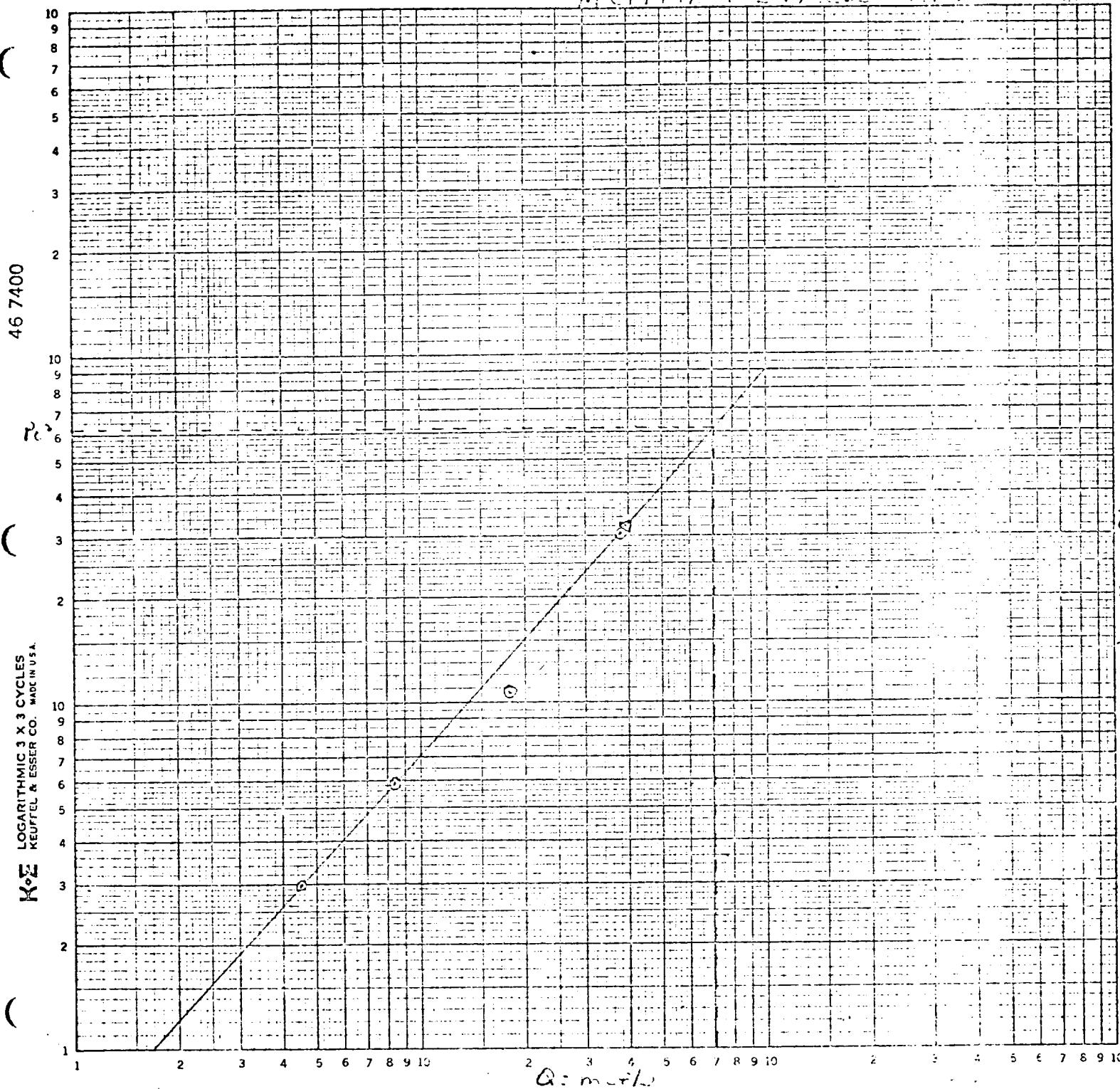


Form C-122
Revised 9-1-65

Type Test		☐ Initial		☐ Annual		☒ Special		Test Date		5-19-77	
Company				Connection							
Merrion & Bayless				New Well							
Pool				Formation				Unit			
NIIP				Pictured Cliffs							
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
May 2, 1977		1315'		1265'		5979' GR		Chaco			
Csg. Size		Wt.		Set At		Perforations:		Well No.			
2.875		6.5 lb.		2.441		1288'		From 1165'		To 1192'	
Tbg. Size		Wt.		Set At		Perforations:		Unit Sec. Twp. Rge.			
none						To		SE/SE 1 26 13			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County			
Gas - Tubingless Completion						none		San Juan			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State			
Casing		@				12.0		New Mexico			
L		H		G _g		% CO ₂		% N ₂		% H ₂ S	
				.60						Prover 2"	
										Meter Run	
										Taps	
FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI									238		SIP
1.	2" x 3/32"			232		60°			232		2 hr.
2.	2" x 1/8"			226		62°			226		2 hr.
3.	2" x 3/16"			216		60°			216		2 hr.
4.	2" x 5/16"			166		55°			167		2 hr.
5.	2" x 5/16"			161		58°					12 hr.
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	0.1410		244	1.000	1.291	1.021	45				
2	0.2648		238	.9981	1.291	1.021	83				
3	0.6082		228	1.000	1.291	1.021	183				
4	1.672		178	1.005	1.291	1.016	392				
5	1.672		173	1.008	1.291	1.016	382				
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
P _c 250 P _c ² 62500											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____						
1		244	59536	2964	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____						
2		238	56644	5856							
3		228	51984	10516							
4		178	31684	30816							
5		173	29929	32571							
Absolute Open Flow 710 Mcfd @ 15.025 Angle of Slope 42.5 Slope, n .92											
Remarks: Well produced dry gas throughout test.											
Approved By Commission:			Conducted By: Fred S. Hamrick			Calculated By: Fred S. Hamrick			Checked By: Steven S. Dunn, Engr.		

Merriam - E. y loss (1.5)



○ 2 hr flow front

△ 12 hr extended flow front

N = .93

A = 0.00015