

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 7/23/80	
Company Hill & Llewellyn <i>Supron</i>						Connection	
Pool Ballard				Formation Pictured Cliffs		Unit	
Completion Date		Total Depth 2350		Plug Back TD 2320		Elevation	
Csg. Size 2.875		Wt. 6.50		Set At 2320		Perforations: From 2074 To 2156	
Tq. Size None		Wt. d		Set At		Perforations: From To	
Type Well - Single - Prodenhead - G.G. or G.O. Multiple Single						Packer Set At	
Producing Thru Casing		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a	
L		H		Gg .650 est		Prover	
				% CO ₂		% N ₂	
				% H ₂ S		Meter Run	
						Taps	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.
NO.						Temp. °F	Press. p.s.i.g.
1.							
2.							
3.							
4.							
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super. Compens. Factor, Fpv	Rate of Flow Q, Mcfd
1.	12.365		130	.9981	.9608	1.000	1542
2.							
3.							
4.							
5.							
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/cbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ Specific Gravity Flowing Fluid _____ Critical Pressure _____ P.S.I.A. Critical Temperature _____ °R		
1.							
2.							
3.							
4.							
5.							
P _c 394 P _c ² 155326					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1803$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1513$		
NO.	P _r	P _w	P _r ²	P _w ²			
1.	16900	154	23714	131522			
2.							
3.							
4.							
5.							
Absolute Open Flow 1775 Mcfd @ 15.025					Angle of Slope θ _____		Slope, n .85
Remarks:							
Approved by Commission:		Conducted By: CRW		Calculated By: <i>[Signature]</i>		Checked By:	

