

OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form O-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 12/15/80							
Company Supron Energy Corp (John Hill)			Connection								
Pool Ballard		Formation Pictured Cliffs		Unit							
Completion Date 12/8/80		Total Depth 3000	Plug Back TD	Elevation 6800 G	Farm or Lease Name Newsom B						
Csq. Size 2.875	Wi. 6.5	d 2.441	Set At 2976	Perforations: From 2774 To 2800							
Trq. Size None	Wi.	d	Set At	Perforations: From To							
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At							
Producing Thru Casing		Reservoir Temp. °F #	Mean Annual Temp. °F	Baro. Press. - P _a							
L	H	Gg est. .650	% CO ₂	% N ₂	% H ₂ S						
Prover		Meter Run		Taps							
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI									578		7 Days
1.			.750	6		50			6		3 Hrs.
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	12.3650		18	1.0098	.9608	1.0000	216				
2.											
3.											
4.											
5.											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
P _c 590		P _c ² 348100									
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0014$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0012$				
1	324	22	501	347599	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 216$						
2											
3											
4											
5											
Absolute Open Flow 216				Mcfd @ 15.025		Angle of Slope θ _____ Slope, n = .85					
Remarks: Dry throughout test											
Approved by Division			Conducted By: CRW			Calculated By: <i>W. Kendrick</i>			Checked By:		

