

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 9/3/81	
Company Supron Energy Corporation				Connection	
Well Ballard				Formation Pictured Cliffs	
Completion Date 8/27/81		Total Depth 3077		Plug Back TD 3068	
Elevation 6998 G		Farm or Lease Name Newsom A			
Csg. Size 2.375	Wt. 6.4	d 2.441	Set At 3084	Perforations: From 2928 To 2958	
Tub. Size None	Wt.	d	Set At	Perforations: From To	
Type Well - Single - Brandedhead - G.C. or G.C. Multiple Single				Packer Set At	
Producing Thru Casing				State New Mexico	
Reservoir Temp. °F B		Mean Annual Temp. °F		Baro. Press. - P ₀	
L	H	G ₀ est. .650	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
ID.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI									692		7 days
1.			.750	32		58			32	58	3 Hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		44	1.0019	.9608	1.0000	524
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons <td>Deg.</td>	Deg.
2.					Specific Gravity Separator Gas <td>X X X X X X X X</td>	X X X X X X X X
3.					Specific Gravity Flowing Fluid <td>X OIL X CON. COM.</td>	X OIL X CON. COM.
4.					Critical Pressure <td>DIST. 3. P.S.I.A.</td>	DIST. 3. P.S.I.A.
5.					Critical Temperature <td>R H</td>	R H

P _c 704	P _c ² 495616	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0061$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0052$
NO. 1	F _t ² 1936	P _w ² 55	P _w ² - P _w ² 492589
2			
3			
4			
5			

Absolute Open Flow 527 Mcfd @ 15.025		Angle of Slope	Slope, n .85
Remarks: Dry.			
Approved By Division	Conducted By: CRW	Calculated By: <i>AK</i>	Checked By: