DIST. 3

1-WD

NEW MEXICO OIL CONSERVATION COMMISSION

1-D 1-F

Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

| | | | | MULTI- | POINT B | ACK PRES | SURE TE | ST FOR GAS | WELLS | | Revised 12-1-55 |
|---|--------------------------------|---------------------|----------------------|--|----------------------------|--------------|-------------------|--|---|-----------------|--|
| Pool | Basin D | akota | · | Fo | rmation | Dak | ota | | _County | San | Juan |
| Init | ialX | alXAnnual_ | | al | | Spec | ial | Date of Test | | | 12/21/61 |
| Comp | any Southw | est Pr | oducti | on Comp | any | Lease | Hancock | Federal | Well | l No | 2 |
| Unit | M | Sec1 | 4 Tw | . 27 | Rg | e. <u>11</u> | Pur | chaser | 1 Paso Na | tural (| Gas Company |
| Casi | ng 41 | Wt. 10 | .50# _I , | D. 4.0 | 40 _{Se} | t at_ 66 | 5 78 P | erf. 652 | 27 | ro6! | 558 |
| Tubi | ng 1½ | Wt. 2. | 75 I. | D. 1.6 | 10 Se | t at 65 | 510 P | erf. Open | n : | Γο | End |
| | | <u></u> | | \ <u></u> | | | | \ <u>.</u> | | | ess. 12.0 |
| | | | | | | | | | | | |
| Date | ucing Thru | tion: | 12-1-6 | - | Packe | r | Si | ngle-Brade | enhead-G. (| G. or (| .0. Dual |
| Dave | Or COMPTC | 01011 | <u> </u> | • ···································· | | | ED DATA | | ,11 1 0m 15 | | |
| m+ | ad Missassah | 4 2 2222 | ****** | 311 \ | / | | | | | _ | |
| Tested Through (Choke) (Matsack) Type Taps Flow Data Tubing Data Casing Data | | | | | | | | | | | |
| \top | (Prover) | (Ch | oke) | Press. | Diff. | Temp. | Press | g Data • Temp. | Casing Daress. | Temp. | Duration |
| No. | (Line) Size | (Ori | fice) ize | psig | h_{W} | °F. | psig | °F. | psig | °F∙ | of Flow Hr. |
| SI | | | | 365 | | | 2021 | | 2021 | | 10 day |
| 1. 2. | | 3/4" | | 385 | | 62 | 385 | 62 | 1480 | | 3 hr |
| 3. | | 1 | | | | | | | | | |
| 4. 5. | | | | | | | | | | | |
| | | | | | | FLOW CAL | CULATIO | NS | | | |
| No. | Coeffic | Coefficient | | | Pressure Flow Temp. Factor | | | Gravity Compress. Rate of Flow Factor Factor Q-MCFPD | | | |
| 110 | (24-Ho | ur) | $r)$ $\sqrt{h_{Wl}}$ | | psia | Ft | | F _g F _p | | | |
| 1. 2. 3. 4. 5. | 12,3650 | | | | 77 | .9981 | | .9463 | 1.046 | | 4,849 |
| 2• 3• | | | | | | | | | | | |
| <u>4.</u> | | | | | | | | ···· | | | |
| | iquid Hydr ty of Liqu | | rocarbo | | | cf/bbl.deg. | | Speci Speci Pc | fic Gravit 2.033 | ty Flow Pc 4 | arator Gas wing Fluid 133.0 226.0 |
| No. | P _w Pt (psia) | P. | E F | Q | $(F_cQ)^2$ | (F (1 | (cQ) ² | P _w 2 | P _c -P _w ² | 1 | Pw Pc |
| <u></u> ;- | <u> </u> | | | | | | | 4133.0 | 1907.0 | <u> </u> | .733 |
| 2. 3. | | | | | | | | | | | |
| 1. 2. 3. 4. | | | | | | | | | | | |
| Abso COMP ADDRI AGEN | ESS 207 T and TITL ESSED | thwest | 8,6 Produ Gibu | ction (| Company Farming | | n .7 | | | | |
| O OFIF | | | | | | RE | ARKS | | 1790 | MFD | |
| | | | | | | | | | / Wron | a 1061 | () |
| | | | | | | | | | DEC 2 | 9 1961 | . <i>]</i> |

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_W) . MCF/da. @ 15.025 psia and 60° F.
- P_c 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P_{f} Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fow Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\mathbf{w}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{w}}$ must be calculated by adding the pressure drop due to friction within the flow string to P_{+} .