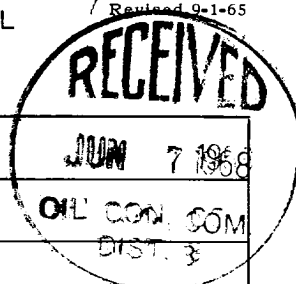


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65



Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-24-68				
Company PAN AMERICAN PETROLEUM CORP.				Connection None					
Pool Basin				Formation Dakota				Unit	
Completion Date 5-15-68		Total Depth 6063		Plug Back TD 6017		Elevation / 208 GL 5765/ 5778		Farm or Lease Name Federal Gas Com "K"	
Csg. Size 4-1/2	Wt. 10.5	d 4.052	Set At 6053	Perforations: 5870 To 5887 From 5901 To 5908		Well No. 1			
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 5948	Perforations: 5922 To 5948 From 5893 To 5899		Unit Sec. Twp. Rge. D 7 27 12			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At None		County San Juan		
Producing Thru Casing		Reservoir Temp. °F 90° @ T.D.		Mean Annual Temp. °F Est. 60°		Baro. Press. - P _a 12 PSIA		State New Mexico	
L 5909	H 5909	Gg .700 est.	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Line Size	X	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	8 days					1823		1824	
1.	2"	.750	830			1139		830	60° est. 3 Hrs.
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		842	1.000	.9238	1.113	10,728
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1836	P _c ² 3,370,896	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{3,370,896}{2,046,095}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4541$
NO	P _w	P _w ²	P _c ² - P _w ²
1	1151	1,324,801	2,046,095
2			
3			
4			
5			

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 15,600$

$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 15,600$

Absolute Open Flow 15,600 Mcfd @ 15.025	Angle of Slope θ _____	Slope, n .75
Remarks: _____		

Approved By Commission:	Conducted By: B. D. Dukas	Calculated By:	Checked By: E. R. Hirst
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