| | Form C-122 | | | | | | | | |
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| | Revised 12-1-55 | | | | | | | | |
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| en Juan | | | | | | | | | |
| | 3-11-60 | | | | | | | | |
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| ing r G | .O. Dual | | | | | | | | |
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| р. | Duration | | | | | | | | |
| | of Flow Hr. | | | | | | | | |
| | 7-day | | | | | | | | |
| | 3-hour blow | | | | | | | | |
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| | Rate of Flow Q-MCFPD | | | | | | | | |
| | @ 15.025 nsia | | | | | | | | |

| | | | MUL | TI-POIN | T BACK PI | RESSURE 1 | EST FOR G | AS WELLS | | Revised 12-1-55 | | |
|---|------------------------------|-----------------|-------------------------------|-----------------|------------------------|---|--|--------------------------------|----------------|---|--|--|
| Pool Angel Pooks Fo | | | | | ormation <u>Dakota</u> | | | | Sen | Juan | | |
| Initial X Annual_ | | | | | | | | | Te st | 3-11-60 | | |
| Company Pubeo Petroleum Corp. | | | | | Lease | | od | Well No. | | 2 | | |
| Unit <u>r.</u> Sec. 34 Twp. 28W | | | | | _Rge1 | PuPu | rchaser_ | chaser El Pago Natural Gas Co. | | | | |
| Casing 51 Wt. 151 I.D. Set at 6668 Perf. 6394 To 6530 | | | | | | | | | | | | |
| Tubing 2" Wt. 4.7 I.D. | | | | | _Set at | | Perf. | | _To | | | |
| (las | Pay: From_ | 6 394 T | °65 30 | L_ | L 6554 xG | | | Bar.Press | | | | |
| Producing Thru: Casing Tubing Tubing Type Well Single—Bradenhead—G. G. or G.O. Dual | | | | | | | | | | | | |
| Dat | e of Complet | ion: <u>2</u> - | 29-60 | Pa: | cker | | Single-Bradenhead-G. G. or G.O. I Reservoir Temp. 138 | | | | | |
| | | | | | OBSE | ERVED DAT | A | | | | | |
| Tes | ted Through | Premar | (Chok | e) 😉 | <u>)</u> | | | Type Ta | ips | Pipe | | |
| ~ | | | ow Data | | | | ng Data | Casing | Casing Data | | | |
| No. | (Prover) (Line) Size | (Choke | Prese | ss. Di | | | ļ | | | Duration of Flow | | |
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| 4. | | | | | | | | | - | | | |
| | | | | *. <u></u> | FLOW (| CALCULATI | ONS | ··· | | | | |
| No. | Coefficient | | | | re Flo | FLOW CALCULATIONS Flow Temp. Gravit, Factor Factor | | | | Rate of Flow Q-MCFPD | | |
| - 1 | (24-Hour) 7 | | h _w p _f | psia | | Ft | Fg | Fpv | | @ 15.025 psia | | |
| 1. 2. 3. 4. 5. | 12.365 | | | 547 | | 7723 | 960 | 8 1.05 | 0 | 6634 | | |
| 3. 4. | | | | | | | | | | | | |
| 5.1 | | , | | | | | | | | · | | |
| | | | | | | E CALCUTA | | | | | | |
| | Liquid Hydro ity of Liqui | | arbons | | — cf/bb | | Spe | cific Grav | ity Flo | arator Gas wing Fluid | | |
| | | | (1-e ^{-?} | <u> </u> | | | Pc- | 1928 | P ² | 3,717,184 | | |
| | $P_{\mathbf{w}}$ | | | | | | | | | | | |
| No. | Pt (psia) | P_{t}^2 | F_c^Q | (F _c | (a) ² | $(F_cQ)^2$ $(1-e^{-s})$ | P _w 2 | $P_c^2 - P_w^2$ | | $\begin{array}{c c} P_{\mathbf{W}} & P_{\mathbf{C}} \\ P_{\mathbf{W}} & P_{\mathbf{C}} \end{array}$ | | |
| 3 | | | | | | | 1,281,42 | 4 | | W | | |
| 3. | | | | | | | | | | | | |
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| ADDRESS 108 West Chucks, Astes, New Mexico | | | | | | | | | | | | |
| WIT | NT and TITLE NESSED | | | | | r. Prod. Waychoff | | Majura | TOT | ttrh_ | | |
| | PANY | | | | n Corpor | | | , | \&FP1 | TILD / | | |

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_w) . MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- $P_{\mathbf{w}}$ Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt- Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- F_{nv} Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.