MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised	12-1-55

Pool	Angel	Peak E	(tensi	e F	ormation	Dake	rta		County	San	Juna	
Initi	al XX		Annı	ual		Spec	ial		Date of	Test_	6/29/60	
Compa	anyat	ec 011	and O	o Cemp	му	Lease	McClane	hen	Wel	1 No	18-D	
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ate	of Comple	etion:	8/22/	/60	Packe	r	51	ngie-Brad Reserv	enhead-G. oir Temp.	G. or G	•0• Duai	
						OBSERV	ED DATA					
'este	ed Through		meek (Choke)					Type Tap	ε	····	
			Flow D	ata			Tubin	g Data	Casing D		 	
0.	(Prover)		noke) Lfice)		Diff.	Temp.	Press	. Temp.	Press.	Temp.	Duration of Flow	
ı	Size			psig	h _w	°F•	psig	°F.	psig	[⊃] F•	Hr.	
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0.	'w Pt (psia)	F	\mathbf{r}^2 F	CQ	$(F_cQ)^2$	(F	'c ^Q) ² -e ^{-s})	P _w 2	$P_c^2 - P_w^2$	Ca P	$\frac{P_{\mathbf{W}}}{P_{\mathbf{C}}}$	
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OMPA DDRE GENT	SS and TIT	toe Of	70, Pa	, 848		MCFPD;		0.75 Btovens,	Englaser			
	ESSED	170					IARKS			RLCE	VFN	

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_w) . MCF/da. @ 15.025 psia and 60° F.
- P_c I 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- P_t Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- F_t Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.

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