

NEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA  
EXCEPT BARKER DOME STORAGE AREA)

Pool Basin Formation Dakota County San Juan  
Purchasing Pipeline Southern Union Gas Company Date Test Filed Jan. 5, 1961  
Operator Astec Oil and Gas Company Lease McClanahan Well No. 18-D  
Unit A Sec. 13 Twp. 28 Rge. 10 Pay Zone: From 6272 To 6396  
Casing: OD 4 1/2 WT. 9.90 Set At 6450 Tubing: OD 2 3/8 WT. 4.70 T. Perf. 6194  
Produced Through: Casing \_\_\_\_\_ Tubing X Gas Gravity: Measured 0.682 Estimated \_\_\_\_\_  
Date of Flow Test: From 12/7 To 12/15 \* Date S.I.P. Measured 12/23/60  
Meter Run Size 4 Orifice Size 2.500 Type Chart S R Type Taps Flg.

OBSERVED DATA

Flowing casing pressure (Dwt) 809 psig + 12 = 821 psia (a)  
Flowing tubing pressure (Dwt) 731 psig + 12 = 743 psia (b)  
Flowing meter pressure (Dwt) 553 psig + 12 = 565 psia (c)  
Flowing meter pressure (meter reading when Dwt. measurement taken:  
Normal chart reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (d)  
Square root chart reading (7.80)<sup>2</sup> x spring constant 10 = 608 psia (d)  
Meter error (c) - (d) or (d) - (c) ± = -13 psi (e)  
Friction loss, Flowing column to meter: \_\_\_\_\_ = 148 psi (f)  
(b) - (c) Flow through tubing: (a) - (c) Flow through casing  
Seven day average static meter pressure (from meter chart): \_\_\_\_\_  
Normal chart average reading 596 psig + 12 = 608 psia (g)  
Square root chart average reading (\_\_\_\_\_)<sup>2</sup> x sp. const. \_\_\_\_\_ = \_\_\_\_\_ psia (g)  
Corrected seven day avge. meter press. (p<sub>f</sub>) (g) + (e) \_\_\_\_\_ = 595 psia (h)  
P<sub>t</sub> = (h) + (f) \_\_\_\_\_ = 743 psia (i)  
Wellhead casing shut-in pressure (Dwt) 1779 psig + 12 = 1791 psia (j)  
Wellhead tubing shut-in pressure (Dwt) 1774 psig + 12 = 1786 psia (k)  
P<sub>c</sub> = (j) or (k) whichever well flowed through \_\_\_\_\_ = 1786 psia (l)  
Flowing Temp. (Meter Run) 82 °F + 460 \_\_\_\_\_ = 542 °Abs (m)  
P<sub>d</sub> = 1/2 P<sub>c</sub> = 1/2 (l) \_\_\_\_\_ = 893 psia (n)

FLOW RATE CALCULATION

$$Q = \frac{2360}{(\text{integrated})} \times \left( \frac{\sqrt{(c)}}{\sqrt{(d)}} \right)^{0.5} = \frac{(0.9786)}{0.9893} = 0.9893 = 2335 \text{ MCF/da}$$

DELIVERABILITY CALCULATION

$$D = Q \frac{2335}{\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^{0.75}} = \frac{2335}{\left[ \frac{2392347}{2510505} \right]^{0.75}} = 2252 \text{ MCF/da.}$$

SUMMARY

P<sub>c</sub> = 1786 psia  
Q = 2335 Mcf/day  
P<sub>w</sub> = 820 psia  
P<sub>d</sub> = 893 psia  
D = 2252 Mcf/day

Company Astec Oil and Gas Company  
By ORIGINAL SIGNED BY L. M. STEVENS  
Title L. M. Stevens, Dist. Engr.  
Witnessed by \_\_\_\_\_  
Company \_\_\_\_\_

- \* This is date of completion test.
- \* Meter error correction factor

REMARKS OR FRICTION CALCULATIONS

GL	(1-e <sup>-S</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> ) R <sup>2</sup>	P <sub>t</sub> <sup>2</sup> (Column i)	P <sub>t</sub> <sup>2</sup> + R <sup>2</sup>	P <sub>w</sub>
<u>1224</u>	<u>0.264</u>	<u>481.978</u>	<u>127.242</u>	<u>552.049</u>	<u>679.291</u>	<u>820</u>