Parrie	od i	12-	-5	L

Size   Size   psig   hw   °F.   psig   °F.   psig   °F.   Hr.	Poo.	l <u>Ange</u>	Peak	·····	_Formation	Dakot	a		County	San Ji	uan	
### Sec. 33 Twp 28N Fig. 10W Purchaser Southern Union Gas Co.    Dasing 4½" Wt. 11.6   1.0. 4"   Sev. 26   6730   Fort.   6550 KB   To   6600KB	Ini	tial <u>XX</u>		Annual		Spec	cial		Date of	Test	11-23 1960	
Dasing 4½	Com	pany_Sunset	t Inter	. Petr.	Corp	Lease	Kutz Fe	deral	Wel	l No	1 <b>3-3</b> 3	
Dasing 4½	Uni	tK	Sec. <u>33</u>	Twp2	2 <b>8N</b> Ré	e. <u>10W</u>	Pur	haser_S	outhern	Union	Gas Co.	
Tubing 2 7/8 Wt. 6.7 I.D. 2 1/2 Set at 6522 Ferf. Open End To  Gas Pay: From 5472 To 6672 L x3												
Gas Fay: From 6472 To 6672 L xGOLBar.PressI_O												
Producing Thru: Casing												
Date of Completion: 11-15-1960   Facker 6452   Reservoir Temp.   160												
Tested Through   (SDOWNEX)   (Choke)   (Modexy)	Date	e of Complet	tion: 11	-15-196	n Packe	r 6452	Sid	gle-Brade Reserve	enhead-G. oir Temp.	G. or (	3.0. Dual	
Tested Through (			u-44.4		<del></del>				_	<del></del>		
Flow Data   Turing Data   Casing Data	Test	ted Through	( Breathern	r) (Chok	a) (Matami		DD DETK		Time Tan	.5		
Press						- Also and within a wild distance	7	Dota			-	
Size   Size   psig   hw   CF.   psig   CF.		(Prover)	(Choke	e) Pres	ss. Diff.	l'emp.		<del></del>			Duration	
SI	No.				ig h	∣ ° <sub>F</sub> .	asia	OF.	nsig	o <sub>F</sub>	1	
1. 3/4 " 317 70 317 70 3 Hours  2. 2. 4. 5.	SI				-0W		<del></del>	<del></del>	<del> </del>			
Show Calculations   Pressure   Flow Temp.   Gravity   Compress.   Rate of Flow   Pressure   Flow Temp.   Factor   Fact	1. 2.		3/4 "	31	7	70					3 Hours	
FLOW CALCULATIONS   Flow Temp.   Gravity   Compress.   Rate of Flow   Factor   Fac	<u>3.</u>											
Coefficient   Pressure   Flow Temp.   Gravity   Factor	4.							+	<del> </del>	ļ		
Coefficient   Pressure   Flow Temp.   Gravity   Compress.   Rate of Flow   Q-MCFPD   Pactor   Factor   Factor   Factor   Factor   Factor   Factor   Factor   Factor   Provided			<u> </u>			ESS CALL CAT	CIT ATTO	C	<u> </u>	<del></del>		
(24-Hour)   \( \sigma \)   \( \text{Pp} \)   \( \text{Psia} \)   \( \text{Psia} \)   \( \text{Pp} \)   \( \text{Psia} \)   \( \text{Pp} \)   \( \text{Pp} \)   \( \text{Pp} \)   \( \text{Psia} \)   \( \text{Pp} \)   \( Pp		Coeffici	ent			Flow	Temp.	Gravity			1	
1. 12.3650 329 .9905 .9325 1.037 3896  2. 3. 4. 5.	No.	(24-Hou	ır)	hwpf	p <b>si</b> a	Fac F	tor	Factor F <sub>o</sub>	Facto	r	Q-MCFPD @ 15.025 psia	
PRESSURE CALCULATIONS  as Liquid Hydrocarbon Ratio c2/bbl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid.60 ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.60 r. 5.55/ (1-e^-s) 0.280 P <sub>c</sub> 1904 P <sub>c</sub> 3625216  No. Pw Pt (psia) Pt F <sub>c</sub> Q (F <sub>c</sub> Q) <sup>2</sup> (F <sub>c</sub> Q) <sup>2</sup> (F <sub>c</sub> Q) <sup>2</sup> P <sub>w</sub> 2 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> Cal. Pw P <sub>c</sub> P <sub>c</sub> 19. 329 (0824/ 2/626.7 4877/9 82560 95.95% 3029.26 772  Absolute Potential: 4453 MCFPD; n re	1.	12,3650			329							
PRESSURE CALCULATIONS  as Liquid Hydrocarbon Ratio c2/bbl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid.60 Pc 1904 Pc 3625216  No. Pw Pt (psia) Pt FcQ (FcQ) <sup>2</sup> (FcQ) <sup>2</sup> (FcQ) <sup>2</sup> Pw Pc Pc Pc Pw Pc Pc Pc Pc Pw Pc Pc Pc Pw Pc	3.											
PRESSURE CALCULATIONS  as Liquid Hydrocarbon Ratio c./bbl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.67) ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Hydrocarbons deg. Specific Gravity Fluid Hydrocarbons deg. Specific Gravity Fluid Hydrocarbons deg. Speci	4.											
as Liquid Hydrocarbon Ratio c:/bbl. Specific Gravity Separator Gas_ravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid.60 P. 1904 P. 3625216  No. Pw Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 Pw2 Pc-Pw Cal. Pw Pc To					ממ	geempr a	ACCID AT	ONS				
Pw					T.R.							
C. S.55/ $(1-e^{-s})$ O.28c) $P_c = 1904$ $P_c^2 = 3625216$ No. $P_w = P_t =$				arbons				Speci	fic Gravi	ty Flow	ing Fluid 69	
No. Pt (psia) Pt FcQ (FcQ) (FcQ) Pw2 Pc-Pw Cal. Pw Fc Pt (1-e-s) Pw Pc Pw Pc Pc Pc Pw Pc	`c	5,55,	<u>/</u>	(1-e <sup>-s</sup>	0.280	3		P <sub>c</sub> 19	004	P <sub>c</sub> 36	625216	
No. Pt (psia) Pt FcQ (FcQ) (FcQ) Pw2 Pc-Pw Cal. Pw Fc Pt (1-e-s) Pw Pc Pw Pc Pc Pc Pw Pc		D		<u> </u>						<del>,</del>		
Pt (psia)  1. 329	No.		$_{ m Pt}^2$	F <sub>c</sub> Q	$(F_cQ)^2$	(F	<sub>c</sub> Q) <sup>2</sup>	$P_w^2$	$P_c^2 - P_w^2$		1 24 1	
Absolute Potential: 4453 MCFPD; n ma	1.		108241	21626-7	4877/3	(1	-e⁻3)	95 454	3020 20		w Pc	
Absolute Porential: 4453 MCFPD; n ma	2.								3007.00	1		
Absolute Porential: 4453 MCFPD; n ma	4.									<del> </del>		
COMPANY GUAGGE Totamartiana P. Datrick with	5.											
ADDRESSAGO S. Beverly Dr. Beverly Hills Calif / 5th Floor 444-17 th Street AGENT and TITLE Thomas F. Popp Dist. Engr. Denver. 2.Colo.					3 7 7 .							
AGENT and TITLE Thomas F. Popp Dist. lingr. Denver. 2.Colo.	ADDR	ESS400 S.	Beverl	<del>nation</del> s y Dr. F	Reverly Petr	Milds C	alif /	5th Flo	0: 444-1	7 th	Street	
WITNESSED Thomas I- Page	AGEN WII'N	T and TITLE ESSED	Thomas	SF POR	<del>pp Dist</del>	- <del>Brigge</del>		Denver,	2,Colo.			

Squeezed Cement Collar & 2012, meld 3000 psi OK, but did not wish to Frac against. Set Retv. Packer and completed and produced under packer

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q  $\equiv$  Actual rate of flow at end of flow period at W. H. working pressure (Pw). MCF/da. @ 15.025 psia and  $60^o$  F.
- $P_c$ I 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw. Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_{f}$  Meter pressure, psia.
- hwI Differential meter pressure, inches water.
- FgI Gravity correction factor.
- Ft Flowing temperature correction factor.
- $F_{pv}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $F_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .