

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		2-5-81																															
Company				Connection																																					
SUPRON ENERGY CORPORATION				Southern Union Gathering Company																																					
Pool				Formation				Unit																																	
Bloomfield Ext.				Chacra																																					
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name																																	
1-23-81		3170		3121		5808		Zachry																																	
Csg. Size	Wt.	d	Set At	Perforations		To		Well No.																																	
2.875	6.50	2.441	3153	From 2967		3086		24																																	
Tub. Size	Wt.	d	Set At	Perforations		To		Unit Sec. Twp. Rge.																																	
No Tubing				From				N 10 28N 10W																																	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple						Packer Set At		County																																	
Single						---		San Juan																																	
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State																																	
Casing		8				12		New Mexico																																	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover		Meter Run		Taps																															
2957		0.650																																							
FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow																															
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F																															
SI	2"		3/4"						1029		7 days																														
1.									32	60°	3 hours																														
2.																																									
3.																																									
4.																																									
5.																																									
RATE OF FLOW CALCULATIONS																																									
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																		
1	12.3650		44	1.0000	0.9608	1.000	523																																		
2.																																									
3.																																									
4.																																									
5.																																									
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio		Mcfd/bbl.																																		
					A.P.I. Gravity of Liquid Hydrocarbon		Deg.																																		
1					Specific Gravity Separator Gas		XXXXXXXXXXXX																																		
2.					Specific Gravity Flowing Fluid																																				
3.					Critical Pressure		P.S.I.A.																																		
4.					Critical Temperature		°F																																		
5.																																									
P_c 1041 P_c² 1,083,681 <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>NO.</td> <td>P_i</td> <td>P_w</td> <td>P_i²</td> <td>P_i² - P_w²</td> </tr> <tr> <td>1</td> <td></td> <td></td> <td>3032</td> <td>1,080,649</td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> </tr> </table> (1) $\frac{P_c^2}{P_i^2 - P_w^2} = 1.0028$ (2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1.0021$ AOF = Q $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 524$												NO.	P _i	P _w	P _i ²	P _i ² - P _w ²	1			3032	1,080,649	2.					3.					4.					5.				
NO.	P _i	P _w	P _i ²	P _i ² - P _w ²																																					
1			3032	1,080,649																																					
2.																																									
3.																																									
4.																																									
5.																																									
Absolute Open Flow						524		Mcf @ 15.025		Angle of Slope @																															
										Slope, n 0.75																															
Remarks:																																									
Approved by Division				Conducted by				Calculated by				Checked by																													
				David Roark				Kenneth E. Roddy																																	