

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 3-22-83	
Company Union Texas Petroleum Corp.				Connection Southern Union Gathering Company	
Pool Basin				Formation Dakota	
Completion Date 1/31/83		Total Depth 6576		Plug Back TD 6518	
				Elevation 5850	
Casing Size 9.625 7.000				Well No. 24-E	
Wt. 40.00 23.00		d 8.835 6.366		Set At 5390 5211-6569	
Perforations: From 6300 To 6419					
Thq. Size 2.375		Wt. 4.70		d 1.995	
Set At 6375		Perforations: Open - Ended From To			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas - Oil				Packer Set At 6150	
Producing Thru Tubing				Reservoir Temp. °F #	
Mean Annual Temp. °F 12				Baro. Press. - P _a 12	
L 6365		H		Gg 0.700	
% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run		Taps	
FLOW DATA					
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w
1.	2"		3/4"		
2.					
3.					
4.					
5.					
TUBING DATA					
	Press. p.s.i.g.	Temp. °F			
	460	57°			
	20				
CASING DATA					
	Press. p.s.i.g.	Temp. °F			
RATE OF FLOW CALCULATIONS					
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg
1	12.3650		32	1.0029	0.9258
2.					
3.					
4.					
5.					
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons Deg.
2.					Specific Gravity Separator Gas X X X X X X X X
3.					Specific Gravity Flowing Fluid X X X X X
4.					Critical Pressure P.S.I.A. P.S.I.A.
5.					Critical Temperature R R
$P_c = 472$ $P_c^2 = 222,784$					
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0198$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0148$
1			4322	218,462	
2					
3					
4					
5					
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 372$					
Absolute Open Flow 372 Mcfd @ 15.025				Angle of Slope @ Slope, n 0.75	
Remarks:					
Approved By Division		Conducted By: Clifton Gates		Calculated By: Ken Roddy	
Checked By:					